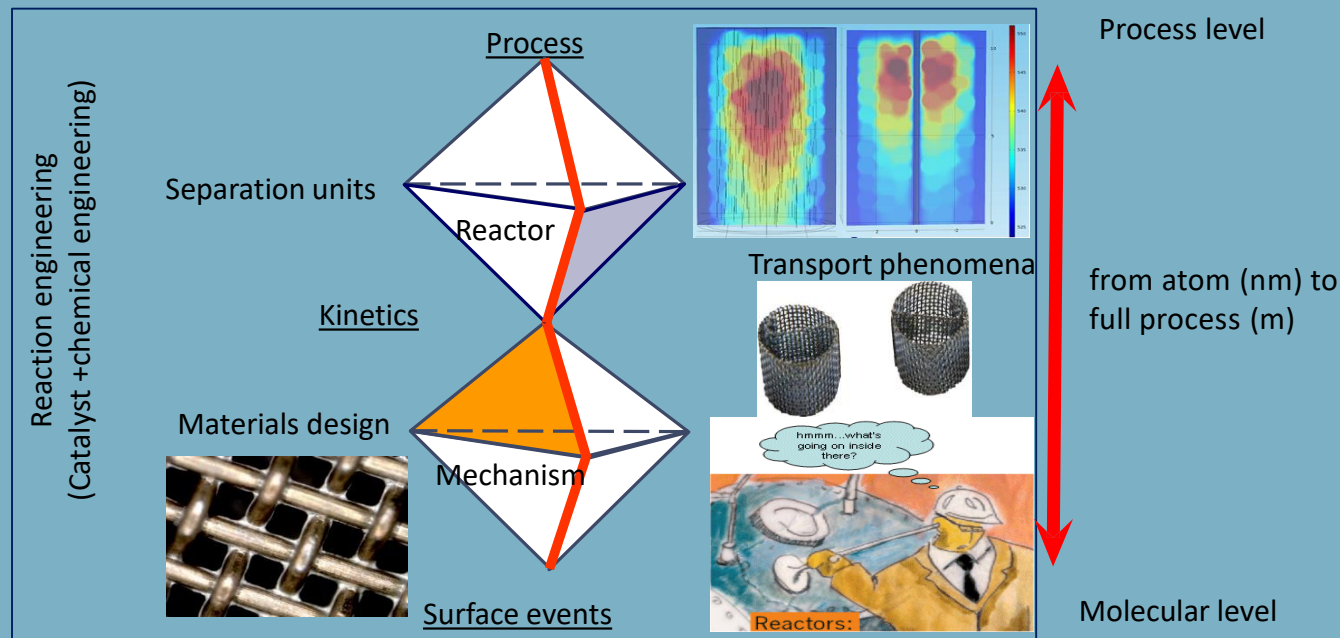




Synergistic Energy–Process Integration for Catalytic Reactor Intensification



Dr Farid Aiouache

Catalyst-chemical engineering approaches for catalytic reactors

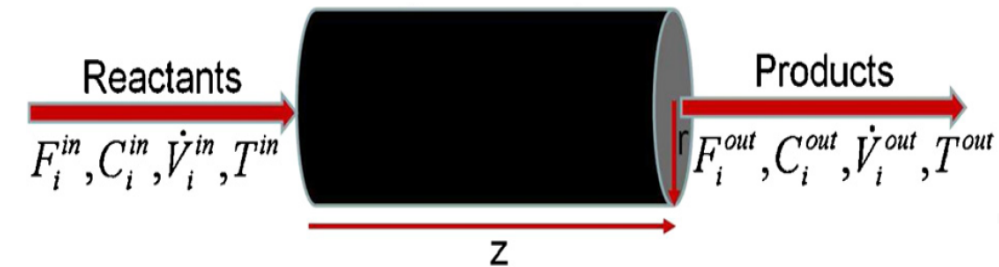
Petersen has commented

- **Engineering Challenge**

Traditional reactor design often relies on oversized approximations, leading to suboptimal performance and excessive capital expenditure.

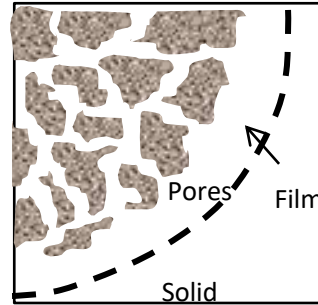
- **Critical Trade-offs**

Balancing chemical event complexity, mechanistic insight depth, computational time requirements, and economic constraints remains central to reactor engineering.

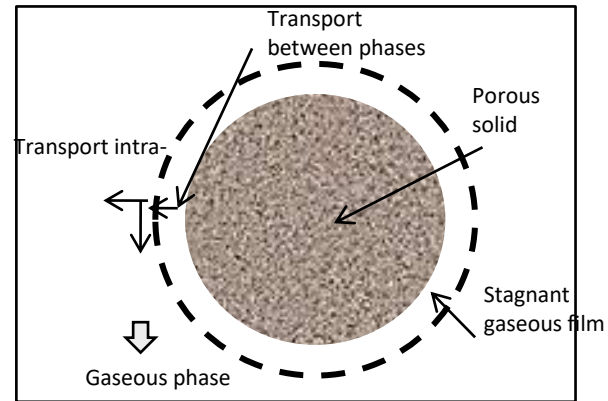


Multiscale Time-Space Context

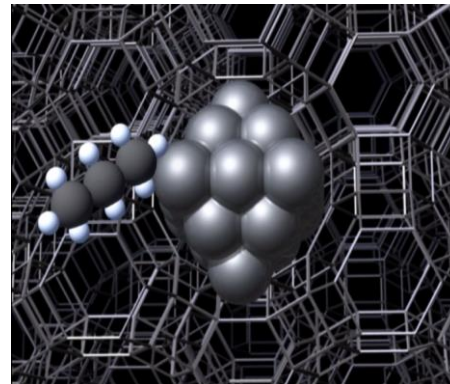
- Inter-particle Level (I)



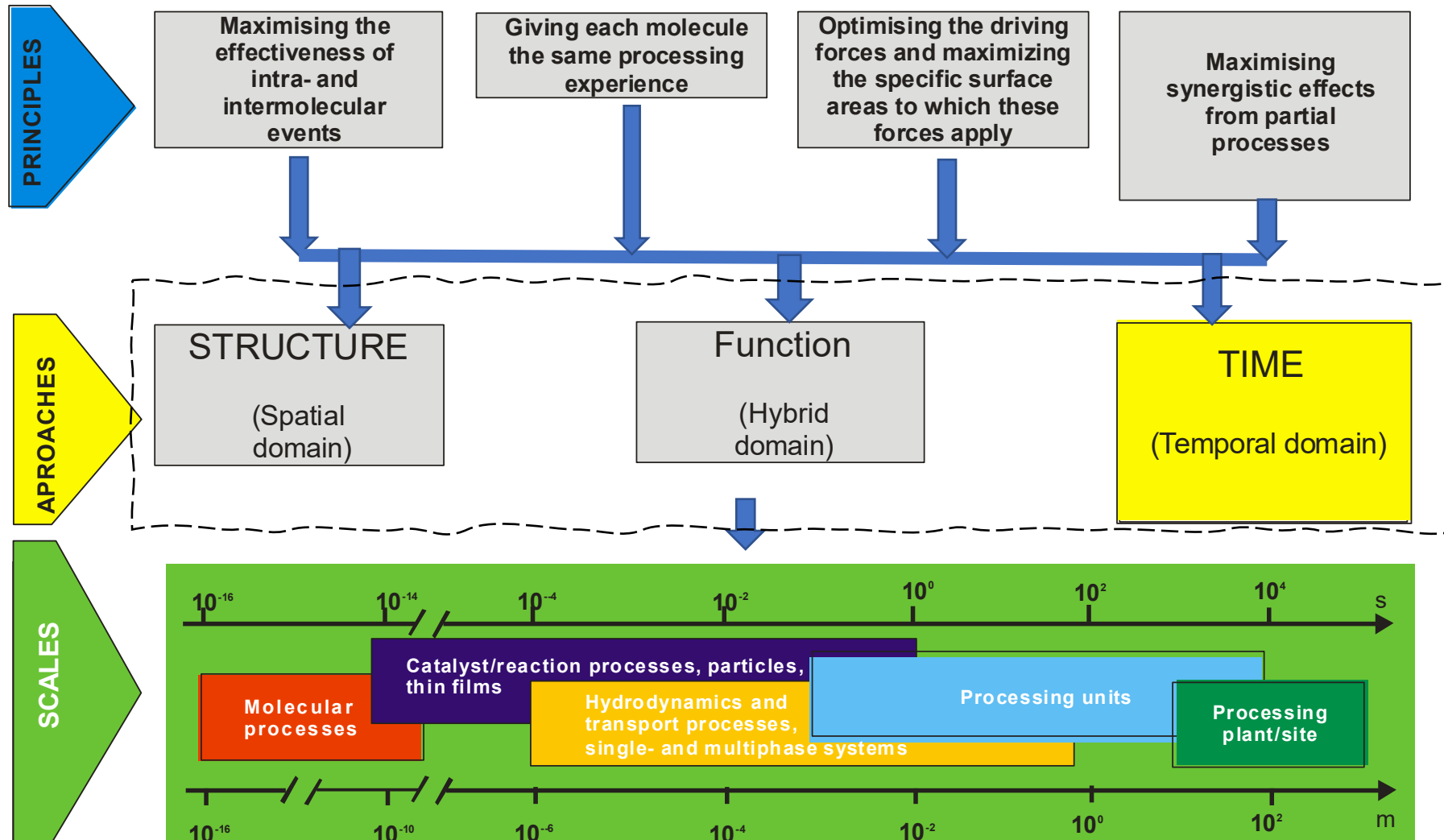
- Inter-phase Level (II)



- Catalyst/Cell Level (III)



Intensification approaches of Catalyst-Reaction engineering

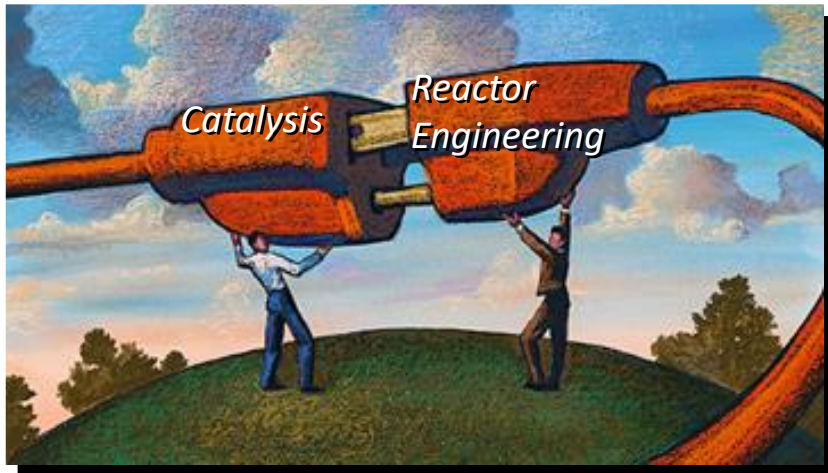


The effective chemical reactor20XX



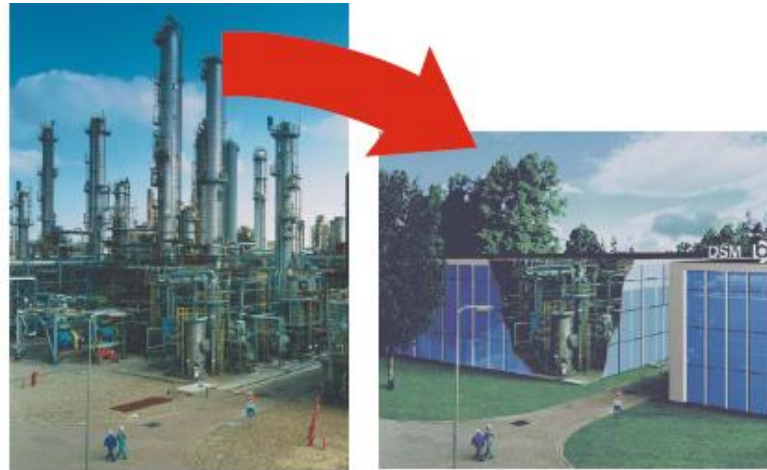
Goals

- Integrated
- Compact
- Run with alternative resources



Actions

- Maximum specific surface area
- Minimum energy and material expenses,
- Smaller equipment
- Ease of operation and scale-up

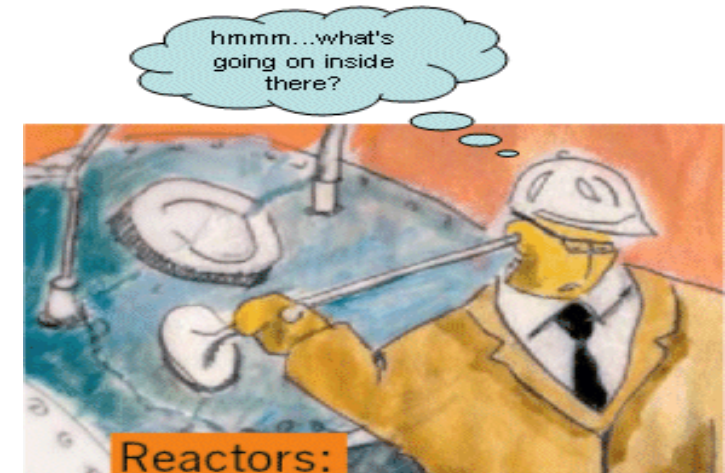


Today

??

Challenges

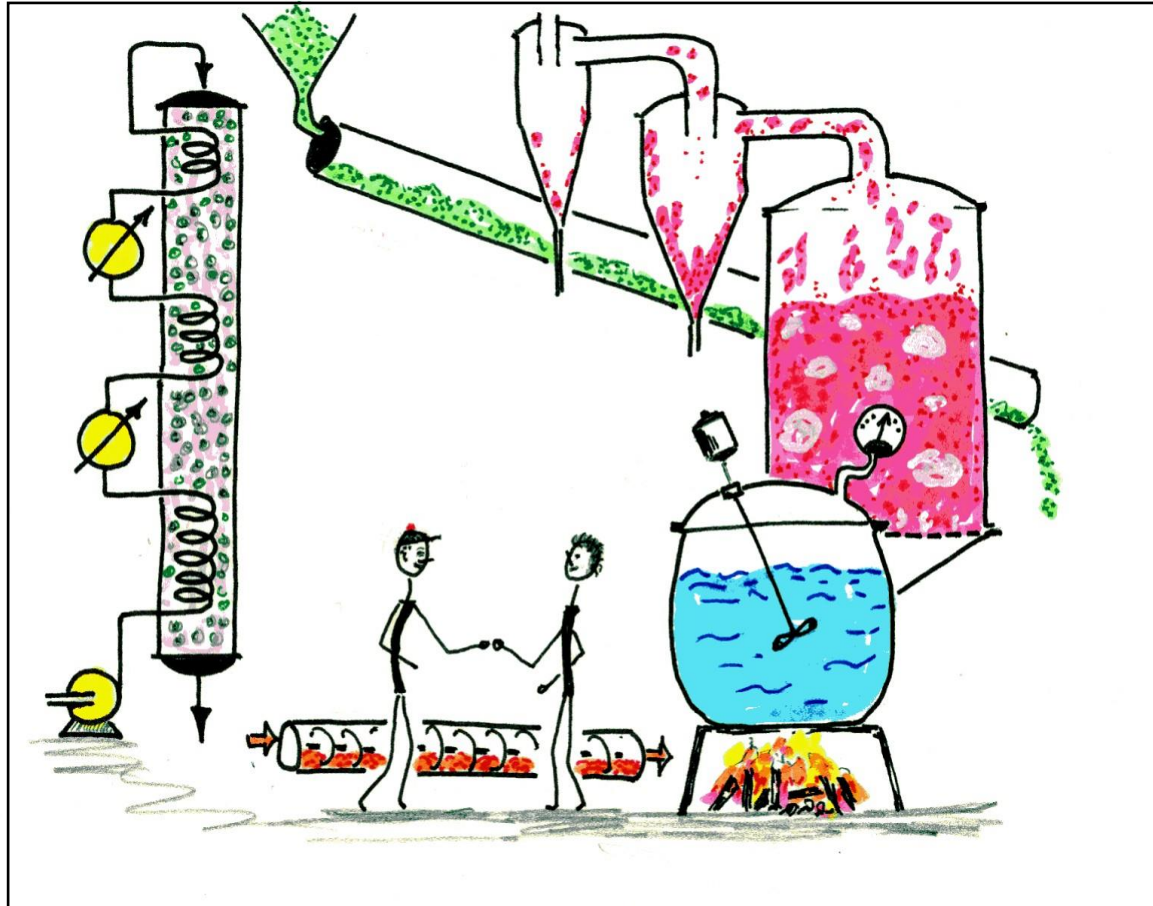
- Predictability & control,
- Understanding and exactness of mathematical descriptions (models)
- Use of AI/ML vs. data scarcity, poor generalisability, and immature frameworks



