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Headwater gas exchange quantified from O₂ mass balances at the reach scale

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25 **Abstract**

26 Headwater streams are important in the carbon cycle and there is a need to better
 27 parametrize and quantify exchange of carbon-relevant gases. Thus, we characterized
 28 variability in the gas exchange coefficient (k_2) and dissolved oxygen (O_2) gas transfer
 29 velocity (k) in two lowland headwaters of the River Avon (UK). The traditional one-
 30 station open-water method was complemented by in situ quantification of riverine sources
 31 and sinks of O_2 (i.e., groundwater inflow, photosynthesis and respiration in both the water
 32 column and benthic compartment) enabling direct hourly estimates of k_2 at the reach-
 33 scale (~150 m) without relying on the nighttime regression method. Obtained k_2 values
 34 ranged from 0.001 – 0.600 h^{-1} . Average daytime k_2 were a factor two higher than values
 35 at night, likely due to diel changes in water temperature and wind. Temperature
 36 contributed up to 46% of the variability in k on an hourly scale, but clustering
 37 temperature incrementally strengthened the statistical relationship. Our analysis
 38 suggested that k variability is aligned with dominant temperature trends rather than
 39 with short-term changes. Similarly, wind correlation with k increased when clustering
 40 wind speeds in increments correspondent with dominant variations (1 $m s^{-1}$). Time
 41 scale is thus an important consideration when resolving physical drivers of gas
 42 exchange. Mean estimates of k_{600} from recent parametrizations proposed for
 43 upscaling, when applied to the settings of this study, were found to be in agreement
 44 with our independent O_2 budget assessment (within <15%), adding further support to
 45 the validity of upscaling efforts aiming at quantifying large-scale riverine gas
 46 emissions.

47 Introduction

48 Revisions of the global carbon cycle have indicated that rivers and other
49 inland waters contribute substantially to the global cycling of organic carbon and
50 emission of carbon dioxide (CO₂) and methane (CH₄) to the atmosphere (e.g., Cole et
51 al. 2007; Battin et al. 2008; Tranvik et al. 2009; Aufdenkampe et al. 2011; Raymond
52 et al. 2013; Hotchkiss et al. 2015; Stanley et al. 2015; Marx et al. 2017). However,
53 due to a lack of an appropriate universal scaling for quantification of emissions,
54 headwaters (stream order < 4) were initially not included in these assessments (*see*
55 Cole et al. 2007), despite the fact they represent 17% of global riverine area (in
56 perennial riverine systems e.g., Downing et al. 2012). Later inclusions of headwaters
57 have proposed that small streams (order 1) might represent more than a third of the
58 total regional emissions of CO₂ from riverine systems (Butman and Raymond 2011)
59 and thus could be more prominent at the global scale (Raymond et al. 2013). This has
60 highlighted the need for better constraining gas exchange at the reach scale (Trimmer
61 et al. 2012), with the overarching goal of fine-tuning parametrizations used for large
62 scale and global upscaling of metabolism and gas emissions.

63 Accurate assessments of gas exchange require quantification of the gas
64 transfer velocity, or piston velocity (k ; unit of length per unit of time⁻¹, e.g., m h⁻¹),
65 which physically controls the exchange of gases at the stream–air interface (*see* Hall
66 et al. 2012). Thus, estimates of k are critical to the assessment of emission of
67 greenhouse gases such as CO₂ (e.g., Hotchkiss et al. 2015; Marx et al. 2017) and CH₄
68 (e.g., Stanley 2015; Crawford and Stanley 2016) and for the quantification of the gas
69 exchange rate of dissolved oxygen (O₂) and estimates of whole-reach metabolism
70 (e.g., Odum 1956). Stream gas exchange is most commonly assessed from total, i.e.,
71 whole-stream, metabolism estimates using open water (*OW*) methods based on local

72 dissolved oxygen (O_2) mass balances (e.g., Odum 1956; Marzolf et al. 1994;
 73 Mulholland et al. 2001; Riley and Dodds 2013; Siders et al. 2017). The OW approach
 74 provides an integrative quantification of gas exchange R_{ex} (in $\mu\text{mol L}^{-1}$ unit of time $^{-1}$)
 75 as

$$R_{ex} = k_2(O_{2(sat)} - O_2) \quad (1)$$

76 with ($O_{2(sat)} - O_2$) being the O_2 saturation deficit, i.e., the difference between the O_2
 77 concentration at saturation for the local physical conditions ($O_{2(sat)}$) and the actual O_2
 78 concentration in the stream water, and k_2 the O_2 gas exchange coefficient, often
 79 termed the re-aeration coefficient (k_2 or K , unit of time $^{-1}$, e.g., h $^{-1}$). The coefficient k_2
 80 represents the product of the depth-corrected O_2 gas transfer velocity, or piston
 81 velocity (k ; unit of length per unit of time $^{-1}$, e.g., m h $^{-1}$) and local stream area-to-
 82 volume ratio, which is often approximated as the inverse of the mean water depth (in
 83 m $^{-1}$) (see Raymond et al. 2012; Demars et al. 2015). As assessments of gas exchange
 84 critically rely on the quantification of k_2 or k , several direct and indirect methods have
 85 been developed for deriving these values.

86 Direct measurements of these parameters are characterized by the de-gassing
 87 of a conservative tracer gas that is subsequently scaled to O_2 (e.g., Wanninkhof et al.
 88 1990; Genereux and Hemond 1992; Reid et al. 2007; Benson et al. 2014). This
 89 approach is logistically demanding and temporal upscaling is difficult (Demars et al.
 90 2015). Indirect measurements depend on parameterizations of the local physical
 91 characteristics of the stream reach such as depth, flow and slope (e.g., Parker and Gay
 92 1987; Parker and DeSimone 1992 and references therein), as well as fitting of gas
 93 transfer parameters to O_2 time series based on simplified relationships (Hornberger
 94 and Kelly 1975; Chapra and DiToro 1991; McBride and Chapra 2005) or more
 95 complex modeling efforts (Holtgrieve et al. 2010; Grace et al. 2015; Appling et al.

2018). Empirical equations and parameterizations have proven to be useful as predictors of gas-exchange dynamics for specific reaches (*see* Genereux and Hemond 1992), but usually show large discrepancies in k_2 estimates when applied to streams with comparable hydrological characteristics (Moog and Jirka 1998; Aristegi et al. 2009; Palumbo and Brown 2014). To further constrain these parametrizations for spatial upscaling, recent studies have focused on a better characterization of the stream morphology. For example, Raymond et al. (2012) used a large collection of stream metadata to more rigorously scale k parametrizations to stream physical characteristics (i.e., flow, depth, slope, discharge).

Although k variability on short timescales, i.e., hours, has been reported (e.g., Tobias et al. 2009; Berg and Pace 2017), direct and indirect methods mostly focus on determining a mean value for k_2 for either the day or night, or an average for the whole day-night period, with little consideration being given to its short-term dynamics that are characteristic of most rivers. Recent application of the aquatic eddy co-variance technique (AEC) in rivers has provided robust assessment of reach-scale (~150 m) benthic metabolism (Koopmans and Berg 2015; Rovelli et al. 2017) and, most recently, an ‘inverted’ AEC approach has been used to directly quantify O_2 gas exchange in large (order 3) streams (Berg and Pace 2017) and in an estuarine embayment (Long and Nicholson 2018). Yet, irrespective of the approach being applied to assess k , little emphasis has been given to small headwaters streams (order 1-2), despite their potential implications for the regional and global carbon cycling (e.g., Butman and Raymond 2011; Raymond et al. 2013).

