

# Experimental Observation of Self-Organised Mode-Locked Emission in a W-Band Free-Electron Maser

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## Abstract

Experimental observation is reported of passive, self-organised mode-locking in a high-power free-electron maser (FEM) oscillator operating near 103 GHz, using a ~1.36 MeV, 1.15 A energy-recovered electron beam. Macropulses of 10  $\mu$ s duration were recorded in which mode-locking is established from the onset of measurable radiation and persists throughout the pulse. Power-detector and heterodyne measurements show a regular train of kW-level spikes with a spacing of 10.4 ns, consistent with the cavity free spectral range. A modal analysis of the intermediate-frequency signal reveals strong phase coherence across more than sixteen longitudinal modes. A distinct sideband appears with a spacing that remains stable to within 0.2 MHz even though the carrier frequency drifts by several megahertz between pulses due to variations in beam energy. This behaviour contradicts the power-dependent scaling expected from synchrotron-driven FEL sidebands and instead indicates a cavity-anchored coupling mechanism. The results demonstrate that robust passive mode-locking can arise naturally in mm-wave FEM oscillators without external modulation.

*Index Terms*—FEL Oscillator, Mode-Locking, Free Electron Maser, Carrier-Modulation.

## 1. Introduction

Free electron masers and lasers (FEM/FEL) are a class of vacuum electronic device that can produce coherent and directed electromagnetic radiation from mm-waves to X-rays. They work by forcing the transfer of energy from a relativistic electron beam to a radiation field. Relativistic electrons are directed into an undulator, a sinusoidal arrangement of a magnetic or electric field (most commonly a static magnetic field) [1]. This work is concerned with an FEM operating with a continuous electron beam with energy close to 1.36 MeV, in an oscillator configuration. A resonator sits within the undulator, and a proportion of the radiation generated is reflected back from an outcoupling mirror and contained within the resonator [2].

The gain curve of an FEM/FEL will cover a frequency range related to the beam energy and system parameters. Within this range an oscillator enforces the condition that only certain discrete frequencies can oscillate without high loss, these are the longitudinal modes. Any mode can grow if the multiple of gain ( $G$ ) and roundtrip reflectivity ( $R_{rt}(f)$ ) is greater than one,  $GR_{rt} > 1$ . Competition exists between these possible modes. Factors which influence a single-frequency outcome include both the gain profile and roundtrip-reflectivity, which is a function of frequency. A weak external signal can be injected into the cavity to bias mode competition and accelerate the rise of a particular longitudinal mode [3, 4], which is useful when a single carrier frequency and narrow bandwidth are desirable, such as for high-capacity mm-wave links [5, 6].

Conversely, it is possible to bias the mode competition such that many longitudinal modes can co-exist. This produces a periodic train of spikes of wideband radiation. This is called Mode-Locking and is a well-known phenomenon widely explored in the optical domain [7, 8]. Less commonly it has been

44 demonstrated in a variety of vacuum electronic devices in the microwave and millimetre-wave bands.  
45 Mode-Locking is critical for metrology, time-keeping, and ultra-fast imaging, where a regular train of  
46 narrow (but broadband) pulses is essential [9]. In the mm-wave/THz domain this can be used for fault  
47 detection and imaging [10].

48 Alberti et al. reported generation of mode-locked pulses around 260.5 GHz by Q-switching the cavity.  
49 Rapid intracavity power swings generate sidebands that support multi-mode operation. Spikes of 1.2  
50 ns width were measured with a 4.2 ns repetition rate and peak power of  $\sim 5$  W [11]. The limited  
51 sideband structure generated by the modulation constrains the extent of achievable mode locking.

52 Traveling-wave tubes (TWTs) are broadband amplifiers that operate with a slow-wave structure [12].  
53 Ginzburg et al. recently showed that a gyro-TWT operating with two beams, one of which acts as a  
54 saturable absorber, can be used to produce mode-locked output. Pulses in the Ka-band (26–40 GHz)  
55 with FWHM  $\approx 0.4$  ns, peak intensity  $\sim 100$  kW, and a repetition rate of 2.5 ns were measured [13]. In  
56 the W-band, Rozental et al. simulated a TWT using a feedback delay [14]. Numerical modelling predicts  
57 sub-nanosecond pulse formation; the authors note that in practice an additional amplifier could  
58 increase the available output power.

59 In Free Electron Masers, Jerby and Bekefi demonstrated mode-locking at 8–11 GHz with a period of  
60 37 ns and a micro-pulse width of 5 ns using a quasi-CW 250 A beam at 250 keV [15]. A PIN-diode  
61 modulator was inserted into the ring cavity, controlling transmission (amplitude modulation) with a  
62 period equal to the cavity roundtrip time (power inferred  $< 2$  kW). Backward-wave interactions have  
63 been explored in certain low-energy ( $\sim 45$  keV), dispersion-engineered free-electron devices employing  
64 periodically loaded slow-wave structures, where they can influence gain and spectral structure [16].  
65 Savilov et al. modelled mode-locking behaviour in a klystron-like FEM using a small-signal injection  
66 region for modulation before the undulator [17]. The theory of mode-locking in FELs has been  
67 previously described [18, 19].