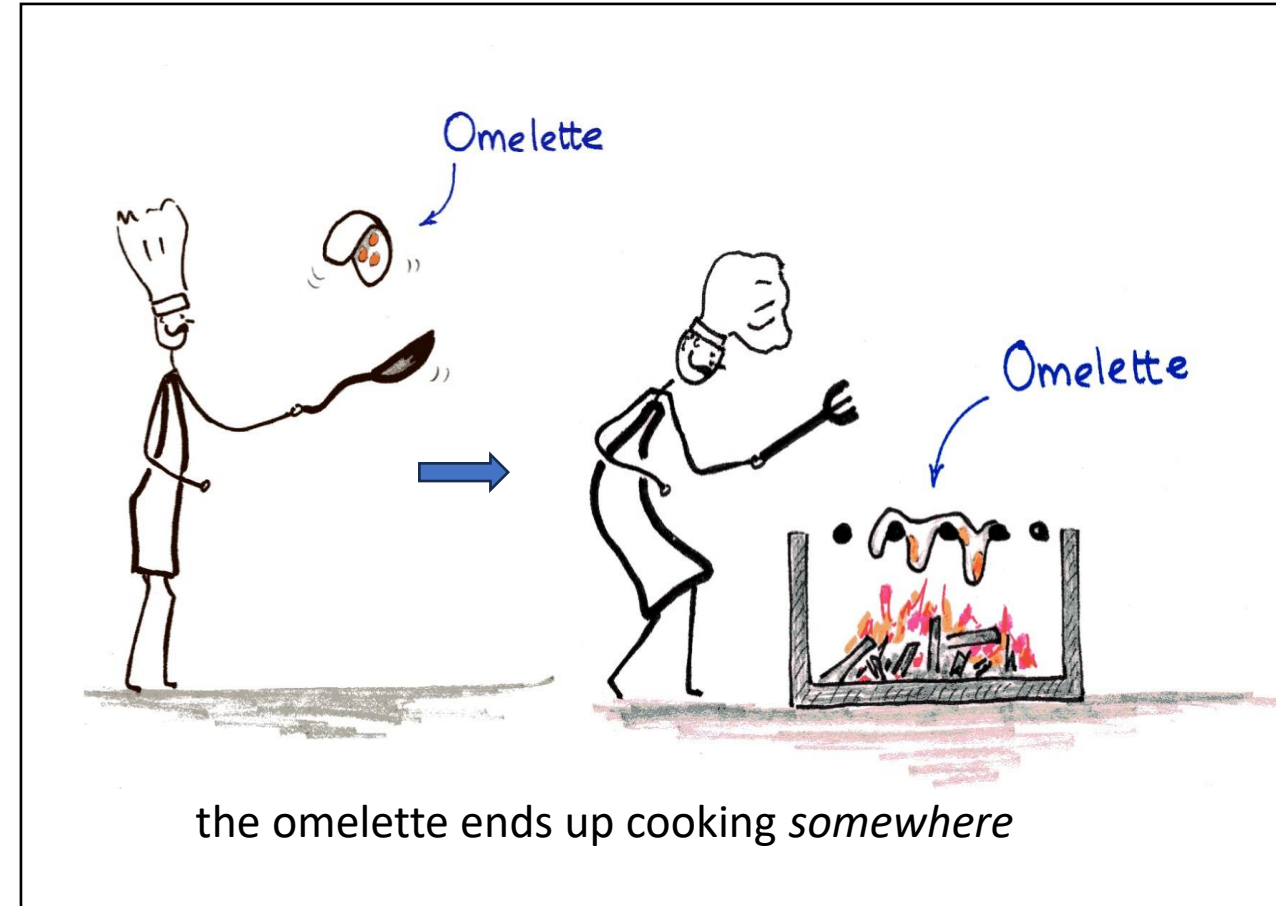
Next-generation reactor systems will seamlessly integrate catalyst design, reaction engineering, and process control to achieve unprecedented **efficiency, selectivity, and sustainability**.

Two rules of thumb

Rule 1. **Treat your reactors well**;understand their behaviour patterns, they become significantly more manageable



Rule 2. **Understand how the system behaves** for a change...



Multiscale Time-Space-function

1. Time-Domain Intensification (Oxidation/PROX of CO)

- SpaciMS
- **Diffused optical tomography**

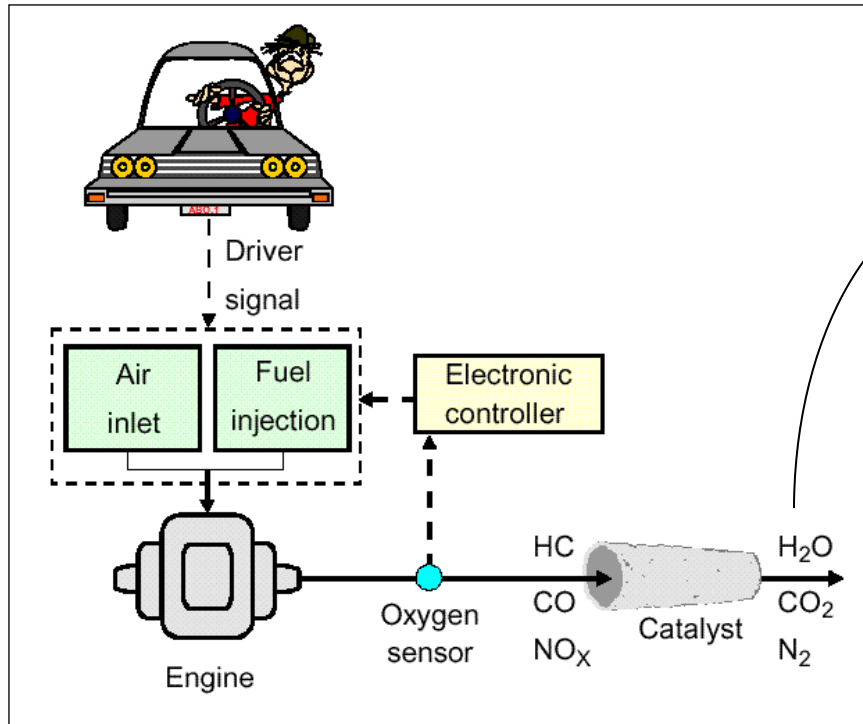
2. Function- Domain intensification

- HDO and H₂O in the hydrogen isotopic exchange reaction
- Waste water detritiation processing

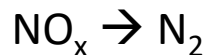
3. Structure- Domain intensification

- DOC removal from potable water by nanomagnetic composites
- **Photocatalytic degradation of phenol in a rotating disk reactor**

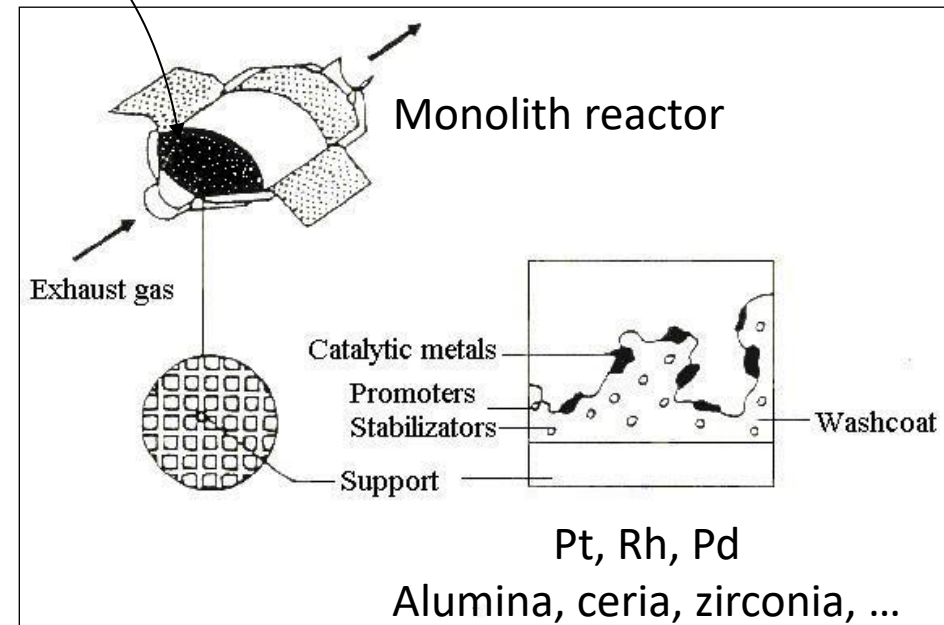
Automotive Emissions Control System



“Three-way” Catalyst



- Most widely deployed heterogeneous catalyst in the world – you probably own one!

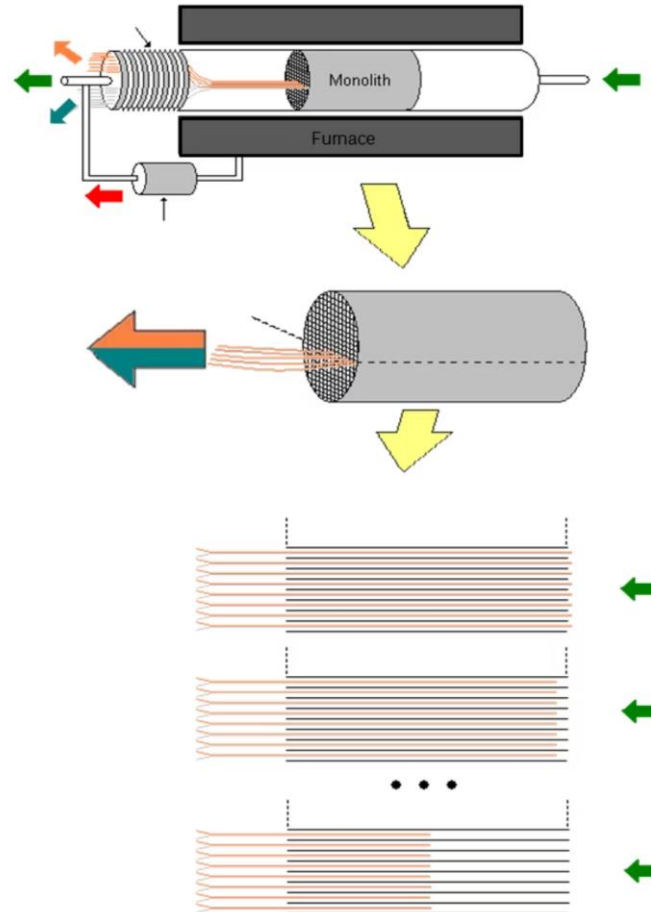


SpaciMS (Spatial Mass Spectrometry) enables real-time, spatially resolved analysis of gas-phase reactions and temperature profiles within operating catalytic reactors

Time domain intensification

SpaciMS (Spatial mass spectrometry)

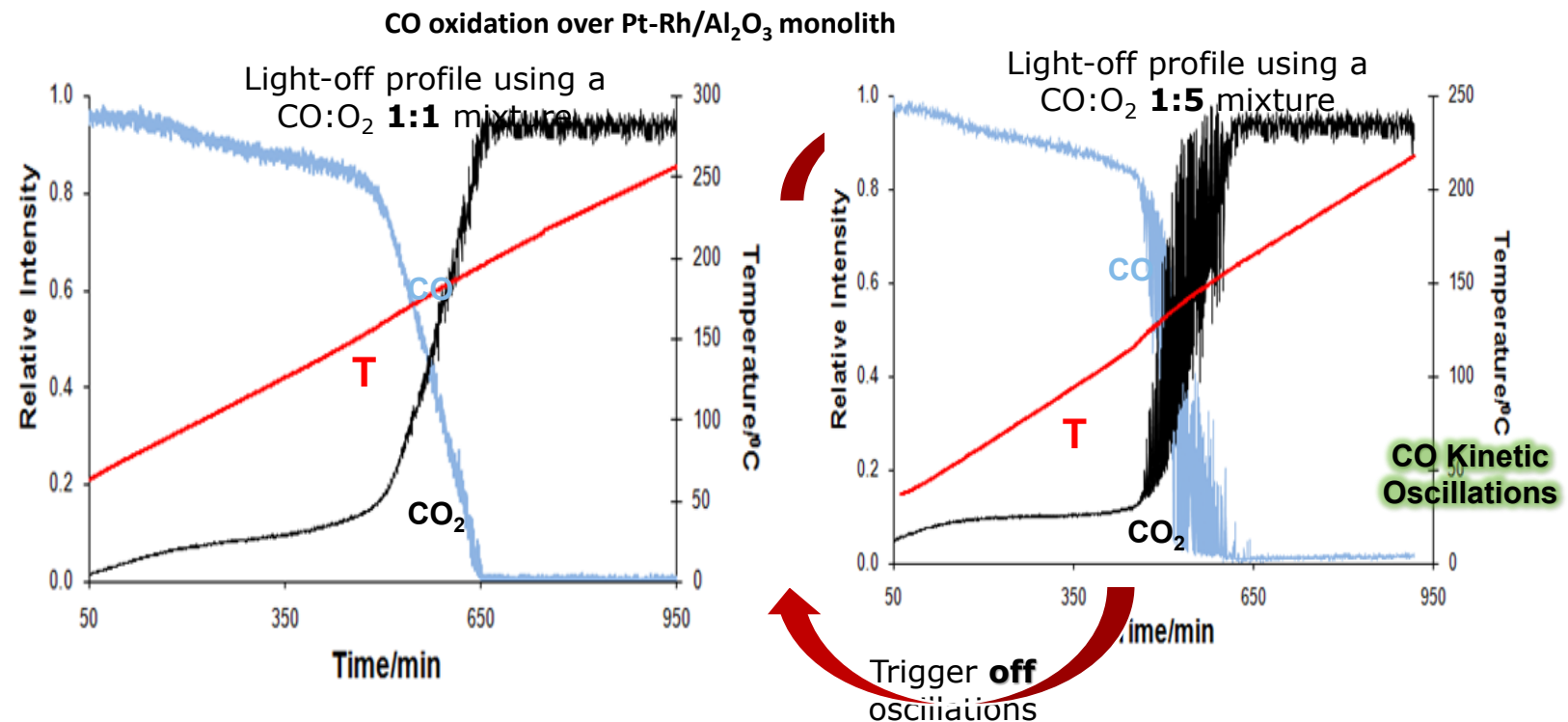
- 3D representation of the Spatial Resolution Set-up
- Tracing locations of reactions



Time domain intensification

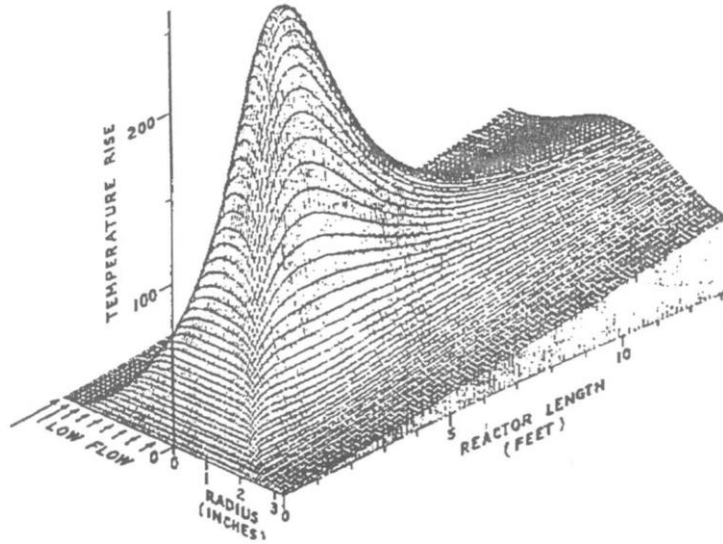
- **SpaciMS**: axial and radial information about chemical species and temperature during CO oxidation

- Probing what is hidden within:
ex. CO oscillations during the oxidation
- Axial and radial information about chemical species and temperature in a reactor
- Commercialised by Hiden Ltd.



**Tuning oscillations
amplitude and periodicity**

Flow Maldistribution and Hot Spot Formation in Packed Bed Reactors



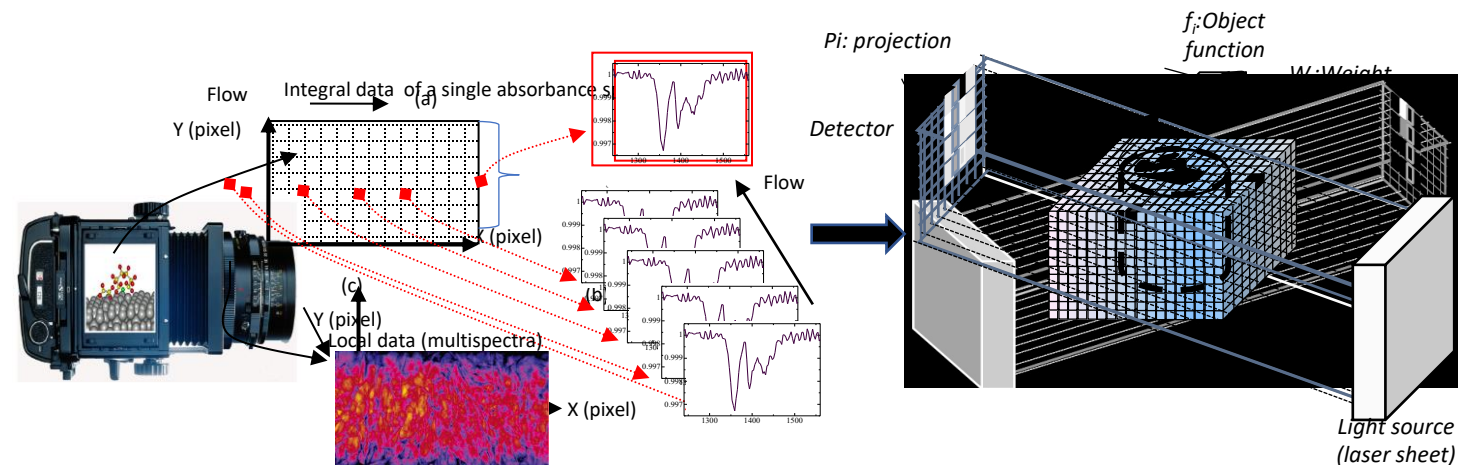
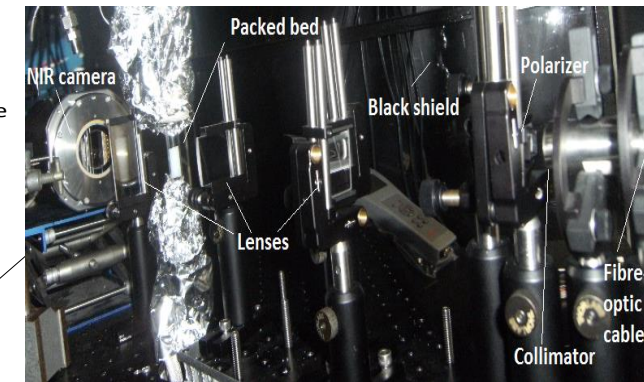
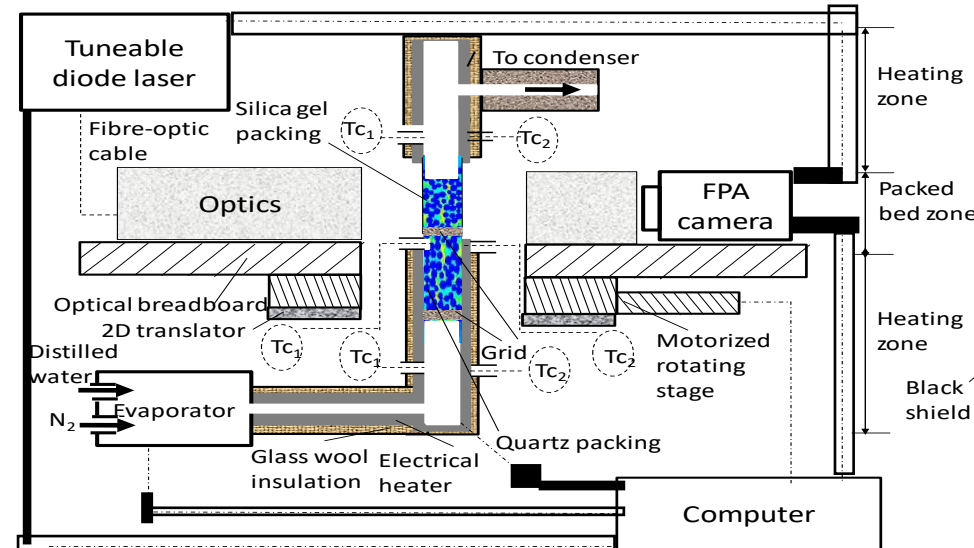
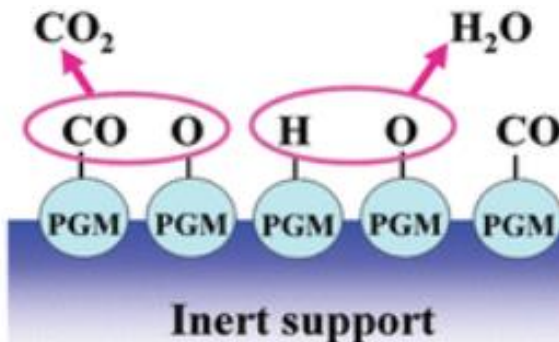
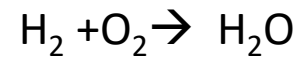
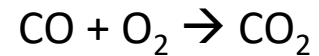
- Localised regions experience reduced flow rates, creating conditions hot spots and accelerated catalyst deactivation.
- This phenomenon creates a self-reinforcing cycle in reduced **mass transfer resistance regions**