The goal of our study was to provide a proof-of-concept for the derivation (values and dynamics) of k_2 and k at the reach scale in small, headwater streams (stream order 1). This was achieved by combining in situ O_2 measurements from a

121 single station OW approach together with direct assessments of riverine metabolism
122 using AEC, sample incubations, and groundwater inflow measurements. The
123 proposed method was compared to the traditional nighttime regression (NR) method,
124 and was used to characterize temporal variability in k on hourly to daily time scales.
125 Furthermore, we evaluate k dynamics and its relation to the local physical drivers
126 such as mean stream flow, temperature and wind patterns. The results of this study are
127 discussed in light of parametrizations of k for regional to large-scale upscaling.
128

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129 **Materials and procedures**

130 Study site

131 This study focused on two headwaters of the Hampshire River Avon, southern
132 England: the Chalk River Ebble (CE) and the Greensand West Avon (GA) (*see*
133 Heppell et al. 2017; Supporting Information Fig. 1). For each headwater, a
134 representative ~150 m reach was selected based on previous surveys of the sub-
135 catchment morphology and geology (*see* field measurements). The selected CE reach
136 (CE1¹; 51° 1' 41.171" N / 1° 54' 56.309" W) was investigated over three days (25-27
137 Apr 2013) in spring, when the reach was characterized by a net outflow of stream
138 water to the aquifer, i.e., a losing reach (*see* Supporting Information Fig. 2). The reach
139 was also characterized by profuse growth (36% cover by area) of *Ranunculus spp.*,
140 which is widespread throughout the sub-catchment (Watson 1987). The water column
141 of the River Ebble was characterized by low turbidity, with suspended sediment
142 concentration limited to, on average, 37 mg L⁻¹ (Heppell and Binley 2016a). The
143 selected GA reach (GA2; 51° 19' 10.173" N / 1° 51' 33.135" W) was investigated over
144 three days from 28-30 Apr 2013. In contrast to the CE reach, the GA reach was
145 characterized by a constant inflow of low-oxygenated groundwater; i.e., a gaining
146 reach (Supporting Information Fig. 2) and only patchy macrophyte coverage (4% by
147 area). Turbidity in the water column was 40% higher on average than at the CE reach
148 (Heppell and Binley 2016a). The reaches are referred to as CE and GA throughout the
149 text.

150

151 Reach scale oxygen budget

¹ Reach designations within the Macronutrient Cycles Programme (<http://macronutrient-cycles.ouce.ox.ac.uk/>).

The assessment of O₂ gas exchange and stream metabolism based on a single station open-water approach (e.g., Odum 1956) relies on O₂ time series. Temporal changes in O₂ concentration, dO_2/dt , are attributed to local whole-stream primary production (P), respiration (R) and atmospheric exchange (R_{ex}) as

$$\frac{dO_2}{dt} = P + R + R_{ex} = P + R + k_2(O_{2(sat)} - O_2) \quad (2)$$

with k_2 being the gas exchange coefficient (in h⁻¹) and $(O_{2(sat)} - O_2)$ the O₂ saturation deficit. The spatial integration of a one-station approach, i.e., the integrated stretch length along the stream, is typically in the order of 1000s of m and can be quantify as $3v/k_2$, with v being the mean stream flow velocity (in m d⁻¹) and k_2 (in d⁻¹) (see Grace and Imberger 2006).

Rates for R and R_{ex} are typically estimated by applying the established nighttime regression (NR) method (Hornberger and Kelly 1975). The method plots the nighttime dO_2/dt at each time step against the O₂ saturation deficit during the night and assumes $P = 0$ and that respiration is light-independent. The resulting linear relationship, obtained via least-squares regression, provides both k_2 (slope) and R (intercept). As NR-based k_2 , k_{NR} , is only obtained at night, many studies have adopted a temperature correction term to account for temperature changes between night and day following the parameterization of Elmore and West (1961):

$$k_{2(T)} = k_{2(20^\circ C)}(1.0241)^{(T-20)} \quad (3)$$

where $k_{2(20^\circ C)}$ is the gas exchange coefficient at 20°C and $k_{2(T)}$ the gas exchange coefficient at the given temperature T .

The O₂ budget (OB) approach used in the current study expands Eq. 2 by accounting for all relevant processes including i) metabolic activity in both sediment

173 and water, and ii) exchange with both the atmosphere and groundwater (Fig. 1). The
 174 temporal O_2 concentration was thus defined as:

$$\frac{dO_2}{dt} = \frac{A}{V} [F_B + F_{WC} + F_K] \quad (4)$$

175 where F_B , F_{WC} , F_K are the O_2 flux (in $\text{mmol m}^{-2} \text{h}^{-1}$) associated with the benthic
 176 compartment, the water column, and atmospheric exchange, respectively. The O_2
 177 fluxes were expressed as volumetric rates (in $\mu\text{mol L}^{-1} \text{h}^{-1}$) by multiplying the values
 178 by the average ratio between stream area (A) and stream volume (V), which, under
 179 smooth stream water surface conditions, is approximated as the mean stream depth (d)
 180 (Demars et al. 2015).

181 The main strength of the proposed approach is that each flux component
 182 within the OB (Eq. 4) can be directly quantified in the field. Estimates of F_B were
 183 obtained from Aquatic Eddy Co-variance (AEC) measurements, while F_{WC} was
 184 quantified by incubating discrete water samples in situ (*see* section 2.3). While F_B
 185 does include both streambed ($F_{\text{streambed}}$) and groundwater contributions to the O_2
 186 budget, fluxes associated with the inflow of O_2 depleted groundwater were
 187 independently quantified as:

$$F_{GW} = v_{gw}(O_{2(gw)} - O_2) \quad (5)$$

188 with $O_{2(gw)}$ being the groundwater O_2 concentration (in $\mu\text{mol L}^{-1}$), O_2 the in-stream
 189 concentration and v_{gw} the local groundwater inflow (in m h^{-1}).

190 The atmospheric exchange rate was quantified as:

$$F_K = \frac{V}{A} k_2 (O_{2(sat)} - O_2) \quad (6)$$

191 with $k = k_2(V/A) \approx k_2d$ being the O_2 gas transfer velocity, or O_2 piston velocity (in m h^{-1})
 192 and $O_{2(sat)}$ the local O_2 concentration at saturation. As $O_{2(sat)}$ can be quantified as a

193 function of temperature (*see* Garcia and Gordon 1992), the OB approach effectively
194 enabled a direct estimate of k_2 .

195 To facilitate comparisons with published reference values and
196 parameterizations from previous studies, k_2 values were also expressed as $k_{2(20^\circ\text{C})}$ (*see*
197 Eq. 3). Similarly, estimates of O_2 gas transfer velocity were also standardized to a
198 Schmidt number of 600^2 (k_{600}) based on Jahne et al. (1998) as

$$\frac{k_{600}}{k} = \left(\frac{600}{Sc_T} \right)^{-1/2} \quad (7)$$

199 where $Sc_T \approx 0.00086842T^4 - 0.10115T^3 + 4.8055T^2 - 124.34T + 1745.1$ is the
200 Schmidt number for O_2 in freshwater at the local water temperature T (*see*
201 Wanninkhof 2014). Stream temperature time series were obtained from background
202 measurements of physical parameters during the observational period at each site
203 (Rovelli et al. 2016b).

204 Field measurements

205 *Site selection* – The investigated reaches (CE and GA) were carefully selected
206 to represent the sub-catchment dominant stream morphology features (e.g., stream
207 course shape, depth, bends, riparian zone) and in-stream habitat patchiness
208 (macrophytes, sediment type). Particular emphasis was given to ensure that each
209 reach also fulfilled the theoretical requirements of the NR method, i.e., streams with
210 relatively high metabolic activity and low gas exchange (*see* Hornberger and Kelly
211 1975). Field measurements were also executed under stable hydrological condition,
212 i.e., constant flow and mean water depth over ≥ 3 days. This enabled i) the evaluation
213 of our local O_2 budget (OB) method and ii) comparisons with the nighttime regression
214

² Schmidt number for CO_2 at 20°C and O_2 at 17.5°C in freshwater.

(NR) method and standardized functional equations for k_2 quantification from mean hydrological parameters (Table 4).

Background physicochemical measurements – Stream water column O_2 concentration, temperature and photosynthetically active radiation (PAR) at the streambed (~15 cm above the bottom) were monitored within each reach at 1 min intervals with a conductivity–temperature–depth logger (CTD; XR-420, RBR, Kanata, Canada), equipped with an Aanderraa O_2 optode sensor (Aanderaa, Bergen, Norway) and a 4 π PAR sensor (QCP-2000; Biospherical Instruments, San Diego, United States). The data were also used to calibrate the O_2 sensors used for flux estimates and to define nighttime periods ($PAR < 2 \mu\text{mol quanta m}^{-2} \text{s}^{-1}$). Wind speed and direction near the stream surface (1.5 m elevation) were recorded at 15 s intervals with a SkyWatch GEOS 11 portable weather station (JDC Electronic SA, Yverdon-les-Bains, Switzerland).