68 Collectively, these demonstrations rely on active modulation or engineered nonlinearities. In  
69 contrast, passive self-organized mode-locking in high-power mm-wave FEL/FEM oscillators remains  
70 comparatively unexplored and experimentally under-documented. In the present work, passive  
71 coupling of the longitudinal modes enables continuous mode-locked operation without active  
72 modulation, secondary electron beams, or intra-cavity PIN diodes.

73 Ottaviani et al. [20] described the simulated formation of ‘frozen spikes’ in deeply saturated FEL  
74 oscillators in terms of sideband instability and super-mode coupling. A behaviour that is physically  
75 equivalent to passive mode-locking. However, in our case the locking frequency remains fixed  
76 independent of intra-cavity power, indicating a distinct beam-mediated inter-mode coupling  
77 mechanism rather than the synchrotron oscillation driven sideband process commonly described in  
78 FEL simulations. While the theoretical literature on FEL-oscillator mode-locking is extensive, there are  
79 comparatively few time-resolved experimental measurements. The present work provides direct  
80 observations of the spectral and temporal evolution of the oscillator during the onset of locking and  
81 throughout a steady-state train of spikes until the beam is switched off.

## 82 2. Experimental Setup

83 An energy recovery electrostatic accelerator was used to supply the  $\sim 1.36$  MeV electron beam. The  
84 1.15 A beam was derived from capacitors which are trickle charged by a 50 kV supply. The overall setup  
85 is shown in Fig. 1. The electron beam generated from the thermionic cathode transfers only a small  
86 fraction of its kinetic energy in the interaction region; simulations for similar conditions indicate an

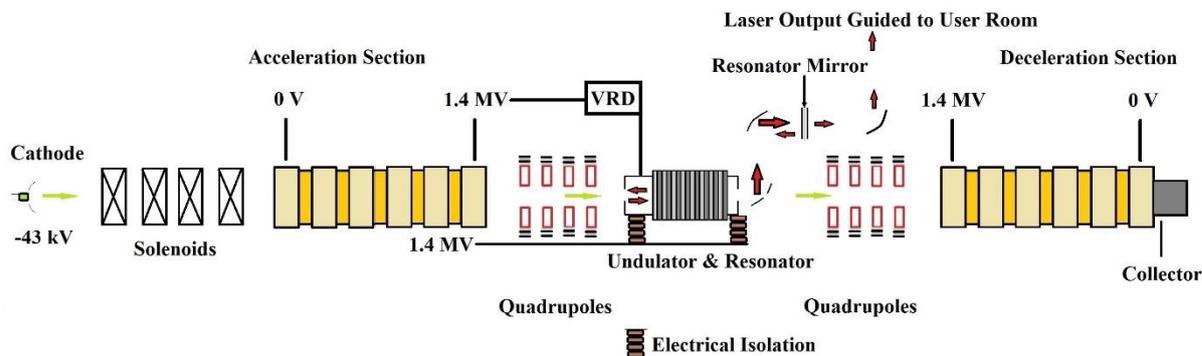
87 average energy decrease of order  $\sim 45$  keV [21], with a broadened post-interaction energy distribution  
88 (some electrons gain energy while the majority lose). Then the electrons are decelerated such that  
89 they are collected at low energy. This means the majority of the electron energy is recovered and a  
90 distinction should be made between the electronic efficiency and the overall system efficiency.

91 There are eight controllable focusing elements before the undulator: four focusing coils in the low-  
92 energy injector region and four quadrupoles after electrostatic acceleration to  $\sim 1.36$  MeV. In  
93 addition, steering elements are used to maintain beam alignment, and the acceleration line itself  
94 provides some focusing. In the present setup, imperfect electron collection leads to a gradual  
95 discharge of the high-voltage terminal during operation, resulting in a beam-energy decrease at a  
96 rate of approximately  $1$  kV/ $\mu$ s. This behaviour is not inherent to Van de Graaff accelerators, but  
97 reflects practical engineering constraints of the present system. The resulting slow energy drift  
98 causes modest frequency pulling of the longitudinal modes, but does not significantly affect the  
99 stability of masing or mode-locking over the  $\sim 10$   $\mu$ s pulse duration. To mitigate this effect, a voltage-  
100 ramping device (VRD) is connected to the undulator and resonator. When the VRD is employed the  
101 resonator is electrically isolated from the high-voltage terminal, and its potential can be ramped  
102 relative to the terminal during the pulse, increasing the electron kinetic energy upon entry to the  
103 undulator. By appropriate choice of ramp rate, this allows partial or complete compensation of the  
104 terminal voltage droop, or deliberate over-compensation when required. After leaving the resonator,  
105 the electron beam is decelerated back to the terminal potential. The VRD waveform is set to begin  
106 after a user-defined delay, and the ramped voltage is discharged after a further user-defined interval,  
107 returning the resonator potential to its pre-ramped state. The microwave power extracted during  
108 masing is supplied by the relatively low-voltage, high-current systems; ideally, no significant energy is  
109 drawn from the high-voltage terminal itself. Further details of the VRD operation are given in earlier  
110 work [21, 22].