Reference: Mobil, Jaffe, Industrial & Engineering Chemistry, 1974

Time domain intensification by NIR diffused optical tomography

Deactivation in CO preferential oxidation (PROX)

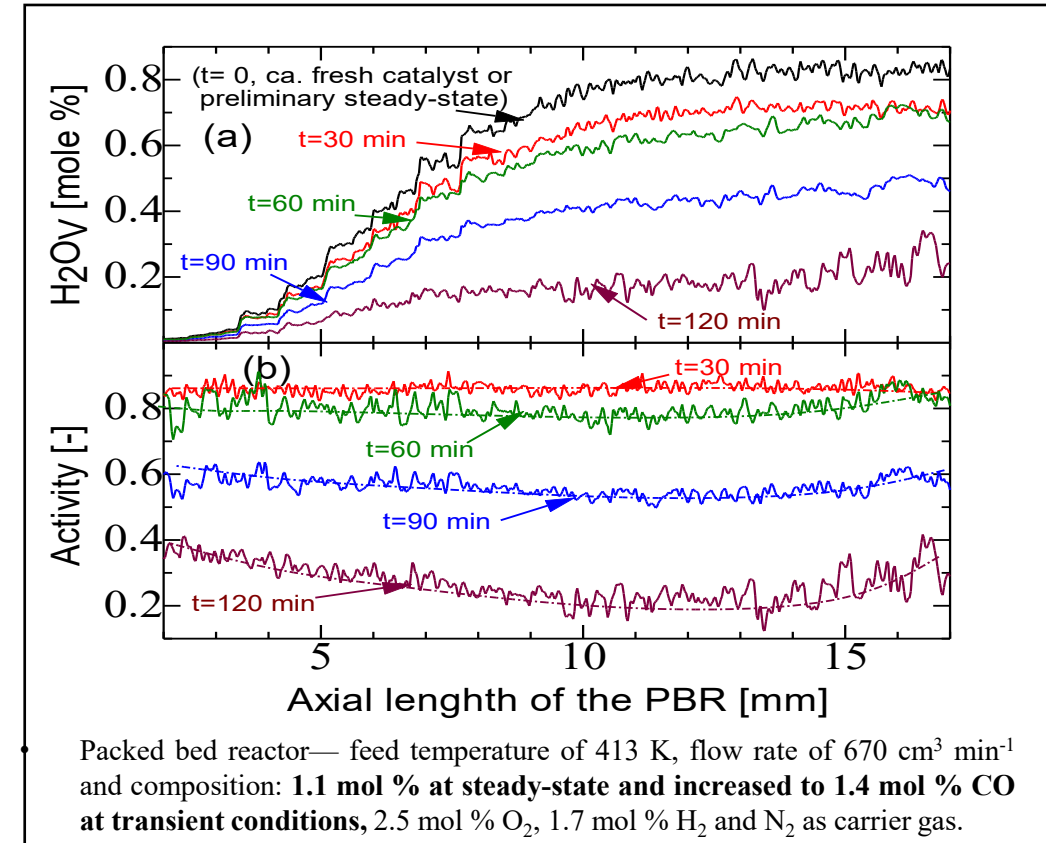
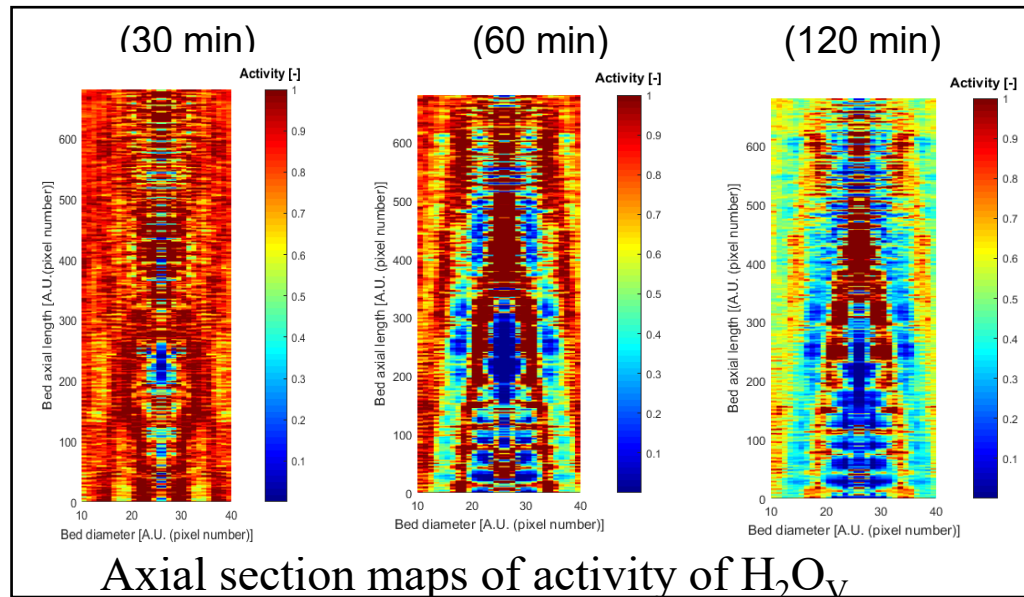
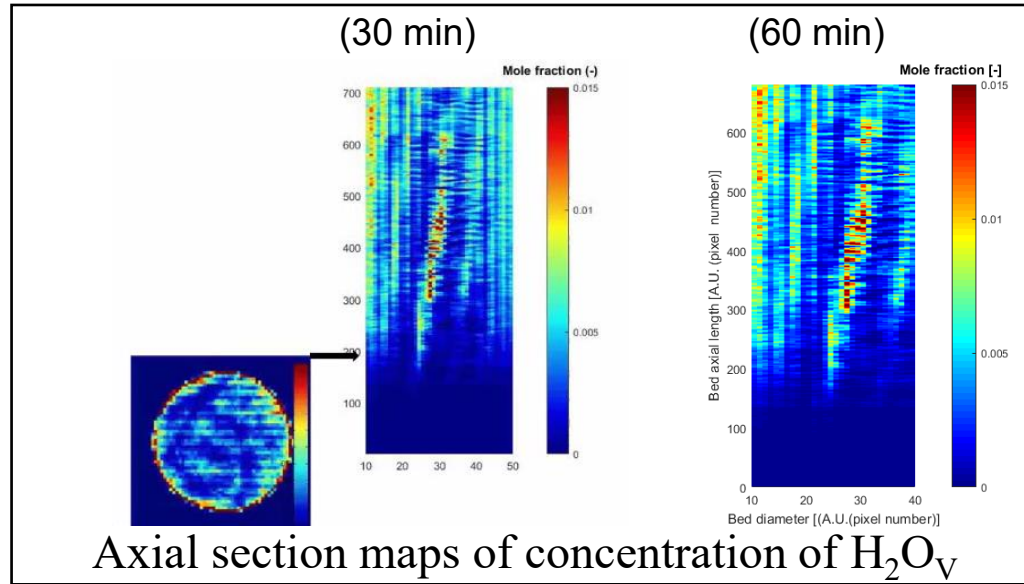
- PROX is for hydrogen purification for feeding the **fuel cells (1-10 ppm in PEM)**



Time domain intensification

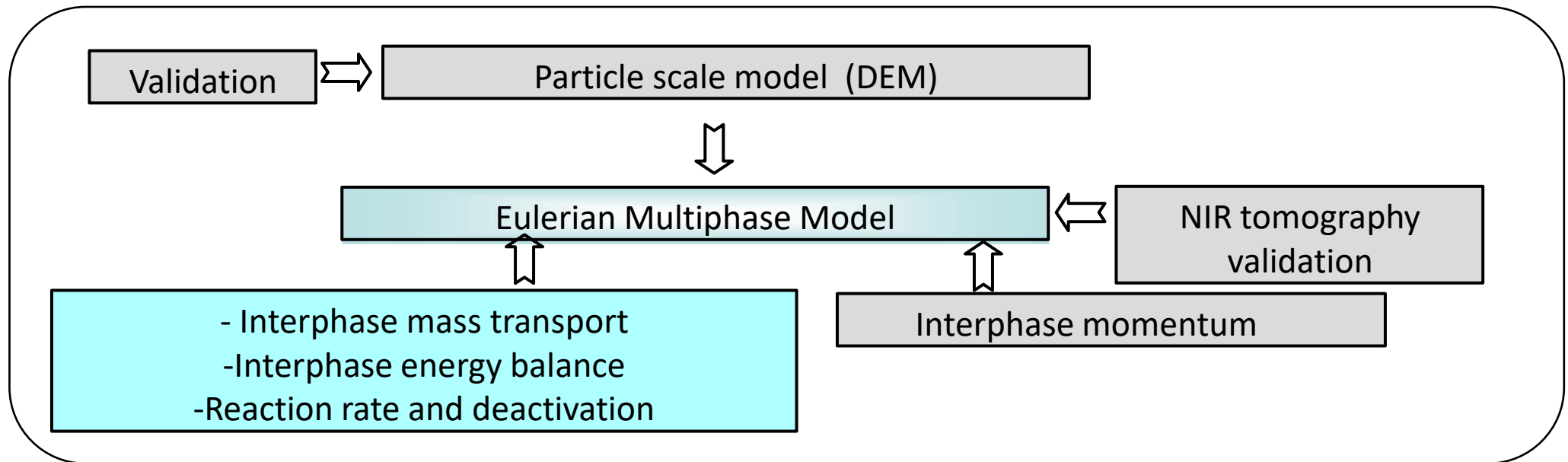


3D Imaging local deactivation in the PROX of CO by optical diffuse tomography



- CO adsorption is stronger than H₂
- CO oxidation is kinetically favoured
- O₂ feed is kept low to prevent H₂ oxidation
- Deactivation in highly convective zones

The 3D modelling framework couples four fundamental transport and reaction phenomena to predict local deactivation in packed-bed PROX reactors.





1. Momentum balance

$$\rho_g u \nabla u = -\nabla P + \mu \nabla \cdot \nabla u - \frac{2}{3} \mu \nabla \cdot \nabla u$$

$$\nabla \cdot (\rho_g u) = 0$$

$$u|_{\tau=0} = u_0, P|_{\tau=1} = P_0$$

2. Mass balance

2.1. in the gaseous phase

$$\frac{\partial c_i}{\partial t} + \nabla \cdot (-D_i \nabla c_i) + u \nabla c_i = 0$$

2.2. in the catalytic phase

$$\frac{\partial c_i}{\partial t} + \nabla \cdot (-D_{ie} \nabla c_i) = R_i$$

3. Heat balance in the gas phase

3.1. Heat balance in the gas phase

$$\rho_g C_{p_g} \frac{\partial T}{\partial t} + \rho_g C_{p_g} u \nabla T = \nabla (k \nabla T)$$

3.2. in the catalytic phase

$$\rho_g C_{p_s} \frac{\partial T}{\partial t} = \nabla (k_s \nabla T) + Q \quad Q = R \Delta H_R$$

4. Deactivation rate (determined experimentally)

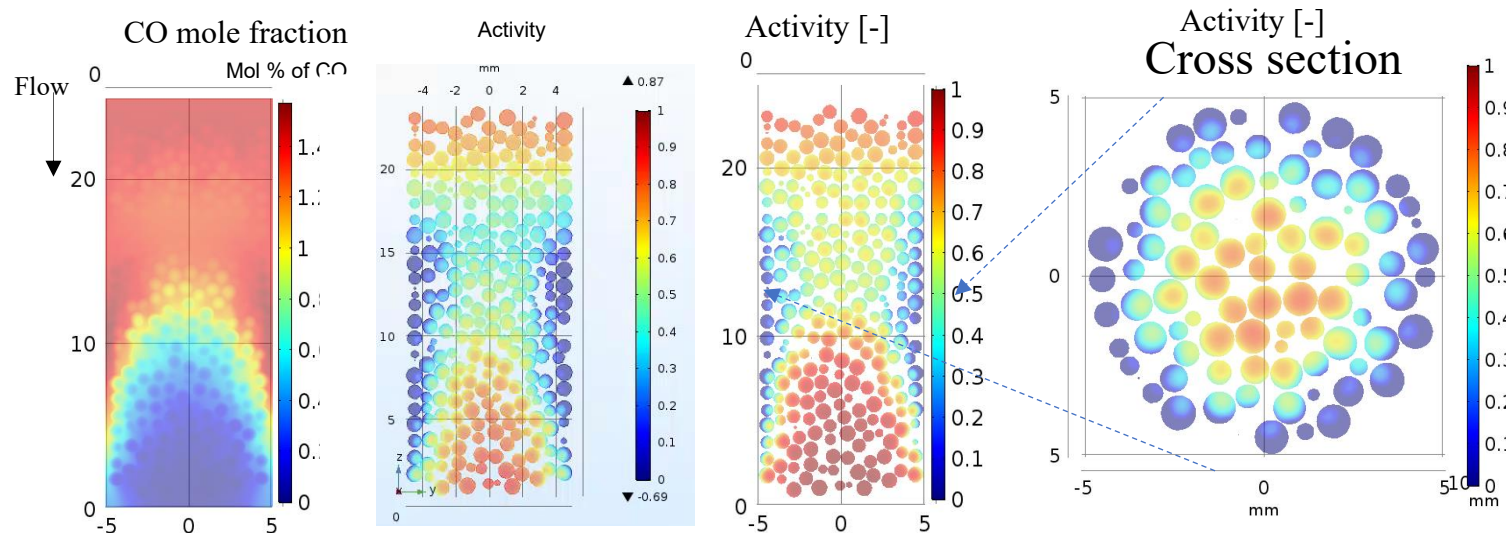
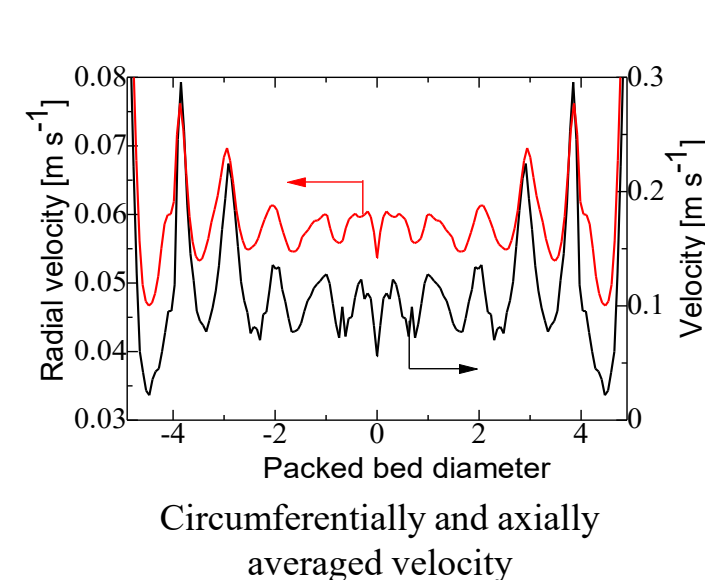
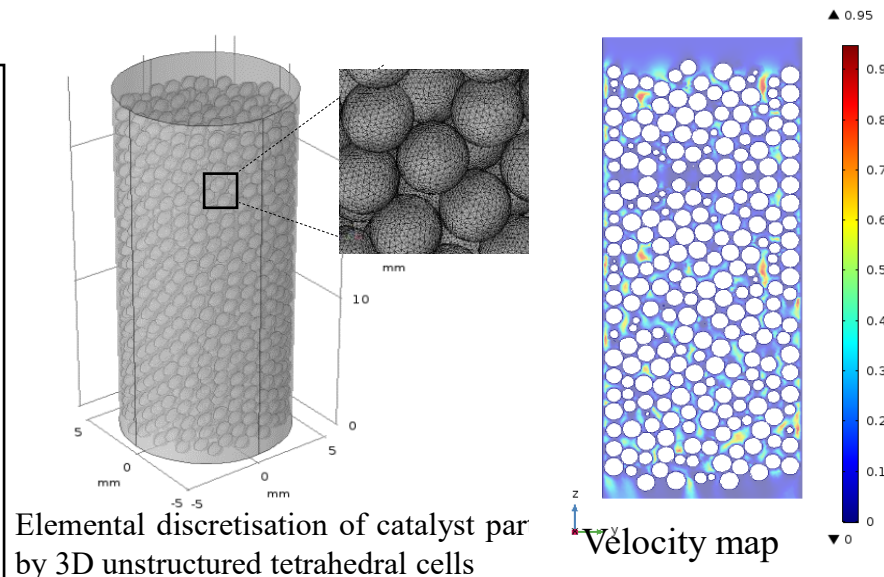
$$\frac{da}{dt} = A_D e^{\left(\frac{E_D}{RT}\right)} c_{CO}$$

$$R_i = a A e^{\left(\frac{E}{RT}\right)} c_{CO} \quad D_{ie} = \frac{\varepsilon_c D_i}{\tau_c} a$$