Benthic oxygen flux – The benthic oxygen flux was quantified using the AEC technique (Berg et al. 2003). Our AEC module consisted of small, lightweight, stainless steel tripod frame equipped with an acoustic Doppler velocimeter (ADV; Vector, Nortek A/S, Rud, Norway), Clark-type O_2 microelectrodes (Revsbech 1989) and submersible O_2 amperometric amplifiers (McGinnis et al. 2011). Up to two O_2 microelectrodes were positioned ~0.5 cm outside the ADV sampling volume, at an inclination of ~60°. Each microelectrode had a 90 % response times < 0.5 s and stirring sensitivity < 0.5 % (Gundersen et al. 1998). The ADV's flow measurements were obtained at 8 – 15 cm from the streambed with a frequency of 64 Hz and with the ADV x-axis aligned to the main flow direction. The acquired datasets were processed following the same procedure described in Rovelli et al. (2017). In short, the dataset was averaged to 8 Hz while applying data quality controls and despiking

240 routines (e.g., Mori et al. 2007) to the dataset to remove dataset artifacts and reduce
 241 signal noise. A double coordinate rotation was applied to the flow time series to
 242 minimize the influence of horizontal motions on the vertical velocity component. The
 243 datasets were then aligned, i.e., time-shifted, to account for the relative distance
 244 between the ADV sampling volume and the microelectrode tip and for the
 245 microelectrode time constant (*see* Donis et al. 2015). The AEC-based turbulent
 246 oxygen fluxes (in $\text{mmol m}^{-2} \text{h}^{-1}$) were estimated from time-averaged vertical
 247 velocity fluctuations (w') and O_2 concentration fluctuations (C'), as

$$F_{AEC} = \overline{w'C'} \quad (8)$$

248 (*see* Berg et al. 2003) via a Reynolds' decomposition, specifically linear detrending,
 249 using the program suite Sulfide-Oxygen-Heat Flux Eddy Analysis (SOHFEA version
 250 2.0; *see* McGinnis et al. 2014). The optimal detrending interval represents a trade-
 251 off between including low-frequency turbulent contributions and excluding non-
 252 turbulent contributions (McGinnis et al. 2008), and was inferred to be 5 min
 253 from cumulative averages of oxygen fluxes and friction velocity (u_*) (*see* Attard
 254 et al. 2014). To account for the effect of transient O_2 concentration changes in the
 255 water column between the sediment-water interface and the AEC measurement height
 256 (h), which can potentially bias F_{AEC} (*see* Holtappels et al. 2013; Rheuban et al. 2014),
 257 an O_2 storage term was estimated after Rheuban et al. (2014). The benthic oxygen flux
 258 corrected for O_2 storage, F_B , was defined as

$$F_B = F_{AEC} + F_{storage} = F_{AEC} + \int_0^h \frac{dC}{dt} dz \quad (9)$$

259 with dC/dt being the measured O_2 concentration gradient.
 260 The smallest area of the streambed that contributes to 90 % of AEC flux, termed the
 261 “footprint area”, was estimated from the sediment surface roughness parameter (z_0)

and h following the parameterization by Berg et al. (2007). Values for z_0 were approximated as $z_0 = h \cdot \exp(-\kappa \cdot \frac{u}{u_*})$ with κ being the von Karman constant (0.41), and u the average flow velocity (Wüest and Lorke 2003).

Water column activity – Water column oxygen production and consumption rates were estimated by incubating 100 mL rack-mounted glass bottles in situ over 24 h in the light and in the dark, with continuous measurements of O_2 concentration via O_2 optical fibers (4 channel FirestingO2; Pyro Science GmbH, Aachen, Germany). A set of 1 dark bottle, and 1 clear bottle were incubated at the streambed, while 1 bottle was incubated near the stream surface. The fourth bottle was either incubated at mid-depth at GA (depth > 0.4 m) or near the surface for the shallower CE. Three additional replicate sets were also mounted on the rack but O_2 measurements were only performed at the start and end of each incubation via Winkler titrations (Winkler 1888). Volumetric oxygen fluxes (in $\mu\text{mol L}^{-1} \text{h}^{-1}$) were estimated from temporal O_2 concentration gradients via linear regressions for daytime and nighttime periods, respectively. No difference in fluxes were observed at the different depths, indicating a homogeneously, well-irradiated water column and thus depth-independent rates. The areal oxygen fluxes F_{WC} (in $\text{mmol m}^{-2} \text{h}^{-1}$) were obtained by multiplying the values with the average stream depth. Contributions from macrophytes were deemed to be well-integrated within benthic measurements and thus were not further addressed within the water column oxygen budget (Rovelli et al. 2017).

Groundwater influx – Dissolved oxygen flux resulting from local inflow of O_2 depleted groundwater was estimated based on measurements of the local hydraulic gradients from in-stream piezometers and porewater O_2 concentrations. Two clusters of in-stream piezometers were installed at each site, approximately 10 m apart in the river thalweg. Each cluster comprised three piezometers screened at 20, 50 and 100

287 cm depth; the 100 cm piezometer was also fitted with narrow polytetrafluoroethylene
288 tubing to depths of 10, 20, 30, 50, 70 and 100 cm for the purposes of pore water
289 sampling. Installation and design of the piezometers followed the description in
290 Binley et al. (2013).

291 Hydraulic head was measured in all piezometers using HOBO pressure
292 transducers (Onset Computer Corporation, Bourne, United States) at GA and
293 Levellogger Edge pressure transducers (Solinst, Georgetown, Canada) at CE.
294 Measurements were validated with manual dips on a fortnightly basis and, if needed,
295 corrected assuming a linear drift. River stage was measured using a pressure
296 transducer suspended within a stilling well. Falling and rising head slug tests
297 (measurements taken by pressure transducers installed inside the piezometers) were
298 used for computation of saturated hydraulic conductivity using the Hvorslev method
299 (e.g., Binley et al. 2013). Vertical groundwater flux was computed using Darcy's
300 Law, from measurements of the hydraulic gradient between the 50 cm deep
301 piezometric head and local stream stage, combined with a weighted harmonic mean of
302 hydraulic conductivity from slug tests carried out in the 20 cm and 50 cm deep
303 piezometers (*see* Binley et al. 2013).

304 Pore water samples were collected from sampling tubes located on the
305 piezometers every two months, from February 2014 to June 2016, using a syringe and
306 tygon tubing. The O₂ concentration of pore water and river water was measured
307 immediately following sample collection using a calibrated Clark-type O₂
308 microelectrode (50 µm tip) connected to an in-line amplifier and data-logging meter
309 (Unisense, Aarhus, Denmark) (*see* Heppell and Binley 2016b).

310 *Data handling* – Collected hydrological and physicochemical data were used
311 to i) characterize average conditions at each reach and ii) assess short term, i.e.,

312 hourly, to diel dynamics. O₂ fluxes obtained for each stream compartment were
313 considered separately, to assess their magnitude and variability within and across the
314 reaches, as well as within the O₂ budget context, to quantify and characterize *k*
315 variability.
316

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317 **Assessment**

318 Reach characterization

319 Hydrological data and background information for each reach are summarized
 320 in Table 1. Temperature ranged from 7.8 – 13.5 °C overall, reflecting a moderate
 321 variation (< 5%) between day and night at the two sites. Daily-integrated PAR
 322 (PAR_{24}) ranged between 11.9 – 17.4 mol quanta $m^{-2} d^{-1}$, with peaks of up to 1630
 323 μmol quanta $m^{-2} s^{-1}$. Overall, the average stream flow, based on ADV measurements
 324 (12 cm above the streambed), was in the order of 0.18 – 0.33 $m s^{-1}$ with an associated
 325 discharge of 0.209 – 0.640 $m^3 s^{-1}$ (Table 1) and showed no significant change between
 326 day and night, or within the observational period, indicating a stable flow. Wind
 327 speeds at CE showed irregular patterns but an overall higher wind speed during the
 328 day than at night (Fig. 2). Wind dynamics at GA, in contrast, were markedly diel,
 329 with an average wind speed of 2.4 – 3 $m s^{-1}$ during the day and 0 – 0.2 $m s^{-1}$ at night
 330 (Fig. 3). At both sites the water column showed well-defined diel fluctuations in O_2
 331 concentration, with nighttime under-saturation (down to 82%) and daytime
 332 oversaturation (up to 133%), with diel O_2 concentration changes reaching $\sim 147 \mu mol$
 333 L^{-1} (Fig. 2, 3). The O_2 saturation deficit ranged from -108 – -96 $\mu mol L^{-1}$, during the
 334 day, to 43 – 65 $\mu mol L^{-1}$, at night. The average deficit over 24h ranged from 2 μmol
 335 L^{-1} to an O_2 saturation surplus of 15 $\mu mol L^{-1}$.