111 The undulator is a planar Halbach type with 26 periods of 44.4 mm, composed of SmCo bar magnets  
112 [23]. The resonator main interaction region which sits within the undulator is an 890 mm waveguide  
113 with two corrugated and two smooth walls. The corrugations are on the walls in the plane of the  
114 electron oscillations, with overall waveguide width 15 mm, and height 10.7 mm, the corrugations  
115 have depth 0.75 mm, and period 0.8 mm. The corrugated interaction waveguide supports the  
116 fundamental  $HE_{11}$  eigenmode with smooth transmission across the operating band and does not  
117 introduce mode conversion. Two additional sections form the ends of the resonator and decouple  
118 the electron beam from the microwaves. The electrons enter the resonator via a flat rectangular  
119 window which is fixed to the end of a smooth-walled 25 mm wide by 10.7 mm high waveguide of  
120 length 210 mm. At the other end of the corrugated waveguide a second smooth-walled section is  
121 connected, likewise with dimensions 25mm width, and 10.7 mm height. Electrons exit the resonator  
122 through a hole in a parabolic mirror 208 mm from the junction with the corrugated waveguide. The  
123 parabolic mirror reflects the masing radiation up out of the electron-beam line to a second parabolic  
124 mirror arranged in a confocal configuration. The radiation is then reflected to a series of wire-grids  
125 which control the out-coupling of the radiation. When the fundamental  $HE_{11}$  mode diffracts into the  
126 wider smooth-walled section, splitting and subsequent recombination of the radiation enable  
127 effective de-coupling of the electron beam and the microwave field [24, 25]. The specific resonator  
128 configuration and testing is described in detail in a prior work [26]. The total optical length of the  
129 resonator is 1.514 m. The cathode to collector distance is 13.48 meters, table I details the main  
130 system specifications.

131 A transmission line consisting of cylindrical corrugated waveguides transports the masing power to  
132 a user room. Power and frequency are sampled using a mixer (Quinstar QMB-FB BB W) and a power

133 detector (Millitech DXP-10 RPFW0). An HP sweep oscillator (86290B) is set to constant frequency out  
 134 and used in combination with a Millitech 380 AMC 10-RFH00 A16800 for the Local Oscillator. The  
 135 signals have been recorded on a Keysight DSCX3104A 5 GS/s, 1 GHz bandwidth oscilloscope.



136  
 137 Fig. 1. Schematic of the EA-FEM based on a Tandem Van-der-Graaf generator. The electrons are generated using a thermionic cathode. They  
 138 are focused and then injected into an acceleration section, which is located within a high-pressure tank where they are brought to near the  
 139 speed of light. Beyond this, they are focused with quadrupoles into the undulator and resonator combination to generate maser radiation.  
 140 Beyond this they are re-focused and decelerated.

141

TABLE I: PROPERTIES OF THE EA-FEL

Beam Current	1-2 A
Beam Energy	1.35-1.45 MeV
Undulator Period	$\lambda_U = 44.4 \text{ mm}$
Undulator Periods	$N_U = 24$
Undulator field Amplitude	0.193 T
Waveguide Fundamental Mode	$HE_{11}$
Radiation Frequency	95-110 GHz

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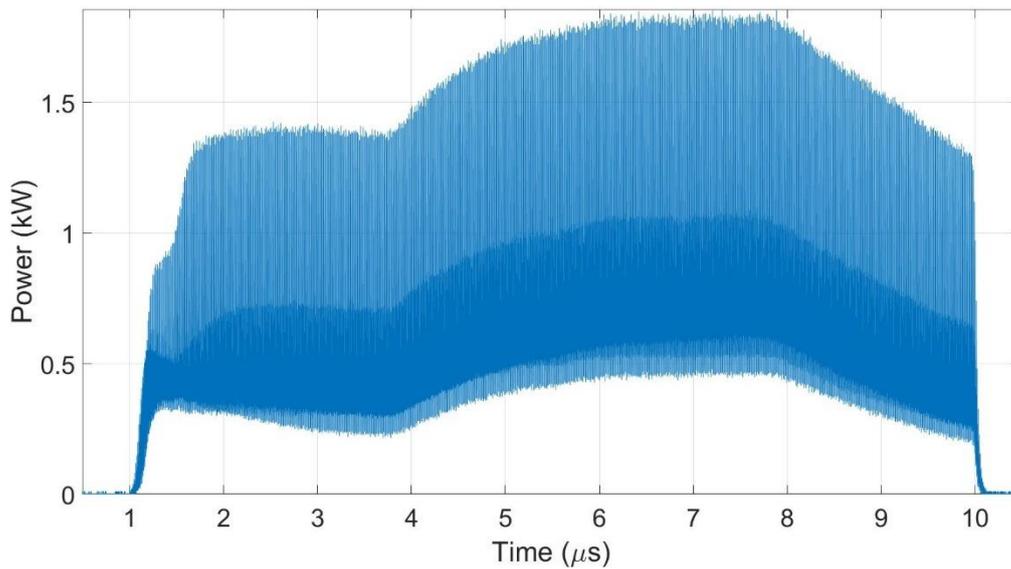
### 143 3. Results