Time-Domain Intensification

3D NIR Imaging local deactivation of PROX

- **Flow rate:** 470 cm³/min with 1.4 mol% CO transient condition
- **CO concentration gradients:** Local accumulation in low-flow regions enhances deactivation
- **Activity distribution:** Circumferentially and axially averaged activity shows correlation with flow patterns



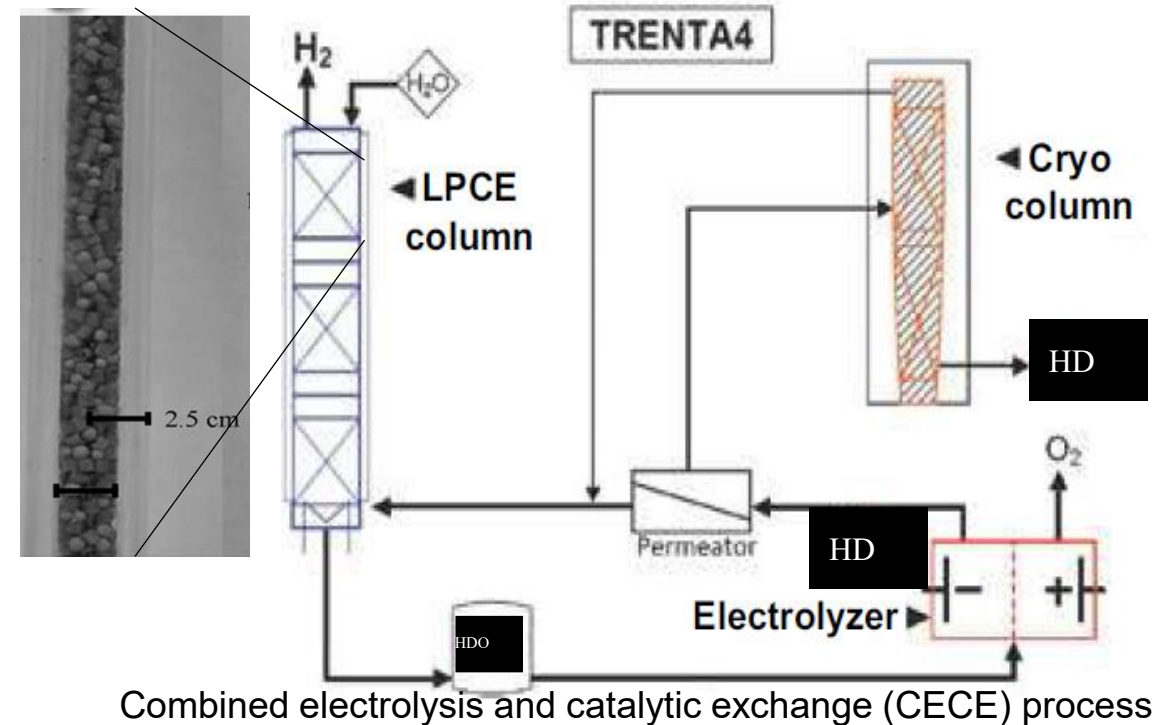
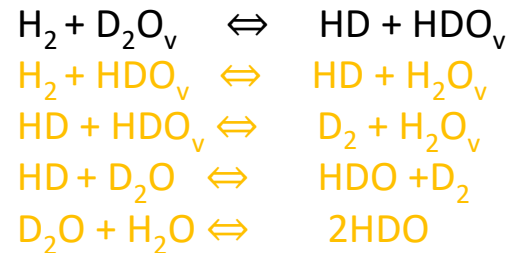
Packed bed reactor at 120 min of time-on-stream, flow rate of 470 cm³ min⁻¹ and composition: 1.1 mol % at steady-state and increased to 1.4 mol % CO at transient conditions along with deactivation, 1.7 mol % H₂ and N₂ as carrier gas

Functional Domain Intensification

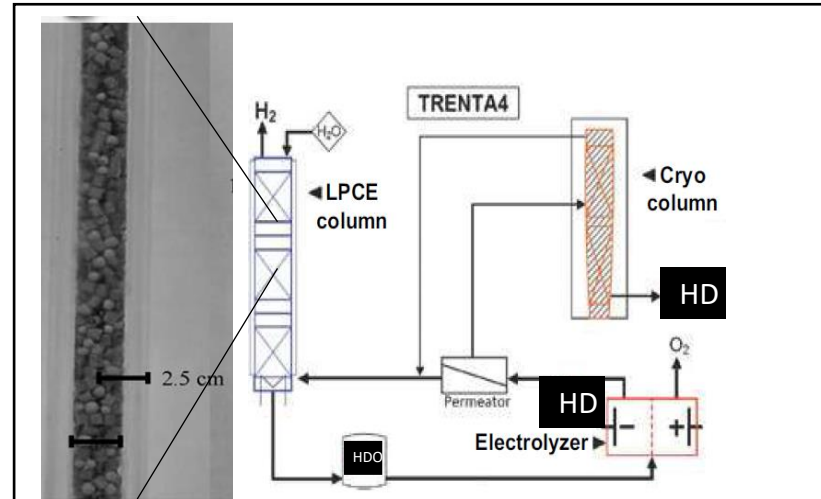
Spatial distributions of compositions and temperature of HDO and H₂O in the hydrogen isotopic exchange reaction

Process Significance

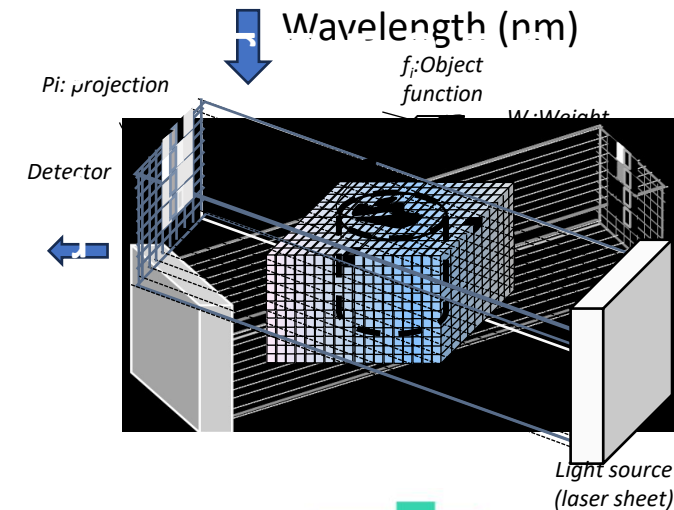
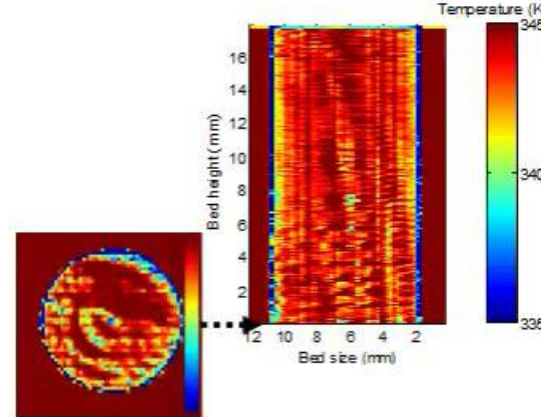
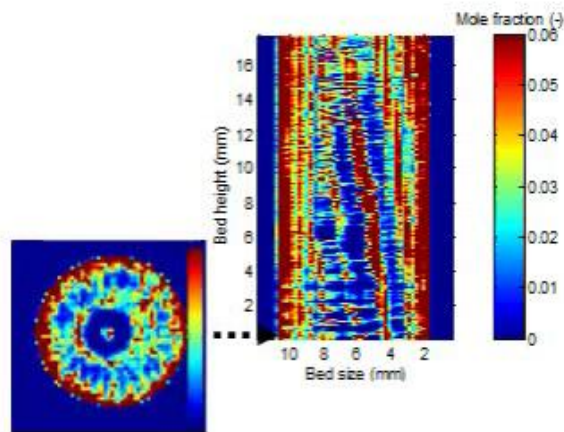
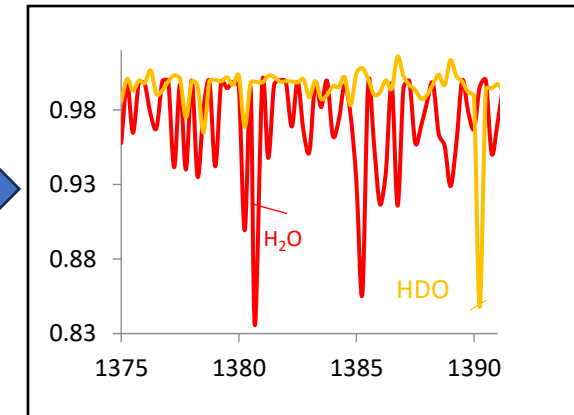
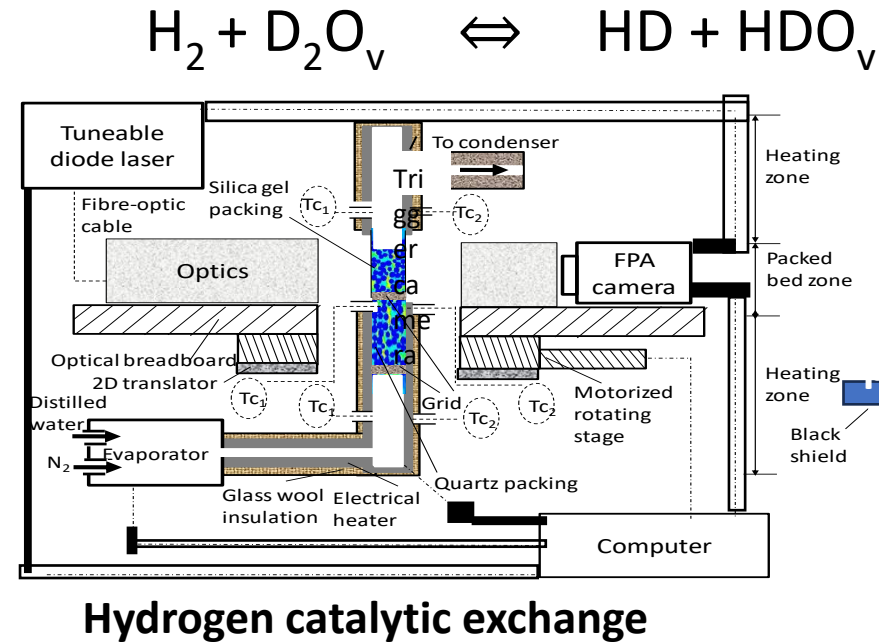
- Detritiation is critical for fusion reactor fuel cycles and managing radioactive waste from heavy water-moderated nuclear reactors.
- The hydrogen isotope exchange between HDO and H₂O enables tritium separation and recovery.



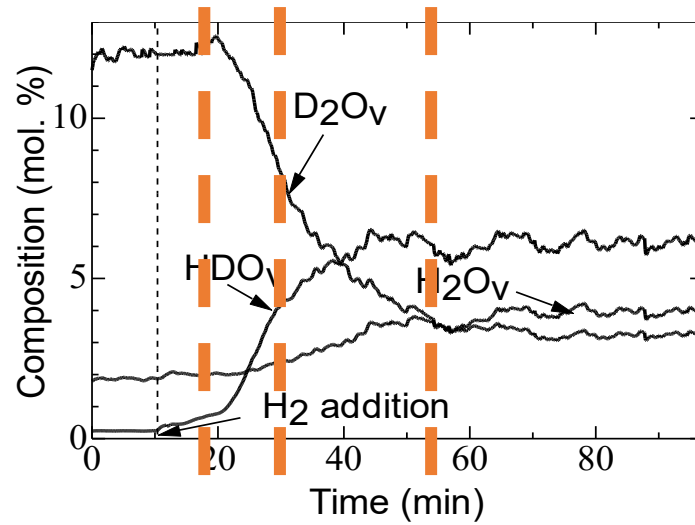
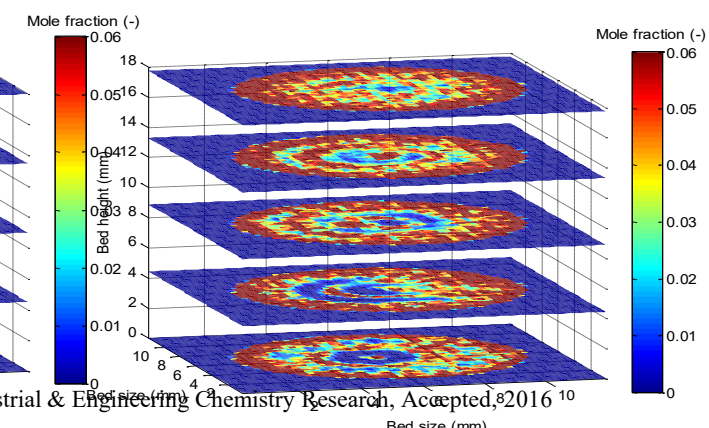
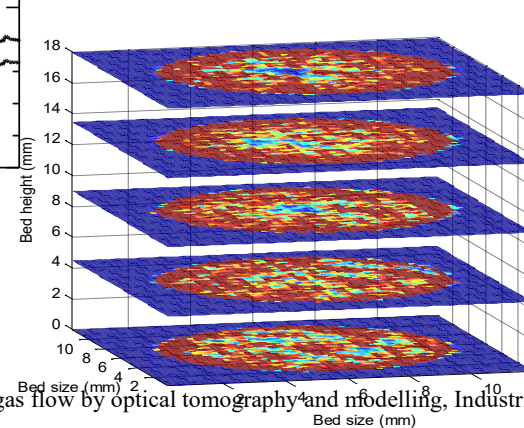
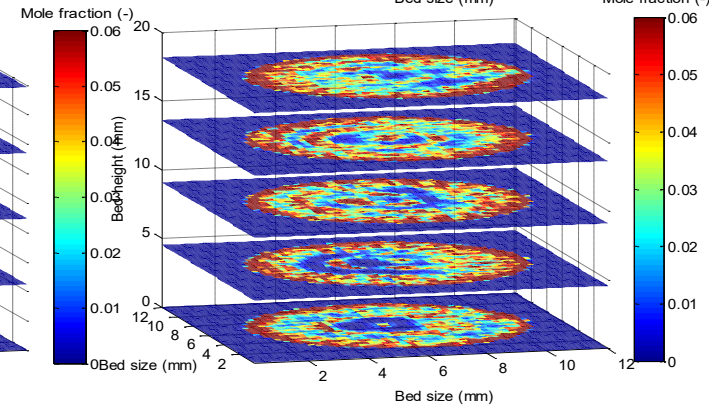
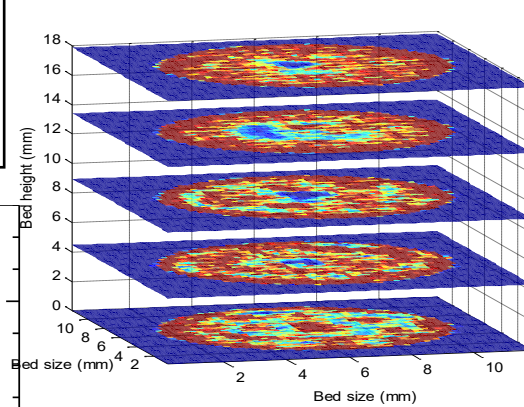
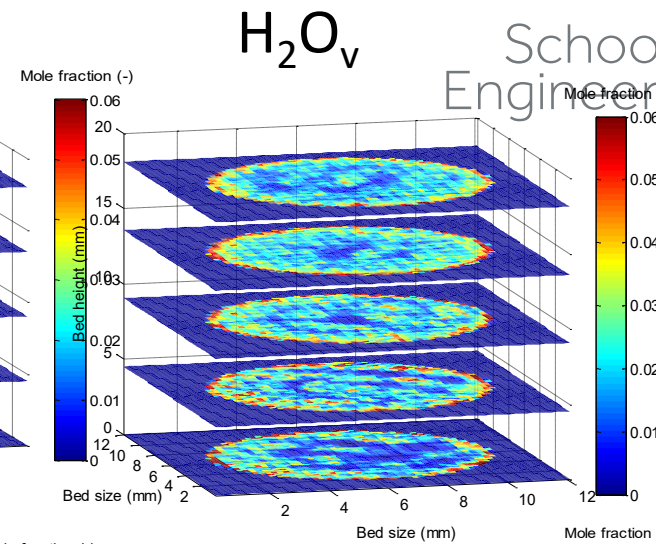
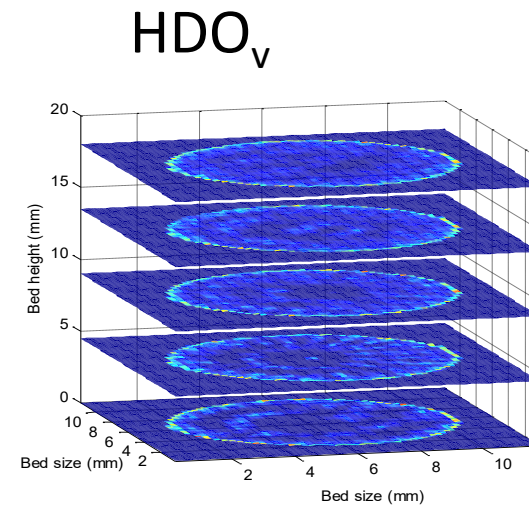
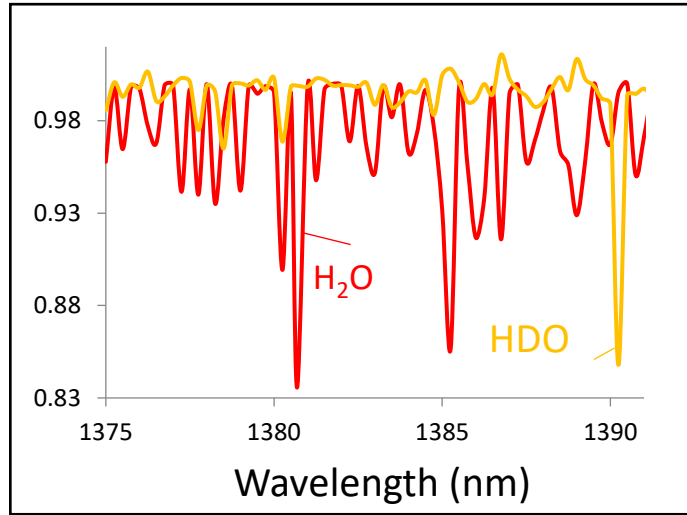
Spatial distributions of compositions and temperature in the isotopic exchange column by laser optical spectroscopy