336

337 Dissolved oxygen budget

338 *Benthic compartment* – Hourly oxygen fluxes for the benthic compartment
 339 ranged between -14.0 to 23.0 $mmol m^{-2} h^{-1}$ (Fig. 2, 3). At CE, oxygen fluxes followed
 340 a clear diel pattern (Fig. 2), with average daytime rates of 4.2 $mmol m^{-2} h^{-1}$ and
 341 nighttime rates of -2.8 $mmol m^{-2} h^{-1}$. AEC-based benthic fluxes were estimated to

cover a footprint area 26 m long and 1 m wide ($\sim 20 \text{ m}^2$), with most of the flux contribution, i.e. the region of maximum flux, located 0.5 m upstream of the AEC sampling point. At GA, a diel pattern in the benthic oxygen fluxes was also observed (Fig. 3). However, both mean fluxes at night and during the day were negative, amounting to $-6.2 \text{ mmol m}^{-2} \text{ h}^{-1}$ and $-3.0 \text{ mmol m}^{-2} \text{ h}^{-1}$, respectively. The theoretical footprint area was 80 m long and 1 m wide ($\sim 70 \text{ m}^2$) with the region of maximum flux located 2 m upstream of the of the AEC sampling point.

Water column – At CE, metabolic activity in the water column was below detection ($< 0.1 \mu\text{mol L}^{-1} \text{ h}^{-1}$) and negligible for the local O_2 budget (Fig. 2). In contrast, in the more turbid, sandy GA, water column activity ranged from net oxygen production rates of $2.8 \mu\text{mol L}^{-1} \text{ h}^{-1}$ during the day, to oxygen consumption of $-0.9 \mu\text{mol L}^{-1} \text{ h}^{-1}$ at night. The average daytime rate of oxygen production was $\sim 1.2 \text{ mmol m}^{-2} \text{ h}^{-1}$, with an average nighttime consumption rate of $-0.5 \text{ mmol m}^{-2} \text{ h}^{-1}$ (Fig. 3).

Groundwater – During our study, the CE reach was losing water to the aquifer. This net local outflow of stream water had no measurable effect on in-stream O_2 concentrations (Fig. 2). At gaining reach GA, the inflow of groundwater amounted to 0.043 m d^{-1} on average, with a mean groundwater O_2 concentration of $63.5 \mu\text{mol L}^{-1}$. Groundwater contributed to an areal O_2 concentration decrease of $-0.4 - -0.7 \text{ mmol m}^{-2} \text{ h}^{-1}$ (average $-0.5 \text{ mmol m}^{-2} \text{ h}^{-1}$), representing 6-7% of the combined nighttime flux caused by metabolic activity in the benthic compartment and the water column (Fig. 3).

Atmospheric exchange – The derived rate of O_2 exchange between the stream and the atmosphere ranged from -22.3 to $14.5 \text{ mmol m}^{-2} \text{ h}^{-1}$. Estimates of k_2 based on the O_2 budget (OB) method ranged from 0.001 to 0.600 h^{-1} , with mean values of 0.252 h^{-1} and 0.259 h^{-1} for CE and GA, respectively (Table 2). Within such range of k_2 and

with mean flow velocities of $0.18 - 0.33 \text{ m s}^{-1}$, one-station based assessment are expected to integrate a stream length of $> 7 \text{ km}$).

Estimates of the gas exchange coefficient k_2 using the NR method (k_{NR}) were 0.555 h^{-1} at CE and 0.434 h^{-1} at GA (Table 3 and Supporting Information Fig. 3), and thus around a factor 2 higher than those obtained with the OB method. (Table 2, 3). At CE, we observed a significant ($p < 0.01$) difference between daytime and nighttime estimates of k_2 (Fig. 2 and Table 2). The average daytime k_2 (k_{day}) was 0.331 h^{-1} and about 2 times higher than k_2 at night (k_{night}). Similar conditions were observed at GA (Fig. 3 and Table 2), suggesting that diel changes in temperature and wind could partly explain the observed difference between day and night variability in k_2 at both sites.

Dynamics and variability of O_2 gas exchange

Temperature – Gas exchange coefficient (k_2) and gas transfer velocity (k) are expected to be related to local stream temperature (Elmore and West 1961; Kilpatrick et al. 1989; Demars and Manson 2013). Yet, temperature has been reported to be a weak predictor of k in some settings (Tobias et al. 2009; Demars and Mason 2013), as well as in modeling studies (e.g., Correa-Gonzalez et al. 2014). For example, Tobias et al. (2009) used a modified sulfur hexafluoride (SF_6) tracer approach to assess variability in k (k_{SF_6}) on time scales of hours (in 3h intervals) and found that k_{SF_6} varied by 30% over a 32 h observational period and could apportion 39% of the observed variability to changes in temperature (Demars and Mason 2013).

At CE, our hourly estimates of k varied by 60%, on average, between consecutive measurements during our 3 days observational period, with temperature accounting for 46% of that variability (Supporting Information Fig. 4). As expected

392 from previous studies (e.g., Tobias et al. 2009; Demars and Manson 2013), part of this
393 variability could be accounted for by applying the Elmore and West (1961)
394 temperature correction to normalize k to 20°C (k_{20} ; Supporting Information Fig. 4).
395 However, we found that temperature corrected k_{20} could only explain 10% of the k –
396 temperature relationship, and only 5% of the variability measured in k at CE. This
397 provided further evidence that the dynamics of k could not be properly accounted for
398 by simple functions for temperature corrections.

399 Instead, at CE we found that the relationship between k and temperature could
400 be strengthened by clustering k values to fixed temperature increments, increasing
401 stepwise from 0.5 to 1.7°C. The best linear relationships (i.e., highest regression
402 coefficients) were observed by clustering data in increments of 1.0 to 1.5 °C ($R^2 >$
403 0.8), with R^2 decreasing, either side, for shorter or longer increments (Supporting
404 Information Fig. 4) and we found the best fit to the data occurred with 1.5°C
405 increments (Fig. 4a). As the clustering procedure partially accounts for the variability
406 in both temperature and k , the trend in increasing fit to the data (higher R^2) suggested
407 that dynamics in k and temperature, and their interaction, may occur at variable time
408 scales. This trend was, however, not observed at GA, where temperature revealed no
409 direct correlation with k on hourly time scales ($R^2=0.02$) or with temperature
410 clustering ($R^2=0.03$), indicating that temperature changes in the water column did not
411 significantly contribute to k variability at the site.

412 Temperature dynamics, however, may affect gas exchange without any
413 detectable changes in bulk O₂ concentrations in the water, as recently proposed by
414 Berg and Pace (2017). The authors applied the same AEC approach as in this study,
415 but in an “upside-down” configuration, with AEC measurements being performed
416 near the (underside) of the stream surface (~5 cm below the atmosphere-water

417 interface), rather than near the streambed. This enabled the quantification of O₂ flux
418 and heat flux across the stream surface, from which they inferred local O₂ gas
419 exchange and values for k . Their results showed that temperature fluctuations
420 occurring just below the surface might bias the quantification of O₂ fluctuations and
421 thus AEC-based assessments of k . The implications of the study by Berg and Pace
422 (2017) suggest that other methodological approaches commonly used for the
423 quantification of k at timescales ranging from minutes to complete diel cycles could
424 also be impacted. The absence of any relationship between water column temperature
425 and k at GA could thus, in part, be attributed to small-scale temperature dynamics that
426 are not accounted for by simple temperature correction functions; though other
427 physical parameters such as wind, for example, could also modulate k at GA.