144 Figure 2 shows the detected power profile of a  $10 \mu\text{s}$  self-mode-locked pulse centred near 103 GHz.  
 145 Mode-locked spikes appear from the very start of the measurable signal and persist for the full pulse  
 146 duration. The shape of the macropulse reflects the evolving electron beam energy. Up to  $3.8 \mu\text{s}$  the  
 147 terminal voltage decreases at  $\sim 0.98 \text{ kV}/\mu\text{s}$ , causing a gradual reduction in power. At  $3.8 \mu\text{s}$  an 18 kV  
 148 voltage ramp is applied to the beam, producing an intra-pulse increase in electronic efficiency and a  
 149 corresponding rise in power. The ramp is discharged at  $7.8 \mu\text{s}$ , after which the power decreases  
 150 again. These changes in power are driven by the beam-energy evolution and are independent of the  
 151 mode-locking mechanism. A shorter segment from 0– $3.6 \mu\text{s}$  is shown in Fig. 3, where the periodic  
 152 structure is more clearly resolved. This regular train of spikes arises from a fixed-phase relation  
 153 between many simultaneously excited longitudinal modes.

154

155 To show the modal behaviour in the time domain a spectrogram was generated from the  
 156 Intermediate Frequency (IF), see Fig. 4. The Local Oscillator (LO) was set to 102.498 GHz. Clearly  
 157 many modes are in simultaneous masing throughout the pulse. There are modes above and below  
 158 the LO, the modes below the LO are folded onto the positive x-axis. Modes above and below the LO  
 159 can be distinguished by their spacing and the direction the frequency is pulled when the accelerating  
 160 potential goes down or up. To consider the relative weight of the modes a Fast Fourier Transform  
 161 (FFT) of the IF is plotted in Fig. 5. In addition to the longitudinal modes, sidebands can be observed  
 162 due to the Amplitude Modulation of the modes. Figure 6 shows a narrower time slice of the power  
 163 measurement. The mean period over 727 successive spikes is 10.32 ns, with a standard deviation of

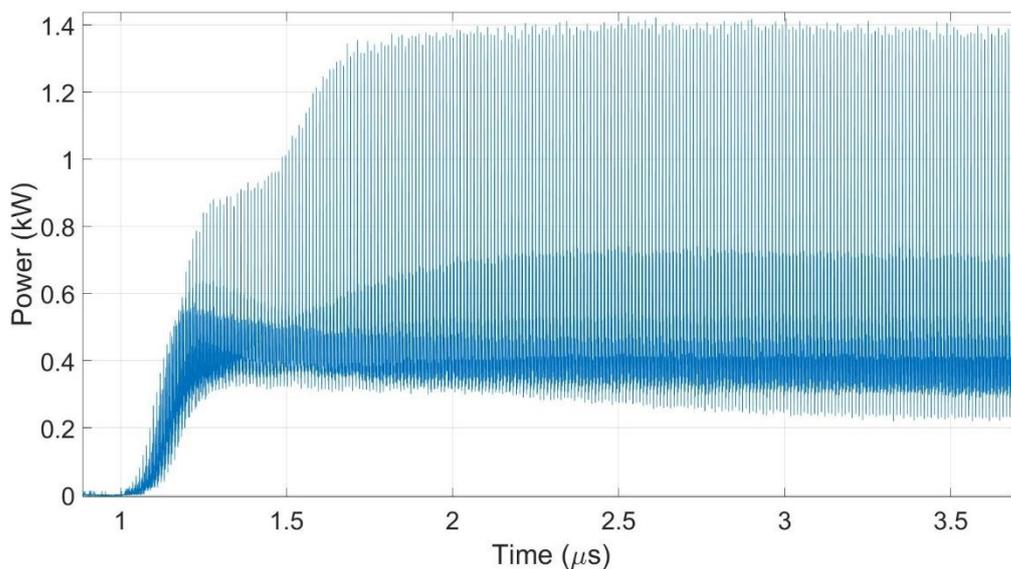
164 0.1 ns. The apparent full width at half maximum (FWHM) of the spikes is  $1.4 \pm 0.2$  ns as measured by  
165 the power detector; this width is limited by the temporal response of the detection system.  
166