Combined electrolysis and catalytic exchange (CECE)



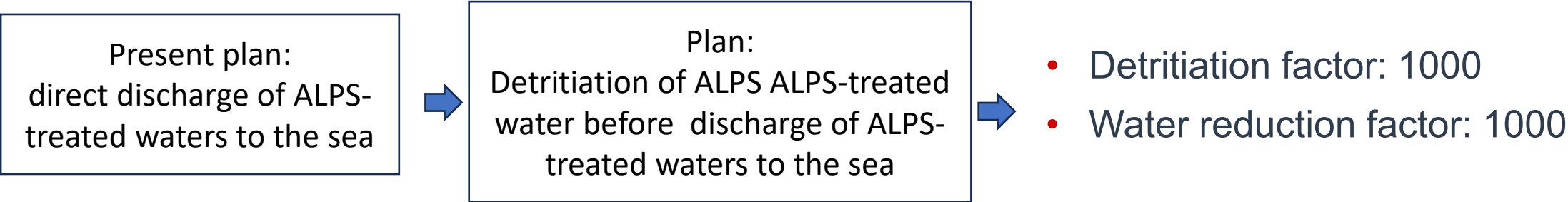
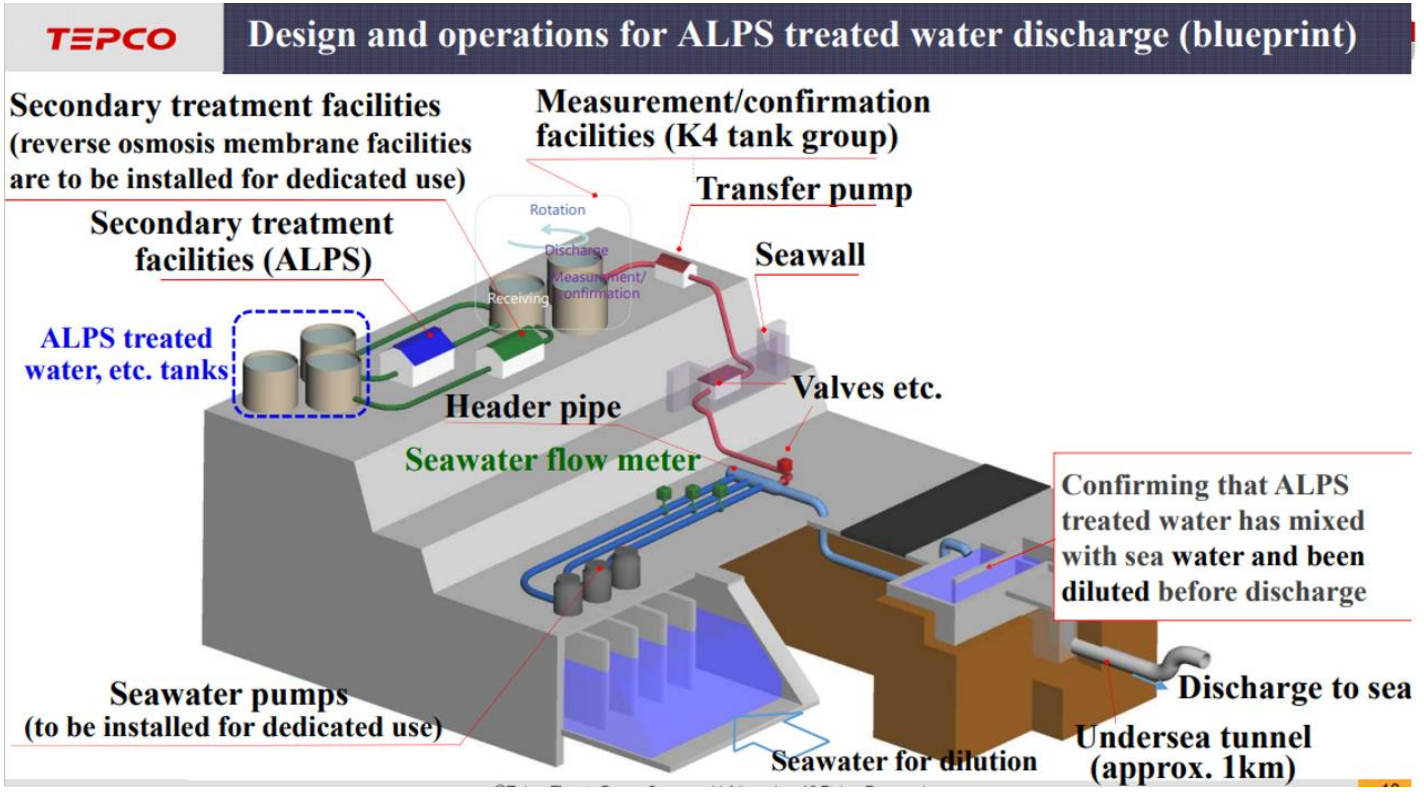
Dynamics of HDO_v , H_2O_v and D_2O_v compositions



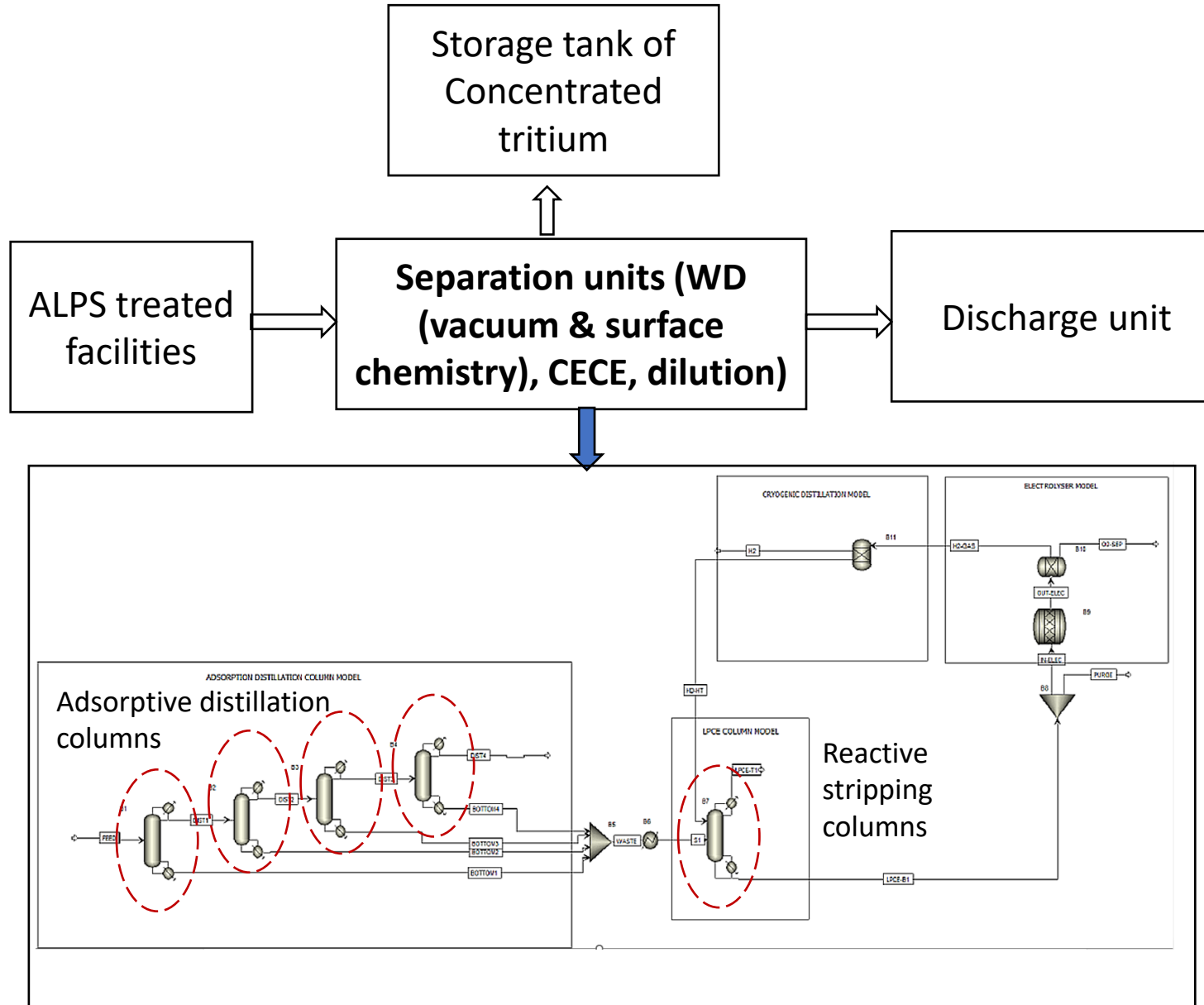
Packing height: 14 mm, particle size 0.7 mm (AR: 13), wall temperature: 333 K, D_2O_v (inlet): 12 mol %, H_2 (inlet): 25 mol. % and N_2 63 mol. %, N_2 flow rate: 250 cm³ min⁻¹

Water detritiation by combined electrolysis and catalytic exchange (CECE)

Water Storage Status	
Volume of water stored in tanks	About 1.31 million m ³ (as of early Sep. 2022)
Secured tank volume	About 1.37 million m ³ (more than 1,000 tanks)
Generation rate of water stored in tanks	About 130 m ³ /day (as of FY2021)



Detritiation, tritium storage and release project

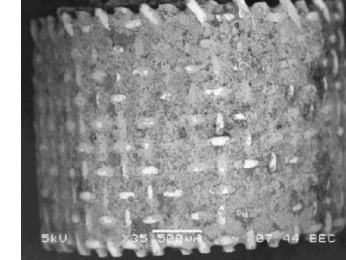
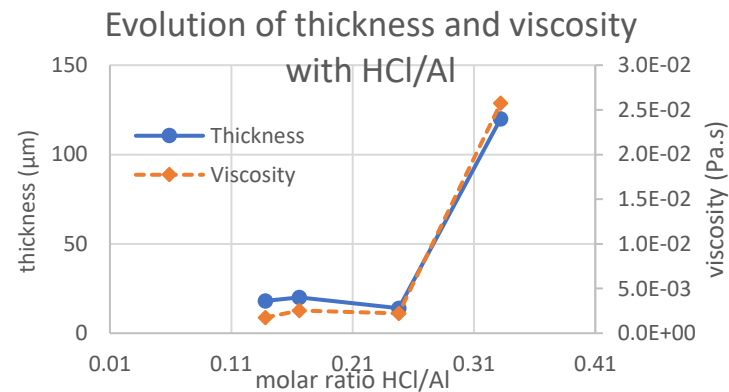
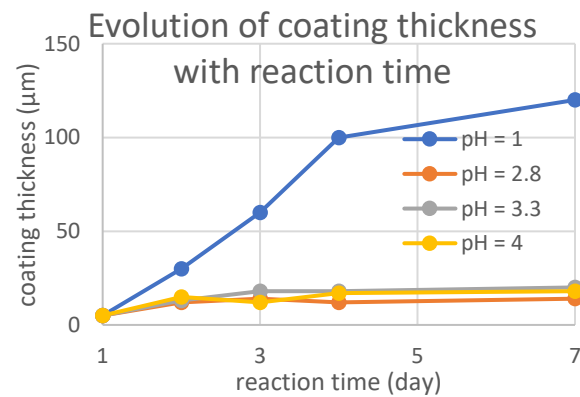


Adsorptive distillation as functional domain intensification

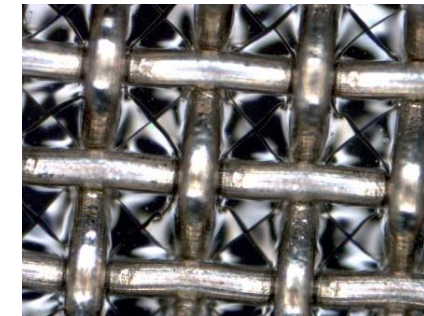
Alumina sol-gel coating of the packing as

- Reactive adsorber internals (function intensification)
- Hydrophobic Dixon ring as a static mixer (Space intensification)

- Hydrochloric acid (HCL)
- Sodium hydroxide solution (0.1 mol)
- 5% ethanol
- tetraethyl orthosilicate (TOSL),
- Alumina hydroxide (Al(OH)₃)

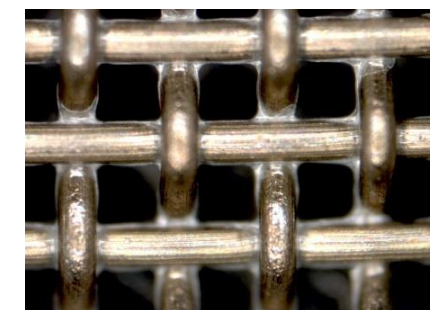


Dixon rings (E.D. Banúsa, O. eet al., Chem. Eng. J. 246 (2014) 353-365)



pH = 1

Sol-gel coating of Alumina hydroxide (pH, peptization and bender formulation) under controlled surface properties of stainless steel

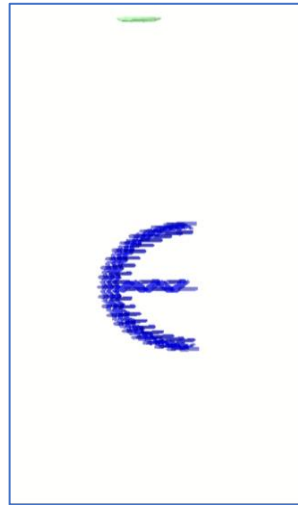


pH = 3.3

Adsorptive distillation as functional domain intensification



Wettability tests



Water flow pattern for the liquid velocity 0.5 (m/s) and **contact angle (Θ) equals to 75°**

Hydrophilic coating



Water flow pattern for the liquid velocity 0.5 (m/s) and **contact angle (Θ) equals to 120°**