428 *Wind* – Here the reaches were open to the wind (e.g., Supporting Information
429 Fig. 1), with frequent wind-induced ripples being observed during the day, suggesting
430 an interaction between flow and wind that could affect gas exchange. On time scales
431 of hours, however, wind dynamics revealed no significant relationship with the
432 derived variability in k ($R^2=0.13$). Similar results have also been reported from other
433 methodological approaches, e.g., tracer release (Tobias and al. 2009) and AEC (Berg
434 et al. 2017); though both studies relied on off-site, rather than on-site wind
435 measurements. As large variability in both k and wind might mask any general trend,
436 wind data were temporally clustered to investigate any time lag between wind
437 dynamics and derived k values. Using a bin interval of 1 m s^{-1} , which represented the
438 dominant (> 90%) wind fluctuations at each site (Supporting Information Fig. 5), we
439 revealed a robust positive linear relationship ($R^2 > 0.7$) between local wind and k_{600} at
440 each site and for both sites combined (Fig. 4b). Given the relatively low range in wind
441 speed ($0 - 4 \text{ m s}^{-1}$), a linear relationship provided a suitable approximation, though for

442 more extensive ranges in wind speed a quadratic form is more appropriate (e.g.,
443 Wanninkhof 1992; Nightingale et al. 2000; Sweeney et al. 2007; Wanninkhof 2014).
444 Similarly to the effect of temperature, increasing or decreasing the size of the wind
445 clustering increment resulted in a lowering of the regression coefficient, thus further
446 supporting the argument of a temporal misalignment between the drivers of k
447 variability and actual k dynamics.
448

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449 **Discussion**

450 Parametrization of gas exchange coefficients

451 Our study was performed under stable discharge and constant stream depth,
 452 which allowed both i) the evaluation of our local O₂ budget (OB) method for deriving
 453 k_2 directly and then, ii) the comparison with the nighttime regression (NR) method
 454 and standardized functional equations for k_2 quantification (Table 4). The advantage
 455 of the OB method over the latter approaches is that the method is not limited to stable
 456 hydrological conditions or specific time periods. This contrasts with the NR method,
 457 for instance, where estimates of k_2 obtained at night might not be applicable during
 458 the day. Furthermore, the OB approach relies on in situ measurements of local O₂
 459 mass balance variables, rather than parametrizations and scaling relationship from
 460 literature values. The method is therefore ideal for investigating discrepancies
 461 between the various procedures for estimating k_2 and thus strengthens the
 462 parameterization procedures applied for upscaling global estimates of outgassing
 463 coefficients for other gases such as CO₂ and CH₄.

464 In this study, the NR method systematically provided among the highest
 465 estimates of k_2 for both reaches. Values of k_{NR} were, on average, a factor of two
 466 higher than k_2 derived by the OB method (Fig. 5). The largest discrepancies, by up to
 467 a factor of three, were observed at nighttime, while, during the daytime, mean values
 468 were within reported uncertainties for this approach (Palumbo and Brown 2014).
 469 Potential issues with NR method applicability or dataset quality were deemed
 470 marginal, as both CE and GA met the requirements of the NR method (*see* Methods),
 471 and the O₂ time series were of a high quality (Supporting Information Fig. 3).
 472 Therefore, the observed discrepancies in k_2 are attributed to a biased estimation of R
 473 derived at nighttime using the NR method (R_{NR}), leading to a systematic

474 overestimation of k_2 .

475 Studies investigating the effect of local inflows of O₂-depleted groundwater
476 have shown that groundwater might bias the quantification of R in open water
477 approaches and thus whole-stream O₂ budget assessments (e.g., McCutchan et al.
478 2002; Hall and Tank 2005; Koopmans and Berg 2015). The magnitude of such effect,
479 which would lead to an overestimation of R , might vary according to hydrological
480 characteristics and hydrological connectivity of each stream, ranging from negligible
481 to substantial (*see* McCutchan et al. 2002). In this study, the contribution from
482 groundwater to the O₂ budgets was quantified directly. At gaining reach GA,
483 groundwater contributions to whole-stream estimates of R were limited to 0.5 mmol
484 m⁻² h⁻¹, representing < 5% of the mean R_{NR} (15.5 mmol m⁻² h⁻¹); the combined R from
485 the benthic compartment and water column activity was 6.7 mmol m⁻² h⁻¹. At losing
486 reach CE, contributions from groundwater were negligible but the NR method still
487 estimated R at 8.7 mmol m⁻² h⁻¹, which is some 3-fold higher than our direct
488 measurements (2.8 mmol m⁻² h⁻¹).

489 An overestimation of R during night could also result from a temporal misalignment
490 between actual changes in whole stream respiration and physical parameters
491 controlling gas exchange. As shown in both datasets (Fig. 2, 3), temperature
492 decreased at night until about 6 – 8 AM, and directly affected the measured saturation
493 deficit. If k_2 is assumed to be constant, as shown from our NR regression plots (*see*
494 Supporting Information Fig. 3), then the temperature-driven increase in the O₂
495 concentration at saturation, and associated O₂ saturation deficit, will result in an
496 erroneous estimate of the magnitude of R_{NR} .

497 It has recently been shown that k (and thus k_2) might display changes of up to a
498 factor of 2–3 over timescales of 10s of minutes to hours, even under constant

hydrological conditions (e.g., Berg and Pace 2017), implying that k_2 will not remain constant over the several hours' time scale associated with the NR method. Since the NR approach considers changes in the magnitude of k_2 as a direct and instantaneous consequence of changes in R , variability in k_2 could explain the magnitude of the R_{NR} bias obtained in this study, though the drivers of that variability, such as temperature, wind and stream discharge, need further investigation (Berg and Pace 2017).

Hydrological parameters such as stream depth, stream flow and stream energy (e.g., slope, shear velocity) have been used to derive k_2 (e.g., O'Connor and Dobbins 1958; Palumbo and Brown 2014) and subsequently k_{600} . Given the local hydrology (0.4 – 0.57 m mean depth, 0.18 – 0.33 m s⁻¹ mean flow velocity), our mean values of k_{600} derived with the (OB) method (0.121 ± 0.007 m h⁻¹ for CE and 0.190 ± 0.016 m h⁻¹ for GA), are well within the range predicted by 19 sets of proposed functional equations extracted from the literature (0.009 – 0.236 m h⁻¹ at CE and 0.023 – 0.373 m h⁻¹ at GA; Table 4, Fig. 5). NR-derived values were also within that range, although they ranked towards the upper end of the range. As expected from previous studies (see Aristegi et al. 2009; Palumbo and Brown 2014), estimates from each equation were highly scattered throughout the obtained range, with little consistency between the two sites. For instance, even equations that were previously identified to perform well in hydrology settings similar to our study, i.e., “top performer” equations (see Palumbo and Brown 2014), still showed large discrepancies - both within and across sites (Fig. 5). In contrast, we found that the revised functional equations provided by Raymond et al. (2012) provided well-constrained estimates, which were not only consistent within sites (see Supporting Information Fig. 6), but also between sites, with mean k_{600} values (0.113 m h⁻¹ for CE and 0.201 m h⁻¹ for GA) within 5–7% of the local estimates from our OB method (Fig. 5).

524

525 **Comments and recommendations**

526 The aquatic eddy co-variance technique (AEC) has been shown to be an
527 effective tool for quantifying streambed metabolism and, more recently, for the
528 quantification of O₂ gas exchange and k from O₂ fluxes near the stream surface (Berg
529 and Pace 2017). A combination of the AEC technique with other traditional methods
530 appears to be a promising next step towards better constrained assessments of gas
531 exchange and k dynamics in headwaters, provided that careful consideration is given
532 to i) the site selection and ii) the representativeness of the reach within the km-sized
533 integration of, e.g., open-water approaches. The O₂ budget (OB) approach presented
534 in this study serves as a proof-of-concept towards this goal. While the approach is
535 more time consuming and field demanding than traditional methods, it does enable i)
536 the compartmentalization of stream metabolism and ii) the assessment of short-term k
537 variability. The study has highlighted short-term variability in k dynamics with a
538 dampened relationship to variations of well-known physical drivers. The apparent
539 lack of correlation could be attributed to temporal misalignments between the
540 variability of the derived k and physical drivers, and to small-scale variability in
541 temperature. This was clearly observed at CE, where temperature-corrected k_{20} and
542 k_{600} values still revealed a marked temperature dependency, suggesting that common
543 temperature corrections were insufficient to fully account for the observed k
544 variability. It remains unclear whether and to what extent such small-scale variability
545 in temperature will affect the overall gas exchange.

546 Although the above aspects are still poorly constrained at the local scale and on short
547 time scales (hours), estimates of k from the most recent functional parametrizations
548 compared well with the independent assessments of this study and should therefore be

549 preferred over earlier parametrizations. Validations of k on local scales such as the
550 ones presented in this study are strongly required to strengthen and add more
551 confidence to the upscaling of k for the quantification of large-scale metabolism and
552 global emission of climate-relevant gases such as CO_2 and CH_4 across headwaters and
553 throughout riverine networks.

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882

883 **Figure Legends**

884 Fig. 1. Dissolved oxygen mass balance approach. Changes in stream O₂ concentration are
885 expressed as a function of contributions from the water column (F_{WC}), benthic compartment
886 (F_B) and atmospheric exchange (F_K) following the parameterization of Eq. 4. Benthic F_B
887 includes contributions from the streambed ($F_{streambed}$) and from groundwater inflow/outflow
888 (F_{GW}). Note that lateral exchange and advection processes were not considered.