167

168 Fig 2: Power as a function of time showing self-mode-locking for the complete pulse. As is typical with this  
169 system the accelerating potential of the High-Voltage-Terminal (HVT) dropped at  $\sim -0.98$  kV/ $\mu$ s. At 3.8  $\mu$ s an 18  
170 kV ramp in the beam energy with a rise time of 0.63  $\mu$ s is started, it's discharged at 7.8  $\mu$ s. The terminal voltage  
171 was initially  $\sim 1.32$  MV (above the -43 kV of the cathode region) and the cathode current 1.15 A.

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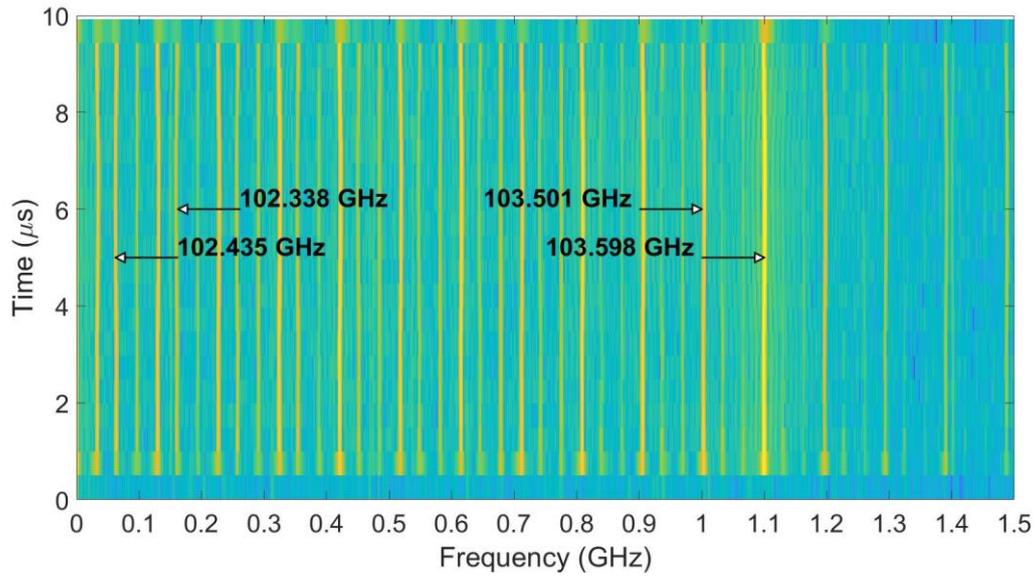


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174 Fig 3: Power as a function of time showing self-mode-locking for the first 3.5  $\mu$ s of a 10  $\mu$ s pulse. During this  
175 time the beam energy is falling at  $\sim -0.98$  kV/ $\mu$ s.

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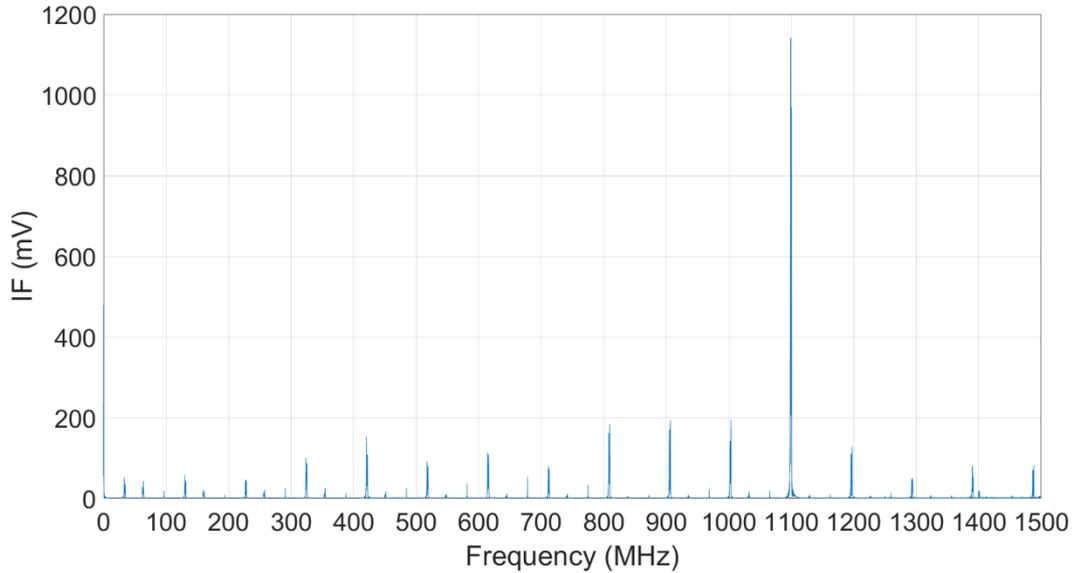
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179 Fig 4: Spectrogram of the IF of the pulse shown in Fig. 2. The Local Oscillator was set to 102.498 GHz. Free  
 180 Spectral Range (FSR)  $\sim$ 96.43 MHz.