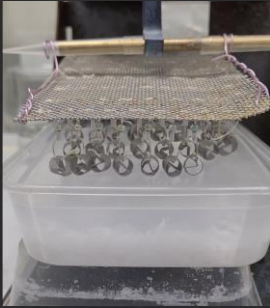
Hydrophobic coating

Functional domain intensification

Adsorptive distillation: HDO



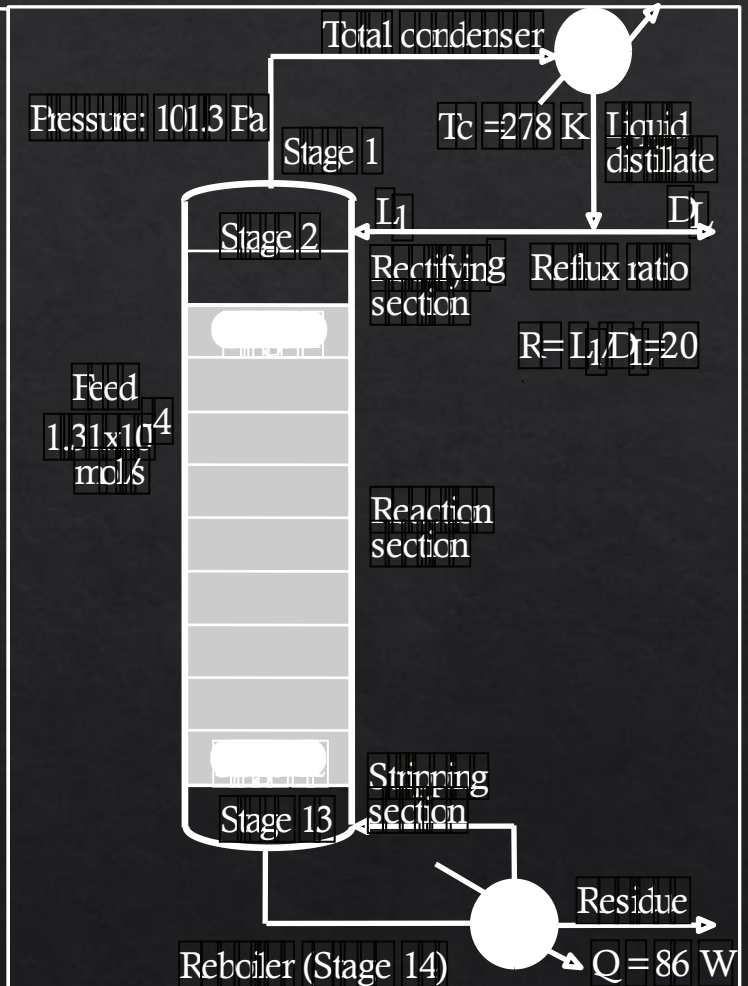
Dixon ring hook device



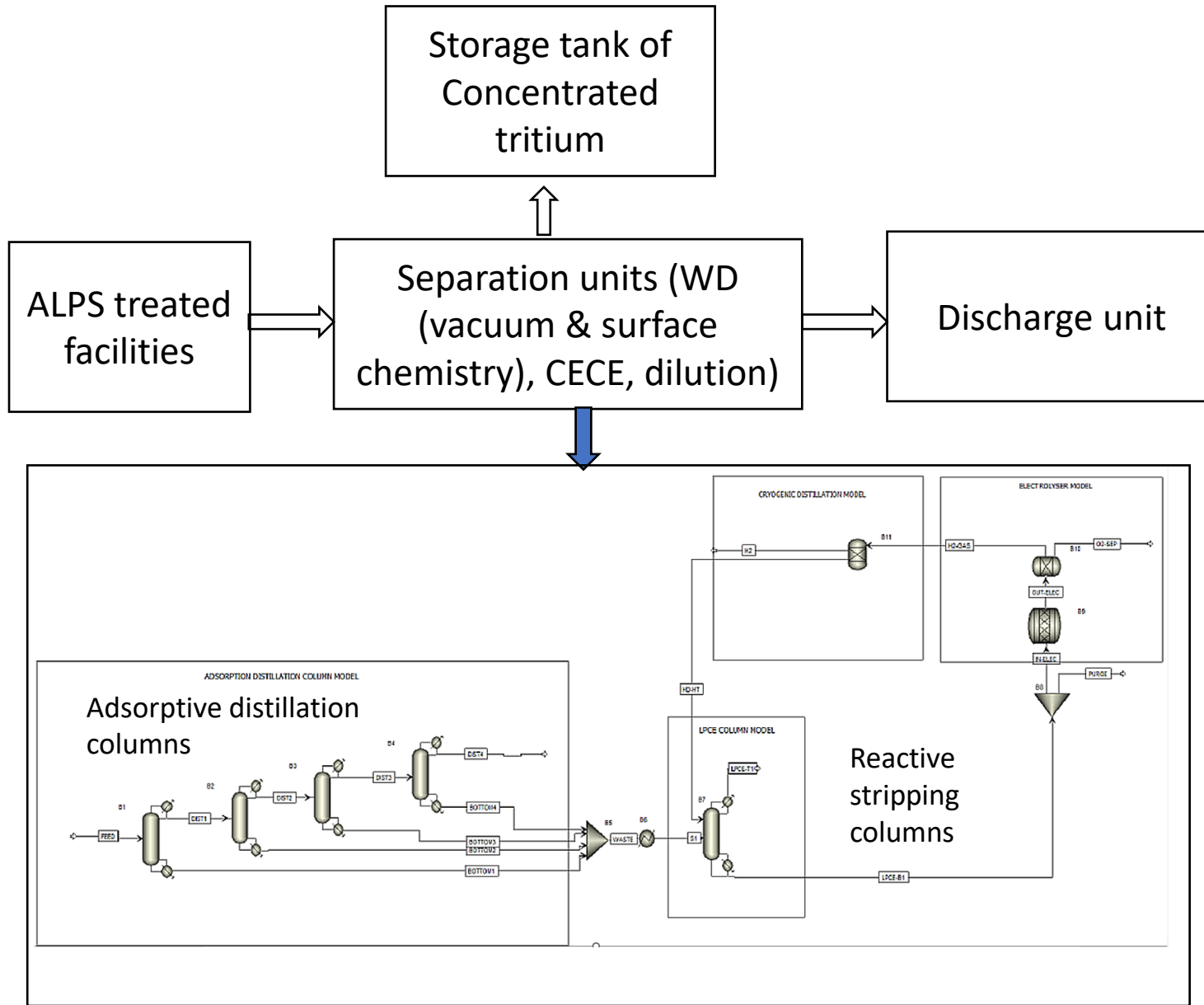
Coated Dixon ring



Standard condition	
Feed temperature [K]	298
Feed of D ₂ O [mol/s]	1.31×10^4
Total pressure [kPa]	101.3
Condenser	Total
Reboiler	Partial
Reflux ratio	20
Condenser temperature [K]	278
Reboiler heat duty [W]	86
Mass of catalyst [g]	5
Rectification section [cm]	12
Reactive section [cm]	32
Stripping section [cm]	6



Detritiation, tritium storage and release project



Stream	Concentration of HDO in Parts per million (PPM)
Feed uncoated	1244.472
Distillate uncoated	1233.349
Bottom uncoated	1353.406
Feed coated	1244.472
Distillate coated	1004.504
Bottom coated	1323.769

- Lab. Improved purification of **15.4 %**
- Simulation developed code by Aspen plus
- Estimation of missing physical properties of radioactive species (HDO, HTO, D₂, T₂, T₂O, D₂O, DTO)
- Four adsorptive distillation columns of **15 m** height, **1.2 m** in size
- Prediction of overall process performance :
A detritiation factor higher than **500**
Volume reduction over **85 %**
- Complete CAPEX/OPEX costing: JPY 1.48B / JPY 1.41B using Guthrie and Turton methods

Structure and functional domain intensification

Removal of DOC from potable water by nanomagnetic composites



Peat land areas

Source



Dissolved Organic
Carbon
(DOC)

Complex with Cl

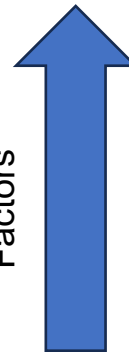


Disinfection by-
products (DBPs)



Trihalomethanes and
haloacetic
acids..(THM) Health
Issue

Factors



Climatic factors like
✓ Warmer temperatures

- ✓ Increased rainfall as well as
- ✓ Exposed and degraded peat

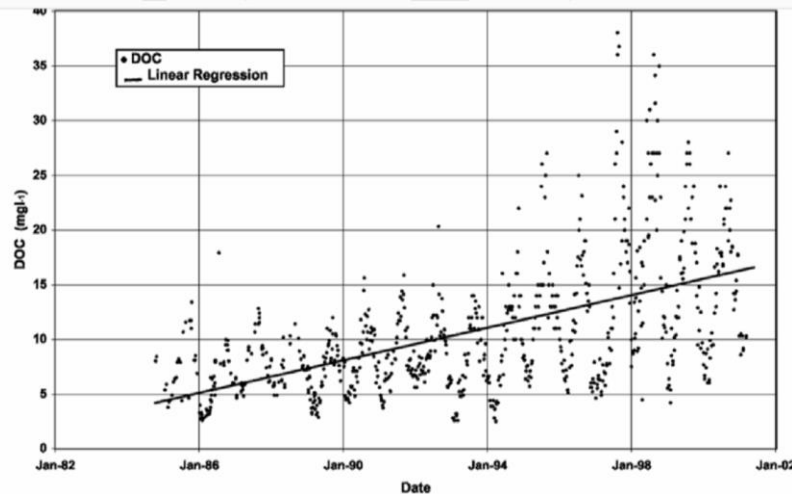
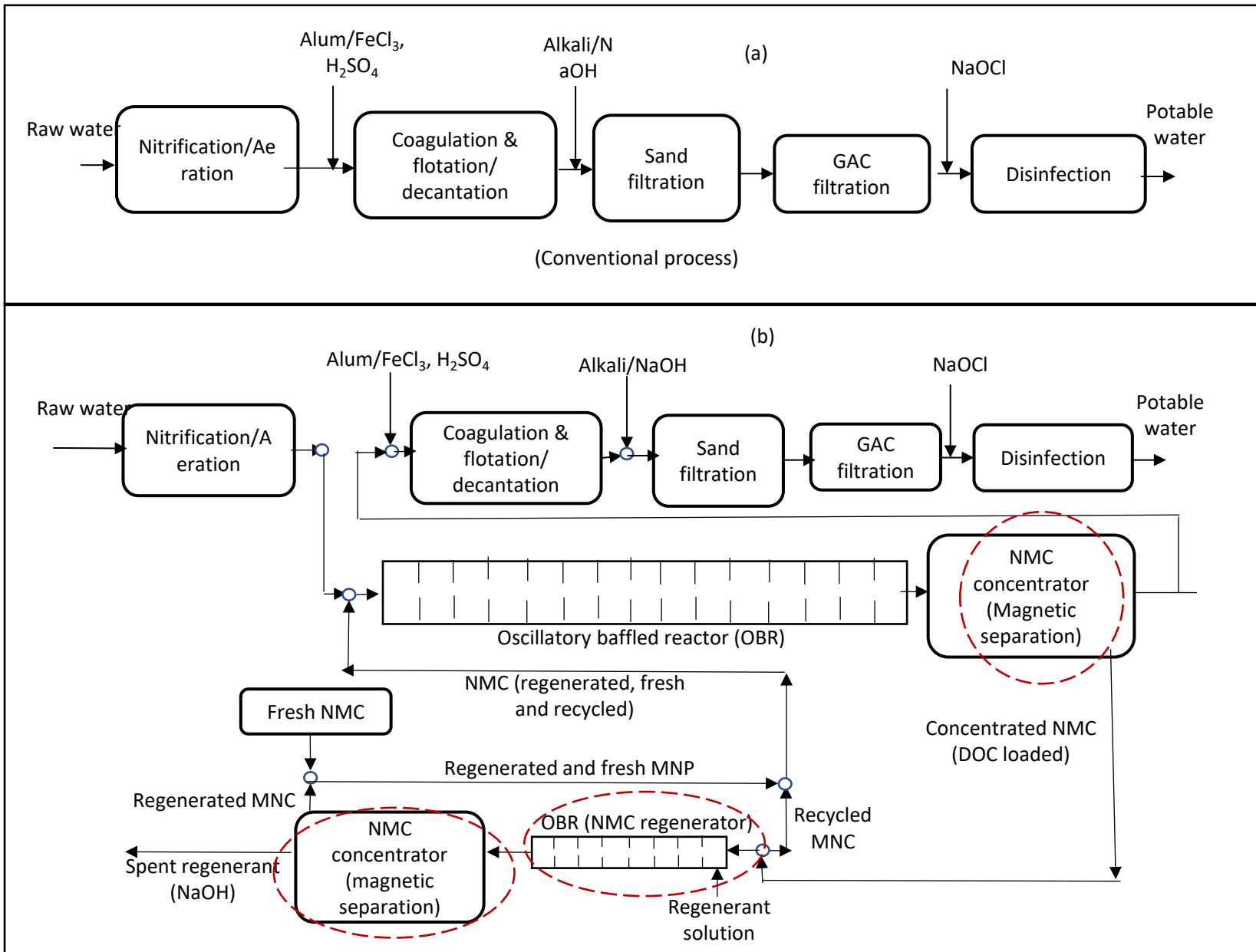


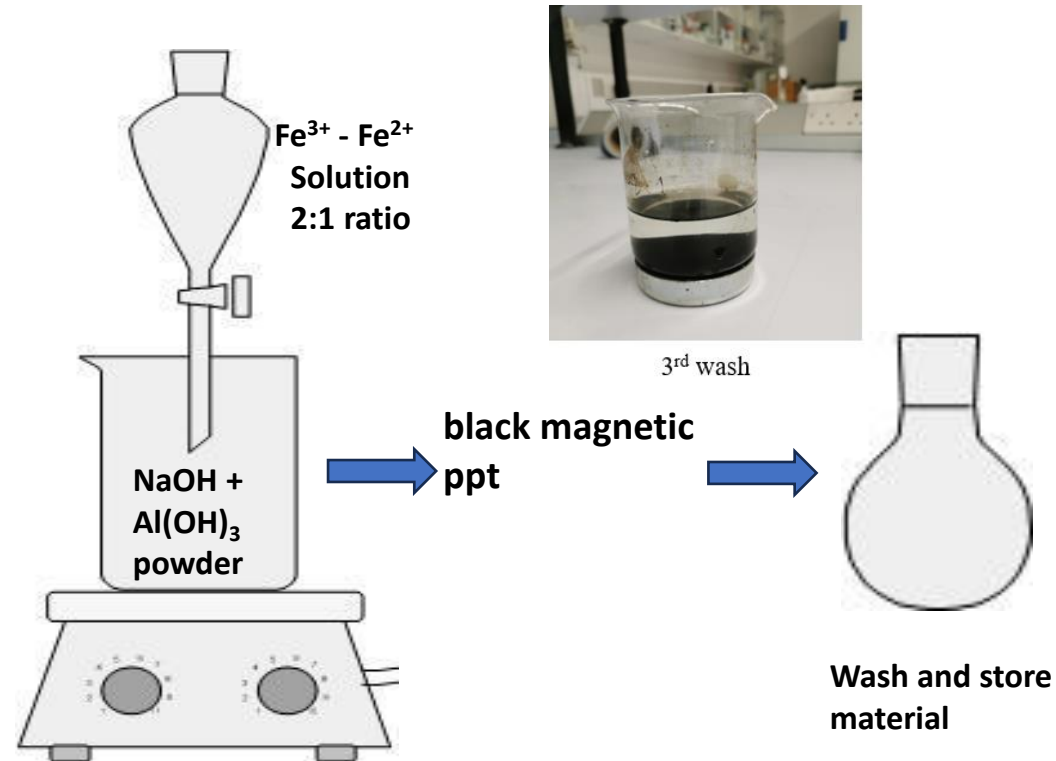
Figure 1 Trends in dissolved organic carbon in the Loch Ard Forest area (McCartney *et al.*, 2003)



Process flow diagram of drinking water treatment at WTW plant with COD removal (a) conventional coagulation/floatation (b) Combined NMC ion exchange and coagulation/floatation

Structure domain intensification

Batch synthesis of the nanomagnetic Composites



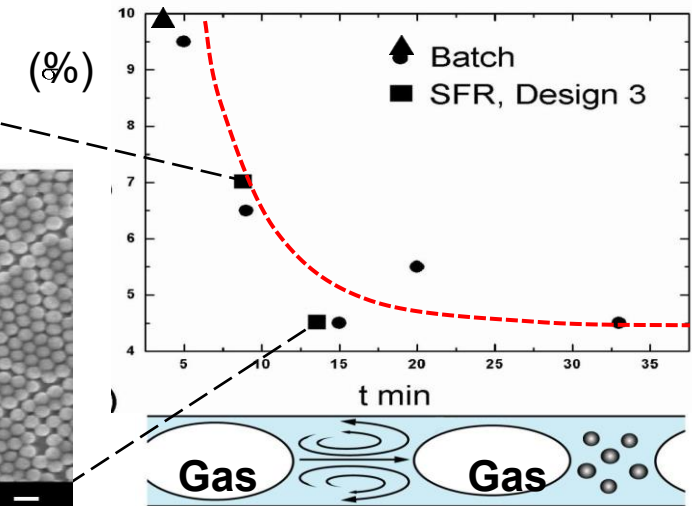
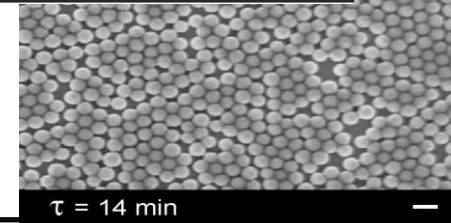
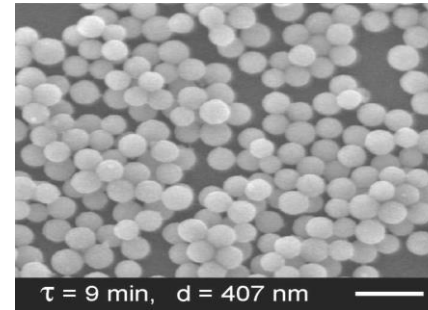
Synthesis of the NMC in batch operation

Silica Synthesis (Batch vs. continuous)

(via nucleation and growth)

- Batch vs. Segmented Flow Reactor (continuous)

- Segmented flow reactor (SFR) achieves continuous synthesis with particle uniformity matching traditional batch methods.
- Traditional method: uniform particles but limited scalability and throughput.



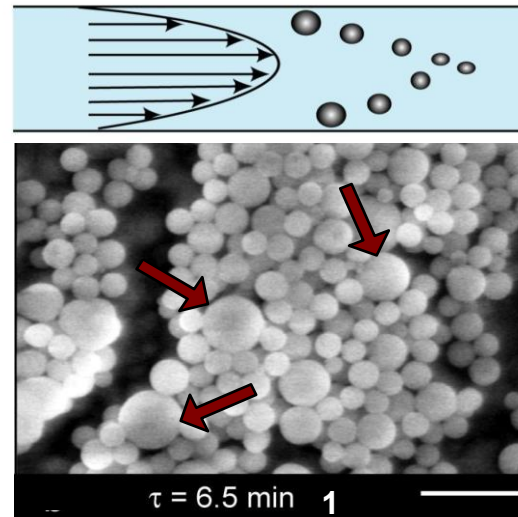
Pratsinis, Dudukovic, and Friedlander methodology (CES, 1986).