889
890 Fig. 2. Estimates of k_2 for the river Ebble (CE) during the spring. (A) Wind speed
891 recorded 1.5 m above the stream surface. (B) Local dissolved oxygen (O₂)
892 concentration (gray line) and associated O₂ concentration at atmospheric saturation
893 (dotted line). Black lines indicate nighttime ($PAR < 2 \mu\text{mol quanta m}^{-2} \text{ s}^{-1}$). (C) Time
894 series of oxygen fluxes encompassing benthic (F_B), water column (F_{WC}) and
895 groundwater (F_{GW}) contributions to the local O₂ budget. (D) Hourly averaged
896 estimates of k_2 based on the O₂ budget (OB) method in spring (circles), with
897 temperature overlain (dashed line).

898
899 Fig. 3. Estimates of k_2 for the river West Avon (GA) during the spring. (A) Wind
900 speed recorded 1.5 m above the stream surface. (B) Local dissolved oxygen (O₂)
901 concentration (gray line) and associated O₂ concentration at atmospheric saturation
902 (dotted line). Black lines indicate nighttime ($PAR < 2 \mu\text{mol quanta m}^{-2} \text{ s}^{-1}$). (C) Time
903 series of oxygen fluxes encompassing benthic (F_B), water column (F_{WC}) and
904 groundwater (F_{GW}) contributions to the local O₂ budget. (D) Hourly averaged
905 estimates of k_2 based on the O₂ budget (OB) method in spring (circles), with
906 temperature overlain (solid line). Note that the wind data were shifted by 24 h to fill
907 the measurement gap on day 1.

908
909 Fig. 4. Temperature and wind dependencies of the gas transfer velocity k . (A)
910 Temperature relationship of k at CE. Values for k (solid black circles), k normalized
911 to 20°C (k_{20} ; open grey circles) and to a Schmidt number of 600 (k_{600} , solid grey
912 circles) were clustered into 1.5°C temperature increments to account for temporal
913 misalignments and to provide the most robust linear analysis ($R^2 > 0.9$; see
914 Supporting Information Fig. 4). (B) Standardized k_{600} as a function of wind speed for
915 CE (solid black squares), GA (open white squares) and both sites combined (dotted
916 line). Wind speeds were clustered into 1 m s⁻¹ bins to account for the dominant

magnitude of wind fluctuations (*see* Supporting Information Fig. 5). Linear trends were obtained via least squares regression.

Fig. 5. Estimates of k_{600} (in m h^{-1}) for (A) river Ebble and (B) West Avon. Estimates are obtained from different published hydrological parameterizations (Equations 1 – 18, and Raymond et al. (2012)); from the O_2 budget (OB) method used in this study (*see* Eq. 4); and from the nighttime regression (NR) method. Equation numbering follows Table 4. Note that crossed equations were reported to be the “top-performer” within a specific mean depth and mean flow range from an extensive database of tracer-based k_2 values and hydrological parameters (*see* Palumbo and Brown 2014). Mean value and uncertainty range (dashed and dotted lines) for the hydrological parameterizations of Raymond et al. (2012) were obtained by combining mean and range from of each equation. (*see* Table 4; Supporting Information Fig. 6). Note that to better highlight the differences between the OB, NR and common parametrizations, the equation order was re-arranged to show an incremental increase in k_{600} .

926 **Tables**

927 Table 1. Summary of hydrological and physicochemical data for river Ebble (CE) and West Avon (GA). Average values are presented as mean \pm
928 standard error. Values between square brackets indicate the range of the measurements.

Site	Period	Daylight [h]	Total PAR [mol m ⁻² d ⁻¹]	O ₂ [% sat]	O ₂ [μmol L ⁻¹]	T [°C]	Depth ¹ [m]	Width ¹ [m]	Flow [m s ⁻¹]	Discharge ¹ [m ³ s ⁻¹]
CE	25-27 Apr 2013	15.3	11.9	106.6 \pm 0.3 [87.7 – 132.7]	367.7 \pm 0.9 [301.5 – 449.5]	10.8 \pm 0.03 [8.4 – 13.5]	0.41	5.25	0.18	0.640
GA	28-30 Apr 2013	15.3	17.4	101.5 \pm 0.3 [82.3 – 127.2]	365.3 \pm 1.2 [303.0 – 449.3]	9.0 \pm 0.02 [7.8 – 10.7]	0.57	2.75	0.33	0.385

929 ¹: Obtained from depth and flow velocity transects performed during the observational period under stable hydrograph (see Rovelli et al. 2016a).

930 Table 2. Estimates of k_2 (in h^{-1}) using the O_2 budget (OB) method. Values for daytime, nighttime and average over the observational period are
931 reported as mean \pm standard error, with n indicating the number of averaged data points. Standardized $k_{2(20^\circ\text{C})}$ (in h^{-1}) and k_{600} (in m h^{-1}) are also
932 reported to enable better comparisons with literature studies.

Site	Day	Night	Mean
	k_2 [h^{-1}] (n)		
CE	0.331 \pm 0.024 (63)	0.170 \pm 0.012 (62)	0.252 \pm 0.015 (125)
GA	0.367 \pm 0.034 (26)	0.188 \pm 0.020 (37)	0.261 \pm 0.021 (63)
	$k_{2(20^\circ\text{C})}$ [h^{-1}] (n)		
CE	0.404 \pm 0.030 (63)	0.214 \pm 0.014 (62)	0.310 \pm 0.019 (125)
GA	0.478 \pm 0.045 (26)	0.248 \pm 0.027 (37)	0.343 \pm 0.028 (63)
	k_{600} [m h^{-1}] (n)		
CE	0.157 \pm 0.012 (63)	0.084 \pm 0.006 (62)	0.121 \pm 0.007 (125)
GA	0.265 \pm 0.025 (26)	0.137 \pm 0.015 (37)	0.190 \pm 0.016 (63)

933
934

Table 3. Estimates of k_2 using the nighttime regression method (k_{NR}). Values are reported with the respective regression coefficient (R^2) for each site. The associated plots are available in the Supporting Information (Fig. 3). The temperature-normalized values of k_{NR} for 20 °C ($k_{NR(20^\circ C)}$), are computed based on the mean nighttime temperature at each site, while the daily NR-based k scaled for a Schmidt number of 600 ($k_{NR(600)}$), in $m\ h^{-1}$ was computed for the mean daily temperatures.

Site	$k_{NR}\ [h^{-1}]\ (R^2)$	$k_{NR(20^\circ C)}\ [h^{-1}]$	$k_{NR(600)}\ [m\ h^{-1}]$	Night temperature (°C)
CE	0.554 (0.78)	0.694	0.273	10.5
GA	0.421 (0.78)	0.539	0.304	8.7

Table 4. Estimates of k_{600} (in m h^{-1}) from established empirical equations applied to the CE and GA study sites. Input variables[#]: d – stream depth (m), u – flow velocity (m s^{-1}), u^* – friction velocity (m s^{-1}), s – stream slope (m m^{-1}), Q – discharge ($\text{m}^3 \text{ s}^{-1}$), and $Fr = u/\sqrt{gd}$ – Froude number with g being the gravitational acceleration constant. Note that most equations provide k_2 at 20°C ($k_{2(20^\circ\text{C})}$, in day^{-1} ; Supporting Information Table 1); $k_{2(20^\circ\text{C})}$ values that were scaled to k_{600} based on Eq.7 and the O_2 Schmidt number for 20°C (Table 1).