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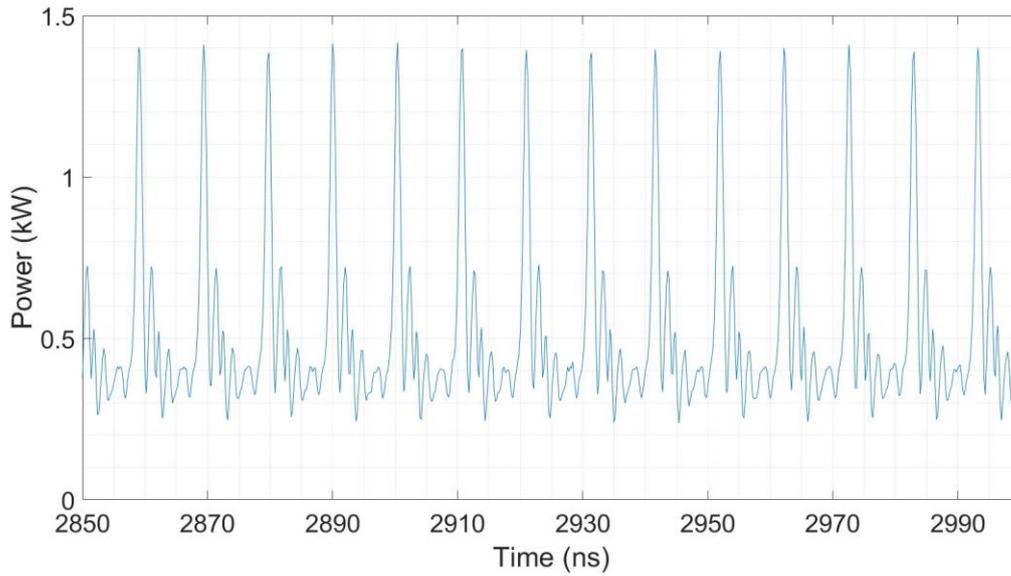
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185 Fig 5: Intermediate Frequency (IF) as a function of frequency for the pulse shown in Fig. 2. The Local Oscillator  
 186 (LO) is set to 102.498 GHz. Longitudinal modes above and below the LO are shown along the same positive  
 187 axis. The spacing of the longitudinal modes is 96.9 MHz. Between these longitudinal modes we also observe  
 188 sidebands due to the amplitude modulation of these modes.

189



190

191 Fig 6: Zooming in on a shorter time slice of Fig. 3 to show the broadband spikes in power. The spacing between  
192 these peaks is on average 10.32 ns, which corresponds to a frequency of 96.9 MHz. The FWHM of the peaks as  
193 measured with the power detector is  $1.4 \pm 0.2$  ns.

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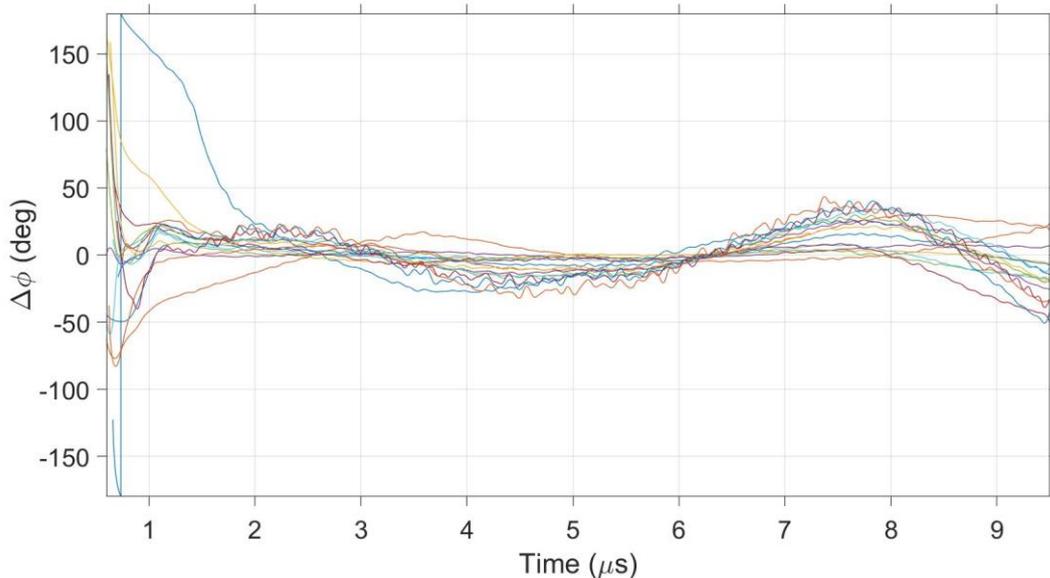
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198 3.1 Phase Coherence