- Laminar Flow Reactor Design

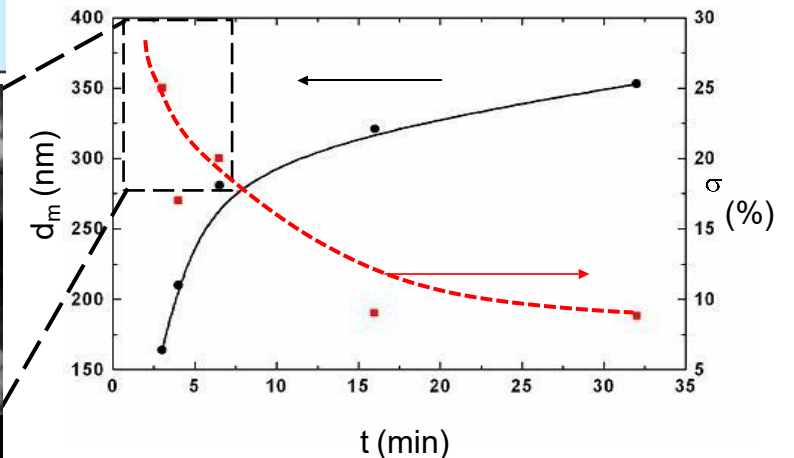
Laminar flow reactor (LFR) enables precise control of residence time distribution, critical for uniform particle nucleation and growth kinetics.

- Low Residence Time:

A wide particle size distribution (PSD) was observed due to rapid, non-uniform particle growth kinetics sensitive to RTD variations.



Khan, et al., Langmuir (2004), 20, 8604



Continuous synthesis nanomagnetic composite in an Oscillatory Baffled Reactor

Magnetite Batch operations

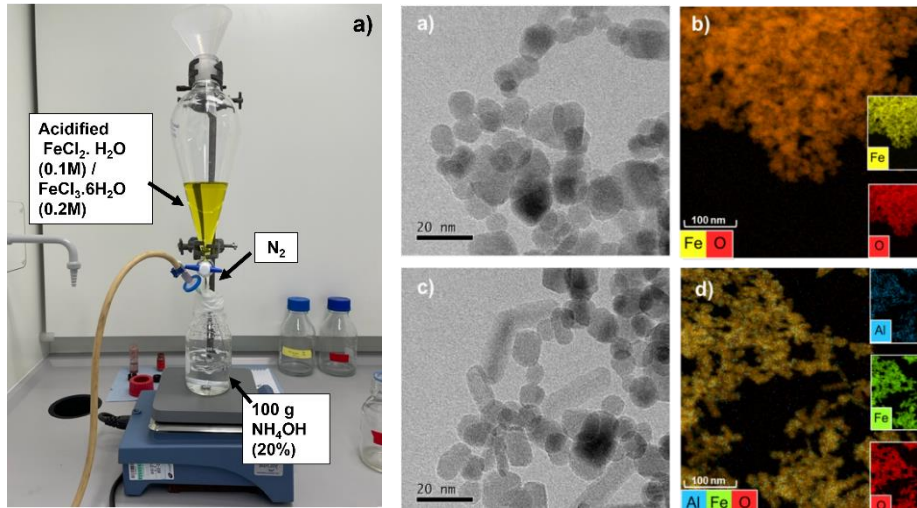
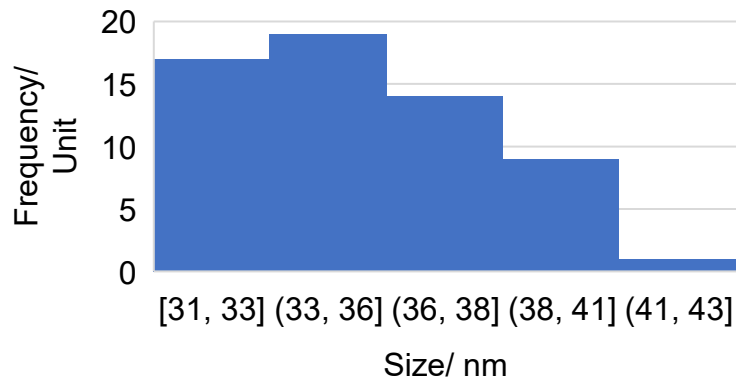
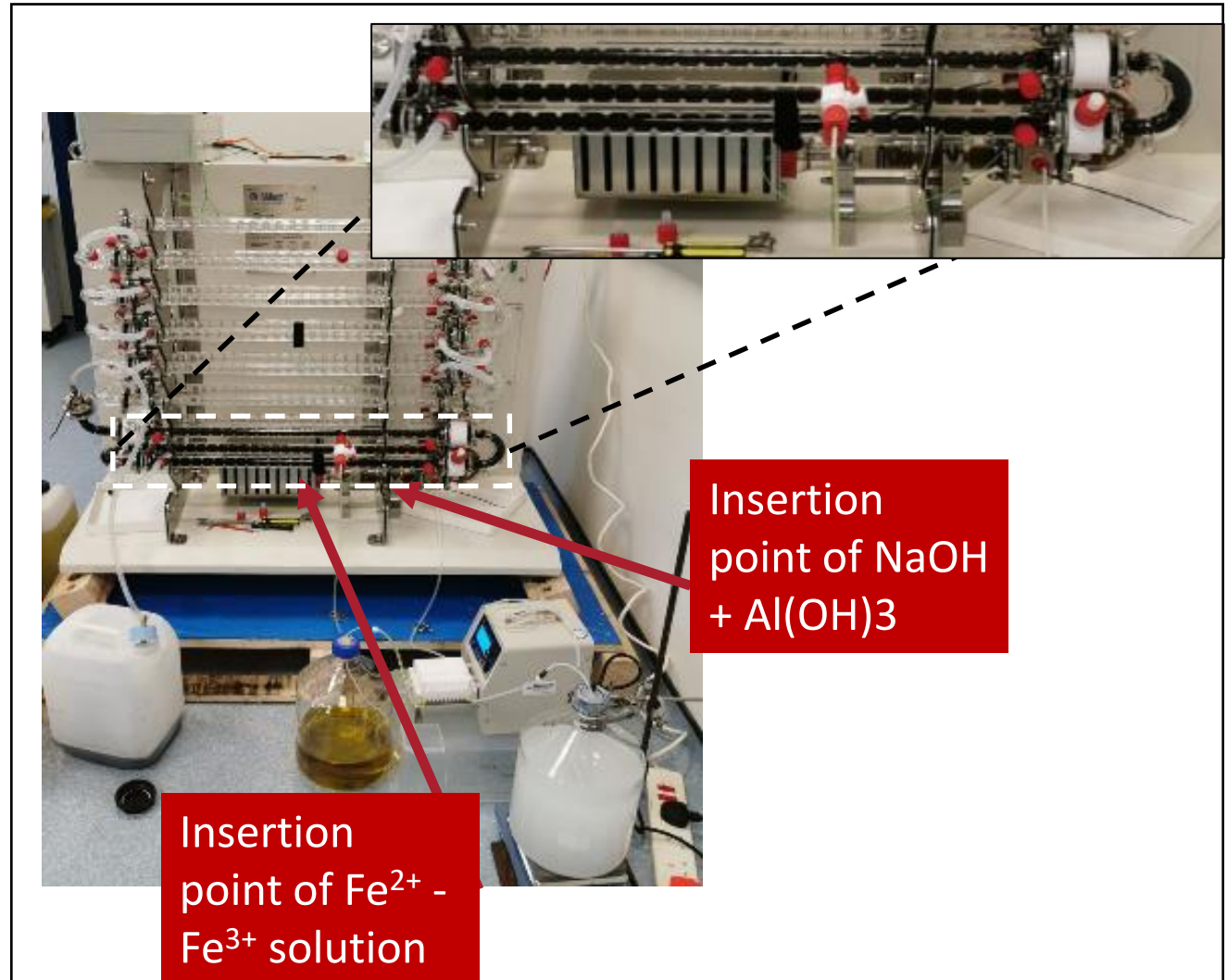


Chart shows size distribution of Magnetite/Maghemite with at 1:1 molar ratio of Fe(II) to Fe(III)

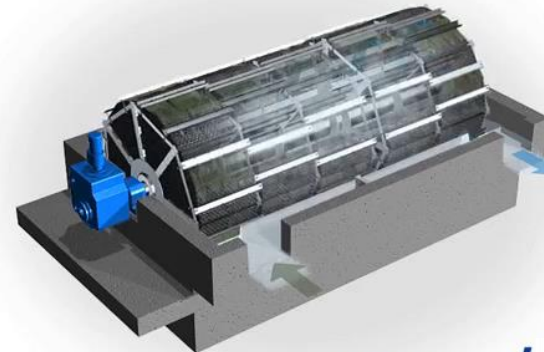
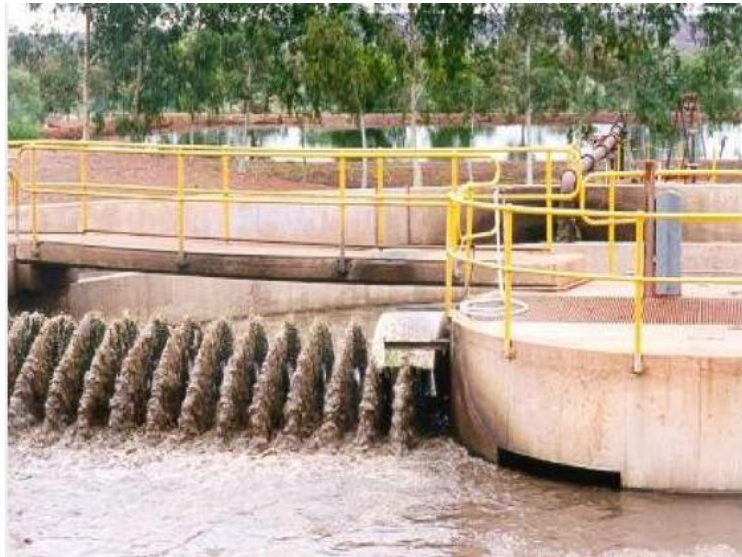


Continuous operations in Oscillatory Baffled Reactor

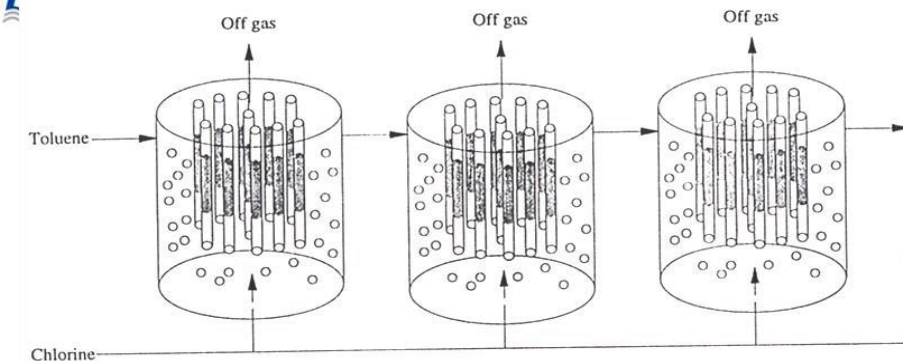
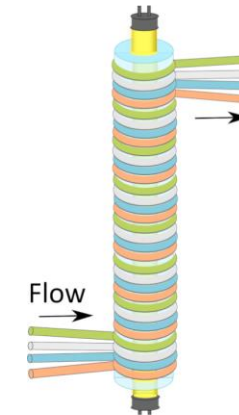
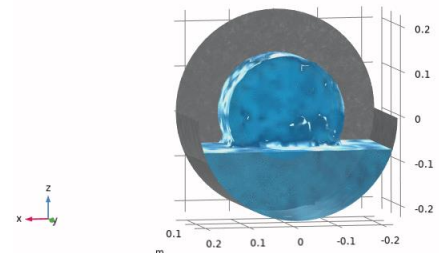


Function-domain Intensification

Photocatalytic degradation of phenol in a rotating disk reactor

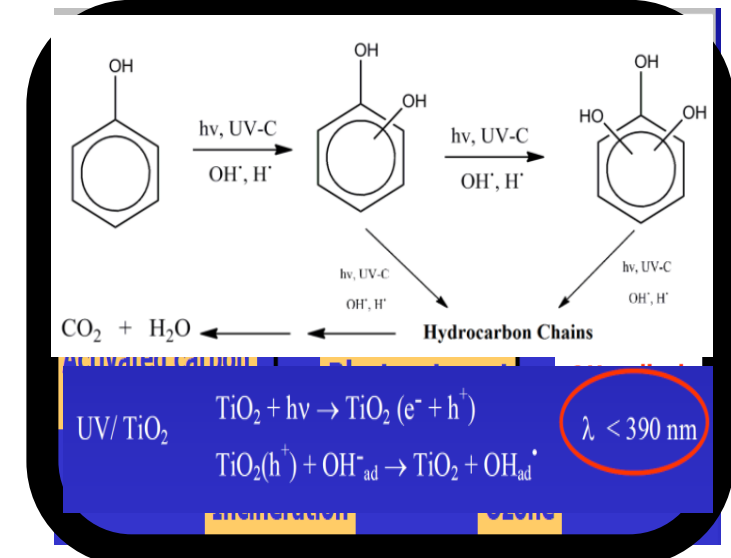
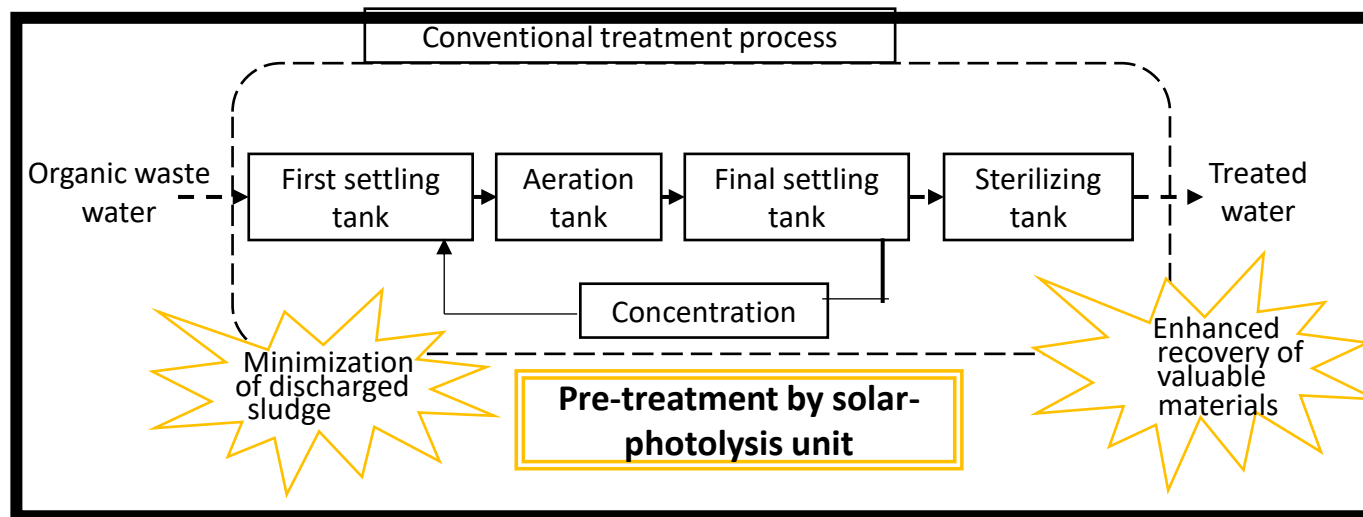
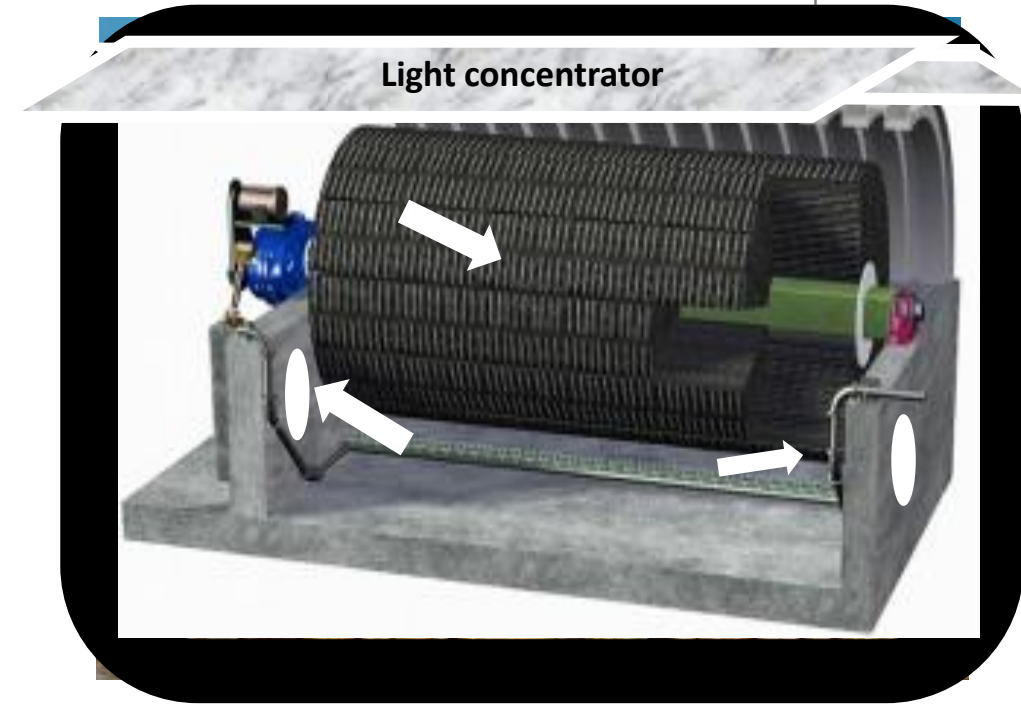