Eq.	Reference	Abbr.##	Equations	CE k_{600} [m h^{-1}]	GA
1	O'Connor and Dobbins (1958)	OD	$k_{2(20^\circ\text{C})} = 3.9 \frac{u^{0.5}}{d^{1.5}}$	0.099	0.114
2a	Churchill et al. (1962)	E ₄	$k_{2(20^\circ\text{C})} = 0.0217 \frac{u^{2.695}}{d^{3.0855} s^{0.825}}$	0.009	0.023
2b		CEB	$k_{2(20^\circ\text{C})} = 5.01 \frac{u^{0.969}}{d^{1.673}}$	0.067	0.096
3	Krenkel and Orlob (1963)	E ₆ , KO	$k_{2(20^\circ\text{C})} = 173.01 \frac{(us)^{0.404}}{d^{0.66}}$	0.199	0.285
4a	Owens et al. (1964)	E ₈	$k_{2(20^\circ\text{C})} = 6.91 \frac{u^{0.73}}{d^{1.75}}$	0.148	0.180
4b		E ₉ , OEG	$k_{2(20^\circ\text{C})} = 5.35 \frac{u^{0.67}}{d^{1.85}}$	0.139	0.158
5	Dobbins (1965)	DB*	$k_{2(20^\circ\text{C})} = 55.2 \frac{1 + Fr^2}{(0.9 + Fr)^{1.5}} \frac{(us)^{0.375}}{d} \coth \left[\frac{4.75(us)^{0.125}}{(0.9 + Fr)^{0.5}} \right]$	0.117	0.139
6a	Langbein and Durum (1967)	E ₇	$k_{2(20^\circ\text{C})} = 5.14 \frac{u}{d^{1.33}}$	0.048	0.078
6b		LD	$k_{2(20^\circ\text{C})} = 5.14 \frac{u}{d^{0.67}}$	0.026	0.054
7	Issacs and Gaudy (1968)	IG	$k_{2(20^\circ\text{C})} = 4.76 \frac{u}{d^{1.5}}$	0.051	0.080
8	Cadwallader and McDonnell (1969)	E ₃ , CM	$k_{2(20^\circ\text{C})} = 186.07 \frac{(us)^{0.5}}{d}$	0.136	0.184

9	Negulescu and Rojanski (1969)	NR	$k_{2(20^{\circ}\text{C})} = 10.91 \frac{u^{0.85}}{d}$	0.085	0.150
10	Thackston and Krenkel (1969)	TK*	$k_{2(20^{\circ}\text{C})} = 24.9 \frac{u^*(1 + Fr^{0.5})}{d}$	0.013	0.025
11	Padden and Gloyna (1971)	PG	$k_{2(20^{\circ}\text{C})} = 4.53 \frac{u^{0.703}}{d^{1.054}}$	0.055	0.082
12a	Bennett and Rathbun (1972)	E ₁ , BR1	$k_{2(20^{\circ}\text{C})} = 32.69 \frac{u^{0.413} S^{0.273}}{d^{1.408}}$	0.163	0.183
12b		E ₂ , BR2	$k_{2(20^{\circ}\text{C})} = 5.58 \frac{u^{0.607}}{d^{1.689}}$	0.140	0.161
13	Parkhurst and Pomeroy (1972)	PP*	$k_{2(20^{\circ}\text{C})} = 48.5 \frac{(1 + 0.17Fr^2)(us)^{0.375}}{d}$	0.097	0.122
14	Bansal (1973)	BN	$k_{2(20^{\circ}\text{C})} = 1.81 \frac{u^{0.6}}{d^{1.4}}$	0.036	0.045
15	Owens (1974)	–	$k_{2(20^{\circ}\text{C})} = 50.8 \frac{u^{0.67} \text{###}}{d^{0.85}}$	0.236	0.373
16	Tsivoglou and Neal (1976)	E ₁₀ , TN	$k_{2(20^{\circ}\text{C})} = k_2' us \text{###}$	0.128	0.325
17	Smoot (1988)	SM	$k_{2(20^{\circ}\text{C})} = 543 \frac{u^{0.5325} S^{0.6236}}{d^{0.7258}}$	0.136	0.206
18	Thackston and Dawson (2001)	TD*	$k_{2(20^{\circ}\text{C})} = 4.97 \frac{u^*(1 + 9Fr^{0.25})}{d}$	0.012	0.024
19a	Raymond et al. (2012)	Rm ₁	$k_{600} = 5037(us)^{0.89} d^{0.54}$	0.113	0.231
19b		Rm ₂	$k_{600} = 5937(1 - 2.54Fr^2)(us)^{0.89} d^{0.58}$	0.125	0.252
19c		Rm ₃	$k_{600} = 1162u^{0.85} S^{0.77}$	0.096	0.160
19d		Rm ₄	$k_{600} = 951.5(us)^{0.76}$	0.097	0.154
19e		Rm ₅	$k_{600} = 2841us + 2.02$	0.127	0.162
19f		Rm ₆	$k_{600} = 929(us)^{0.75} Q^{0.011}$	0.102	0.160
19g		Rm ₇	$k_{600} = 4725(us)^{0.86} Q^{-0.14} d^{0.66}$	0.128	0.287

944 #: Average stream depth and flow velocity are taken from (Table 1). The average shear velocity, u_* , computed as $u_* = u(C_D)^{1/2}$, with C_D being the drag coefficient (Wüest and
 945 Lorke 2003). An average C_D of 3.3×10^{-3} was used for both sites based on further surveys of the River Avon sub-catchments (Rovelli et al. 2017). The average slope, 0.002 m m^{-1} ,
 946 was estimated from GPS measurements during the respective field campaigns.
 947 ##: Reference equation numbers and abbreviations from Aristegi et al. (2009) and Palumbo and Brown (2014), respectively.
 948 ###: This equation requires depth in cm and flow velocity in cm s^{-1} .
 949 ####: with k_2 being $31183 \text{ s m}^{-1} \text{ d}^{-1}$ for $Q < 0.280 \text{ m}^3 \text{ s}^{-1}$ and $22500 \text{ s m}^{-1} \text{ d}^{-1}$ for $Q > 0.280 \text{ m}^3 \text{ s}^{-1}$, respectively (Palumbo and Brown 2014).
 950 *: These equations were identified to be the most suited (i.e., top performer) for the site mean depth and flow based on the suggestions of Palumbo and Brown (2014).

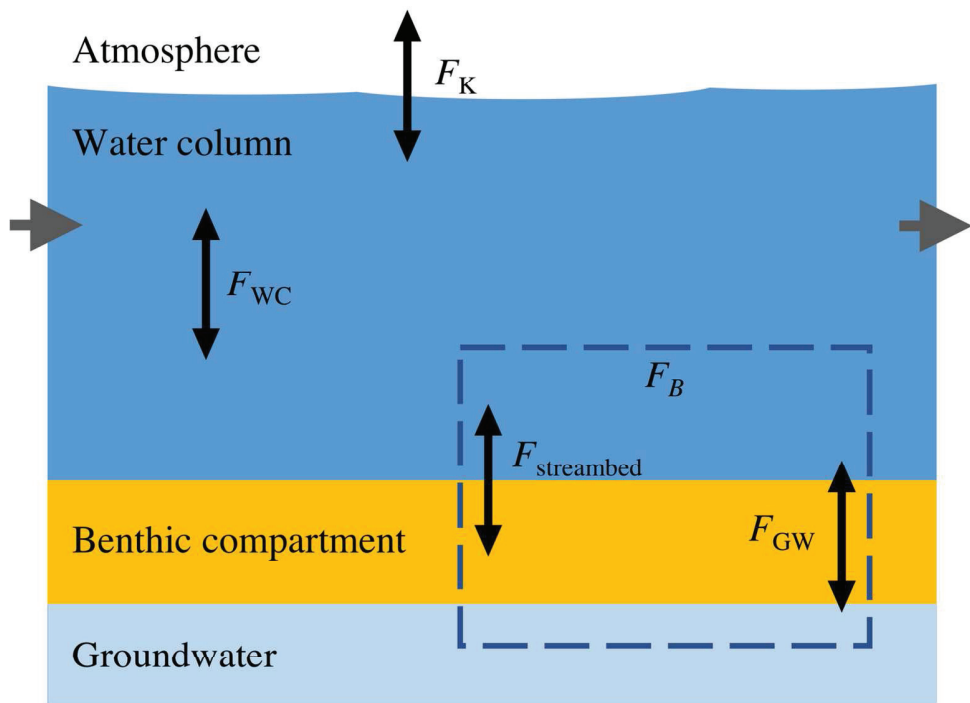


Figure 1. Dissolved oxygen mass balance approach. Changes in stream O₂ concentration are expressed as a function of contributions from the water column (F_{WC}), benthic compartment (F_B) and atmospheric exchange (F_K) following the parameterization of Eq. 4. Benthic F_B includes contributions from the streambed ($F_{streambed}$) and from groundwater inflow/outflow (F_{GW}). Note that lateral exchange and advection processes were not considered.