199 Using the intermediate-frequency signal  $V_{IF}(t)$ , the relative phase evolution  $\Delta\phi_m(t)$  of each  
200 longitudinal mode  $m$  was extracted with respect to the dominant mode (by power) at 103.597 GHz.  
201 For each mode the complex envelope was obtained numerically by mixing  $V_{IF}(t)$  with  $e^{-i\omega_m t}$   
202 followed by low-pass filtering.  $\Delta\phi_m(t)$  was then defined as the difference between the  
203 instantaneous phase of mode  $m$  and that of the reference mode. Over the interval 2-9  $\mu\text{s}$ , seven of  
204 the strongest modes exhibit a mean absolute phase deviation  $\langle |\Delta\phi_m(t)| \rangle < 6.2^\circ$ . Across the full set  
205 of detected modes between 102.144 GHz and 103.694 GHz,  $\langle |\Delta\phi_m(t)| \rangle$  lies in the range  $2.2^\circ$ – $18.8^\circ$ .  
206 This confirms strong phase coherence among the dominant longitudinal modes throughout the  
207 macropulse and is consistent with stable passive mode-locking.

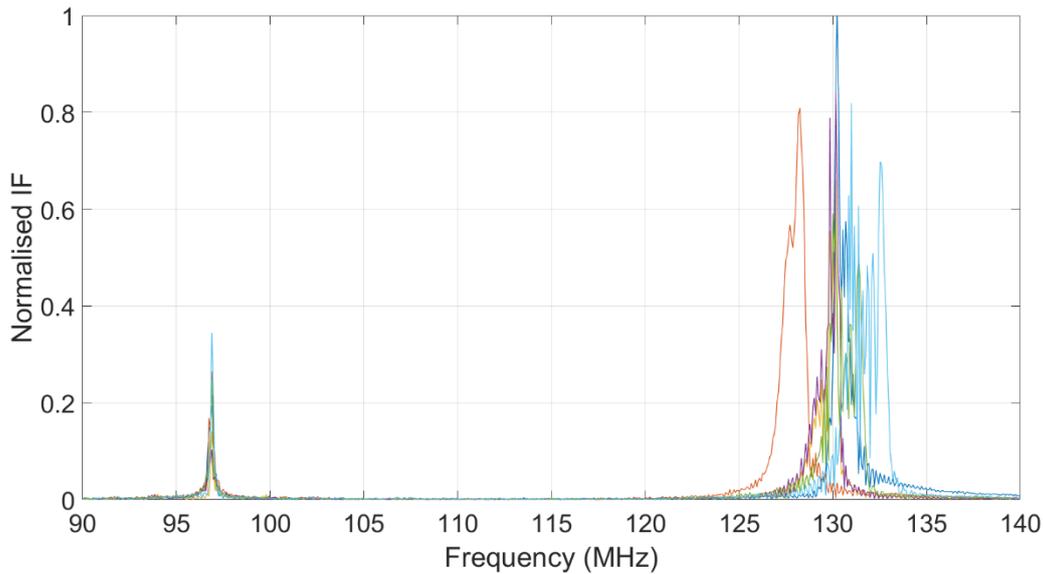


208  
209 Figure 7: Longitudinal mode phase coherence relative to the dominant mode at 103.597 GHz. Upper freq.  
210 range 103.694 GHz Lower freq. range 102.144 GHz.  
211

212 3.2 Sidebands

213 To examine the sideband behaviour, Fig. 8 shows the FFTs of six independent mode-locked pulses,  
214 each centred on a longitudinal mode and its lower sideband. Two features are immediately apparent.  
215 First, the carrier frequency (one of the longitudinal modes) shifts by several megahertz between  
216 pulses, reflecting the pulse-to-pulse variation in beam energy. Second, despite this carrier drift, the  
217 sideband frequencies remain fixed to within 0.2 MHz across all six pulses. The sidebands are  
218 therefore referenced to the laboratory frame rather than to the instantaneous resonant frequency of  
219 the beam. Although the relative sideband amplitudes vary both between and within pulses, their  
220 absolute frequencies remain essentially constant. This behaviour is consistent with a stable, cavity-  
221 defined mode-locking frequency that is insensitive to small changes in beam energy.