Time=0 s

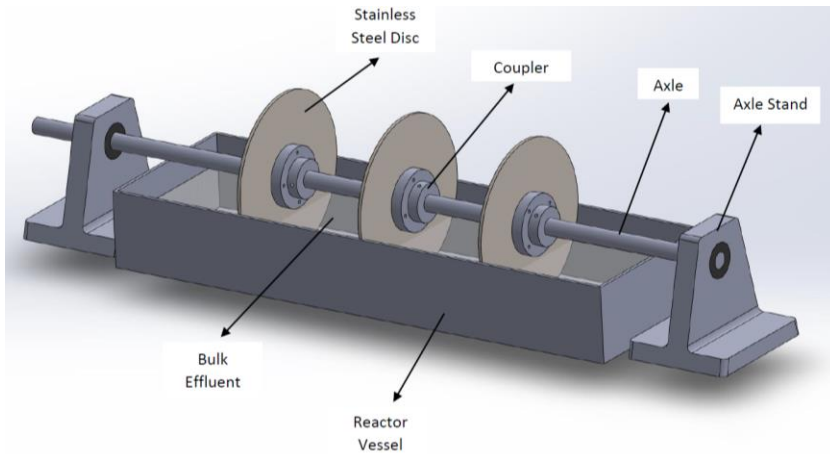


Schematic of Bubble Column Type of Photo Reactors (Commercially Used)

- UK sewage sludge production: 1.1 million dry tonnes per year, (Agricultural land: 62 %; Incineration: 19 %; land reclamation: 11 % and composting: 8%.
- Feasibility of 3D modelling of flow, mass and optical tracing



Kinetics of phenol degradation

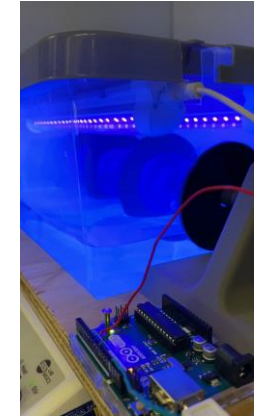


Assembly of photocatalytic reactor

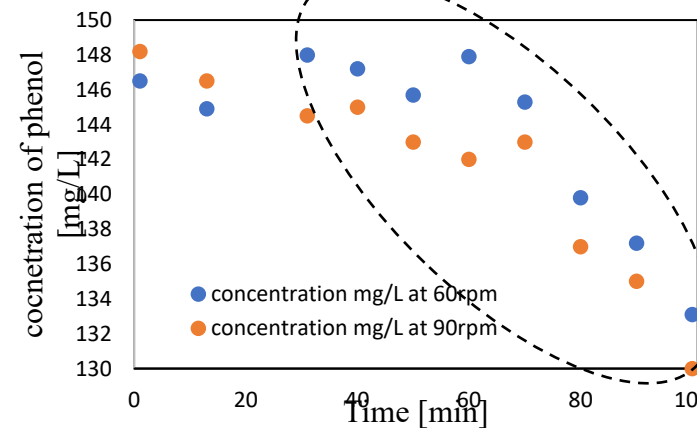
- Sonicating a slurry of TiO_2 in water ..10 g/L
- Hydrophobic/hydrophilic disc surfaces vs. mixing

Procedure

- Sand etching, controlled dipping at 0.87 mm/s, calcination (400°C)
- Surface stability testing (sonication and thermal) strength



- Volume = 750 mL, 15 W, UV-A (350 nm) bar light, Rotational speed = 25 rpm , Initial concentration = 150 mg/L, - Operating time = 100 minutes



Constant	Value
k (mg/L min)	0.680 ± 0.028
K (L/mg)	0.400 ± 0.117

$$R = aI_0 e^{-\epsilon hc} k K \frac{c}{1 + Kc}$$

Apparent first-order kinetic constant of $k_{deg} 0.002 \text{ min}^{-1}$. equivalent to photocatalytic space time yield (PSTY) of $6.25 \text{ mol day}^{-1} \text{ kW}^{-1}$

Concentration vs time for phenol degradation from 0-100 minutes. Initial concentration 150 mg/L, Two illumination bulbs of 15 W.

3D modelling by CFD (Comsol Multiphysics)

Film mass transport
+reaction

Momentum transport

Ray transport



1. Momentum transport

Euler-Euler approach with volume of fluid (VOF) analysis

- Navier-Stokes equations

$$\frac{\partial u}{\partial t} \rho + \rho(u \cdot \nabla)u = [-pI + \mu(\nabla u + \nabla u^T) + F_g + F_s]$$

- Phase field model (ϕ)

Where $\rho = \sum \phi; \phi = \alpha_q \rho_q; \sum \alpha_q = 1$

$$\frac{\partial \phi}{\partial t} + \mathbf{u} \cdot \nabla \phi = \gamma \nabla \cdot \left(\epsilon_{ls} \nabla \phi - \phi(1 - \phi) \frac{\nabla \phi}{|\nabla \phi|} \right)$$

2. Mass transport

2.1. in the liquid phase

$$\frac{\partial c_i}{\partial t} + \nabla \cdot (-D_i \nabla c_i) + u \nabla c_i = 0$$

2.2. In the disc catalytic phase

$$\frac{\partial c_i}{\partial t} + \nabla \cdot (-D_{ie} \nabla c_i) = R_i \quad \begin{aligned} R_i &= a I_0 e^{-\epsilon h c_i} k_{obs}(c_i) c_i \\ &= k'_{obs}(I_0, c_i) c_i \end{aligned}$$

3. Ray tracing geometry based on particle tracking concept (Landau and Lifshitz)

- Analogy of wave vector and frequency to the momentum \mathbf{p} and Hamiltonian H

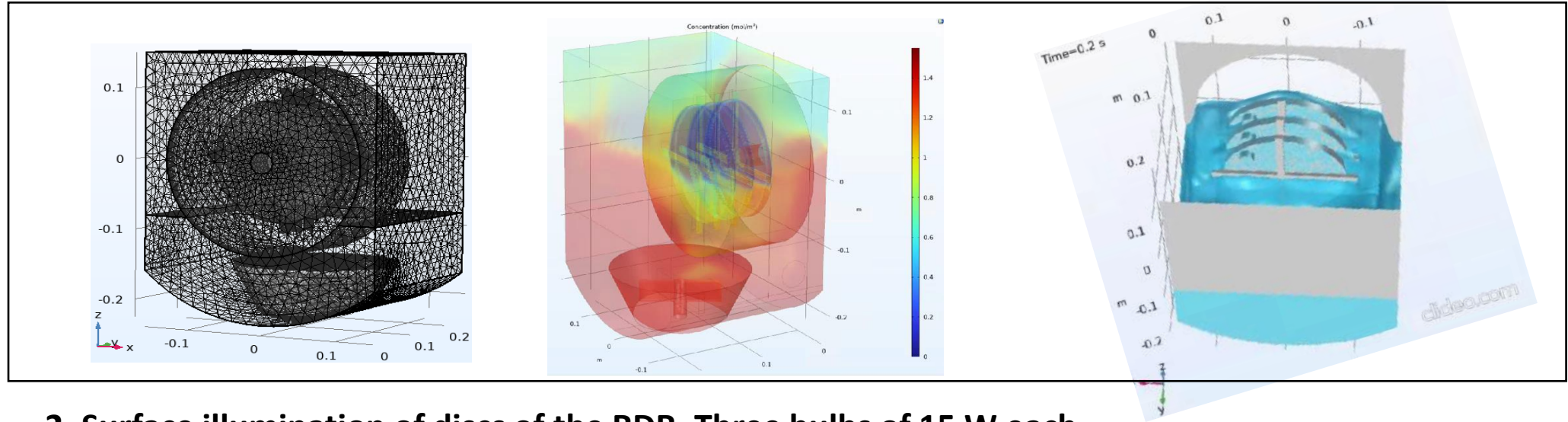
S is integral of Lagrangian $\frac{dq}{dt} = \frac{\partial \omega}{\partial k} \quad \frac{dk}{dt} = \frac{\partial \omega}{\partial q} \quad \omega = \frac{c|k|}{n(q)}$

CFD 3D modelling

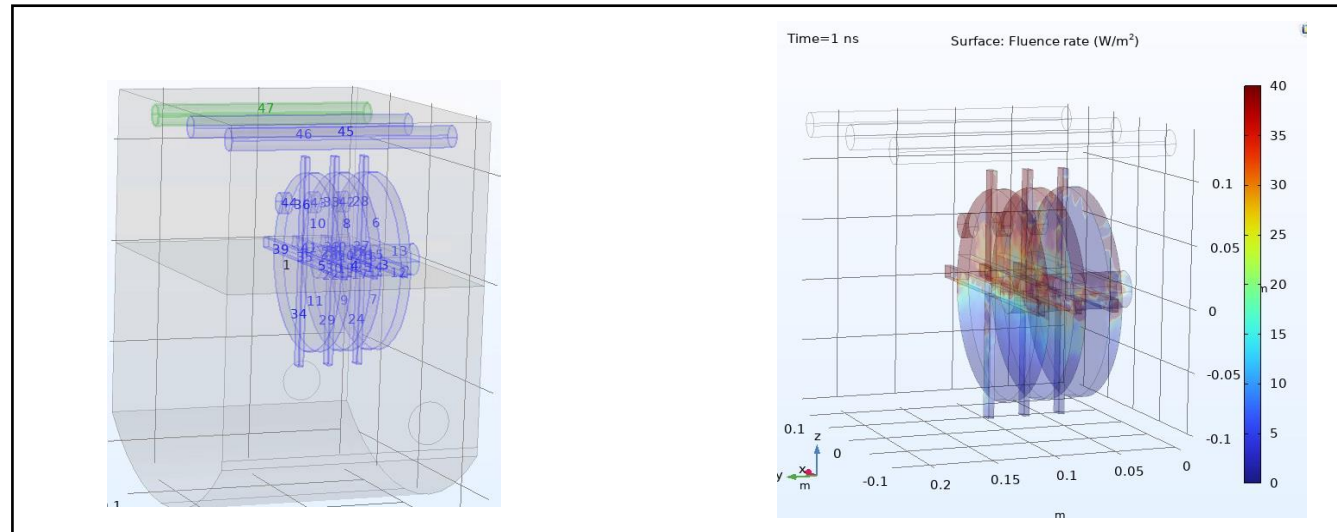
Discretisation by moving meshes



1. Surface liquid level localisation

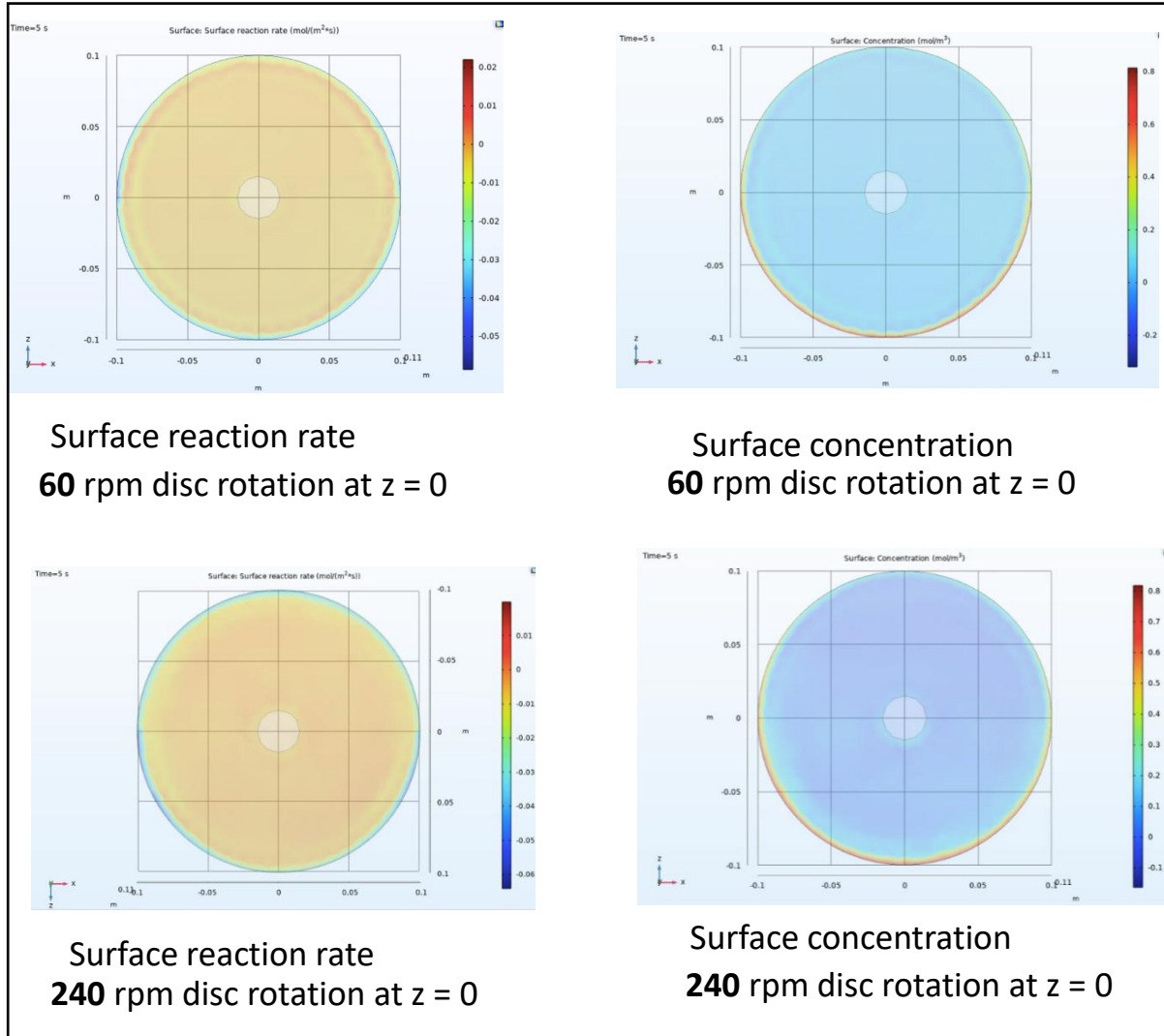


2. Surface illumination of discs of the RDR. Three bulbs of 15 W each

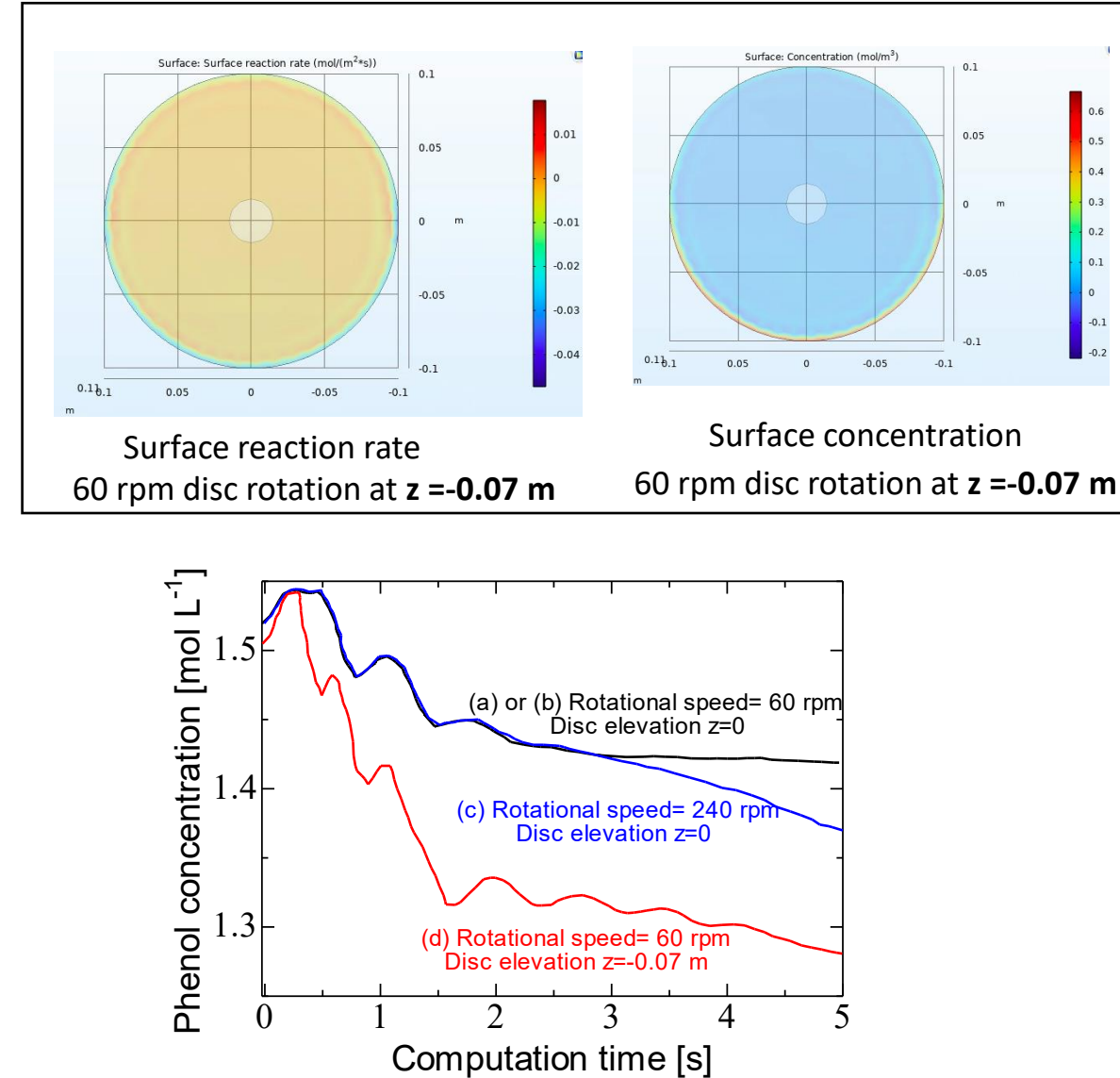


Progressing from reaction kinetics to transport-limited

Rotational speed



Liquid level



- Cultivate multi-scale concept process engineers
- Thermodynamic limitations are circumvented by innovative design
- ML uses tools to unify multifunctional units: reactor hydrodynamics and separation behaviour into single models
- AI models capture complex physics, helping organisations make better decisions.



With reduced expertise

- Mechanistic models give physical pictures and will remain..