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227  
 228 Figure 8: Observing the overlaid FFT of six pulses focused in on a mode  $\sim 130$  MHz from the LO at 102.498 GHz  
 229 For each of the six pulses there is a corresponding lower sideband.  
 230

## 231 4. Discussion

### 232 4.1 Interpreting the Sideband Behaviour

233 In this system in the steady single-mode regime sidebands have not previously been noted. This is  
 234 consistent with the absence of significant amplitude modulation (AM). In the mode-locked regime,  
 235 however, the radiation field is a phase-locked sum of adjacent longitudinal modes and forms a pulse-  
 236 like envelope that circulates in the cavity. This envelope acts as an effective ponderomotive potential  
 237 supermode. In addition to the standing-wave field of the dominant longitudinal mode. In FEL theory,  
 238 trapped electrons oscillating in the ponderomotive potential can produce AM at the synchrotron  
 239 frequency  $\Omega_s$ , which depends on the radiation power and beam energy. Sidebands generated in this  
 240 way are expected to shift as the intra-cavity power and synchronism conditions change. In our  
 241 measurements, by contrast, the carrier frequency (a longitudinal mode) shifts by several megahertz  
 242 within and between pulses in response to small variations in beam energy, while the sideband  
 243 frequencies remain fixed to within 0.2 MHz across all six pulses shown in Fig. 8. Including in a pulse  
 244 where the output power changes by  $\sim 50\%$  during the macropulse. This behaviour rules out a simple  
 245 synchrotron-oscillation origin for the observed sidebands. Instead, the sideband frequencies are  
 246 effectively defined in the laboratory frame by the cavity dynamics of the mode-locked field (for  
 247 example via a parasitic higher-order mode path). They appear insensitive to changes in beam energy  
 248 or output power. Such cavity-anchored sidebands are consistent with a stable passive mode-locking  
 249 mechanism that is not governed by the space-charge-driven sideband processes commonly assumed  
 250 in FEL simulations.

251 The experimental evidence instead points to a mechanism anchored by the cavity rather than the  
 252 beam frame. A lab-fixed spectral offset of  $\sim 31\text{--}34$  MHz corresponds to an effective coupling delay of  
 253  $29\text{--}33$  ns, suggesting a fixed-path secondary feedback channel within the resonator system. The  
 254 precise origin of this delayed coupling is beyond the scope of the present work, but possibilities  
 255 include weak excitation of a higher-order resonator mode, unbalanced mode conversion or imperfect  
 256 recombination in the resonator decoupling sections or a small fraction of radiation returning via a

257 longer external path. Such pathways naturally generate a stable beating with the longitudinal mode  
258 comb, producing a passive and power-insensitive sideband spacing consistent with the observations.

#### 259 4.2 Periodic Spikes in Power, General Consideration

260 The FWHM of the spikes shown in Fig. 6 are limited by the response time of the detector. In free  
261 electron maser/laser oscillators the shortest achievable spike duration is limited by optical–electron  
262 slippage in the undulator. For the present undulator the slippage time is  $\tau_{\text{slip}} \approx 0.15$  ns, implying a  
263 minimum spike width of order  $2\tau_{\text{slip}} \approx 0.3$  ns. The corresponding Fourier-limited spectral width ( $\sim 5$   
264 GHz) represents an upper bound on the bandwidth of modes that can coherently participate in the  
265 mode-locked pulse. In practice, the number of contributing modes is further constrained by the  
266 frequency-dependent cavity reflectivity and gain profile.

267 The  $1.4 \pm 0.2$  ns FWHM spikes measured by the power detector reflects not the intrinsic pulse width  
268 but the instrument response; the actual field spikes are likely much narrower. The measured modal  
269 spectra in Fig. 5 show  $> 16$  identifiable longitudinal modes. This is consistent with a multi-gigahertz  
270 bandwidth and with spike envelopes substantially compressed relative to the detector-limited trace.

271 Overall, the temporal structure is consistent with passive mode-locking sustained by a broad, phase-  
272 coherent set of longitudinal modes rather than by power-dependent dynamical effects. The  
273 persistence of well-formed spikes throughout the  $10 \mu\text{s}$  macropulse suggests that the coupling  
274 mechanism stabilising the phases remains effective even as the beam energy and output power vary  
275 significantly during the pulse.

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277

## 277 **5. Conclusion:**

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279 This work has experimentally demonstrated passive, self-organised mode-locking in a high-power  
280 free-electron maser oscillator operating near 103 GHz. A train of temporally regular spikes persists  
281 for the full  $10 \mu\text{s}$  macropulse and is supported by strong phase coherence across more than sixteen  
282 longitudinal modes. The measured sideband spacing remains fixed to within 0.2 MHz even as the  
283 carrier frequency shifts by several megahertz, indicating that the locking frequency is defined by  
284 cavity dynamics rather than beam-dependent synchrotron processes. Together, these results show  
285 that stable passive mode-locking can arise naturally from the resonator's internal coupling, without  
286 external modulation, and over a wide range of beam conditions. Further work will examine the origin  
287 of the effective coupling path responsible for the observed cavity-anchored sideband structure.

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