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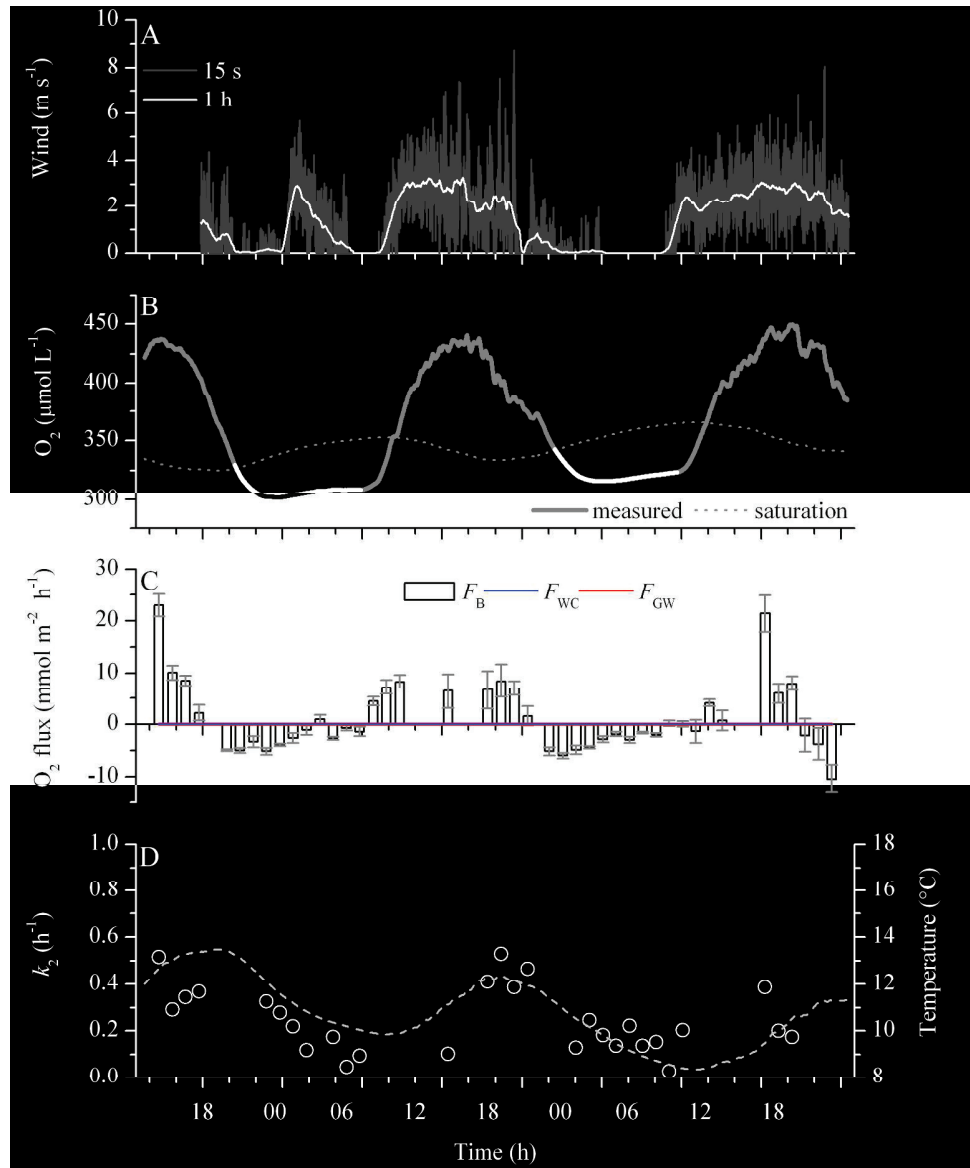


Figure 2. Estimates of k_2 for the river Ebble (CE) during spring. (A) Wind speed recorded 1.5 m above the stream surface. (B) Local dissolved oxygen (O_2) concentration (gray line) and associated O_2 concentration at atmospheric saturation (dotted line). Black lines indicate nighttime ($\text{PAR} < 2 \mu\text{mol quanta m}^{-2} \text{s}^{-1}$). (C) Time series of oxygen fluxes encompassing benthic (F_B), water column (F_{WC}) and groundwater (F_{GW}) contributions to the local O_2 budget. (D) Hourly averaged estimates of k_2 based on the O_2 budget (OB) method in spring (circles), with temperature overlain (dashed line).

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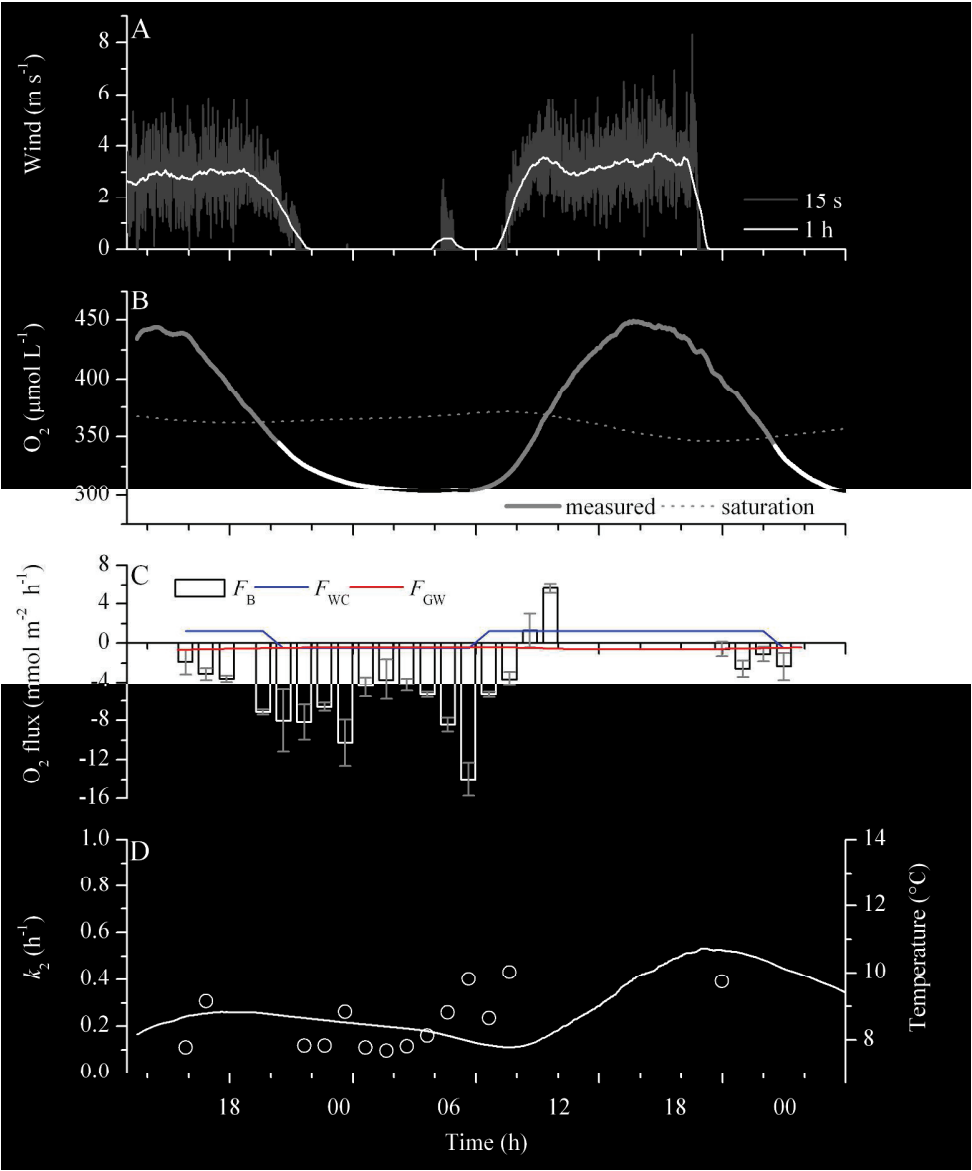


Figure 3. Estimates of k_2 for the river West Avon (GA) during the spring. (A) Wind speed recorded 1.5 m above the stream surface. (B) Local dissolved oxygen (O_2) concentration (gray line) and associated O_2 concentration at atmospheric saturation (dotted line). Black lines indicate nighttime ($PAR < 2 \mu\text{mol quanta m}^{-2} \text{s}^{-1}$). (C) Time series of oxygen fluxes encompassing benthic (F_B), water column (F_{WC}) and groundwater (F_{GW}) contributions to the local O_2 budget. (D) Hourly averaged estimates of k_2 based on the O_2 budget (OB) method in spring (circles), with temperature overlain (solid line). Note that the wind data were shifted by 24 h to fill the measurement gap on day 1.

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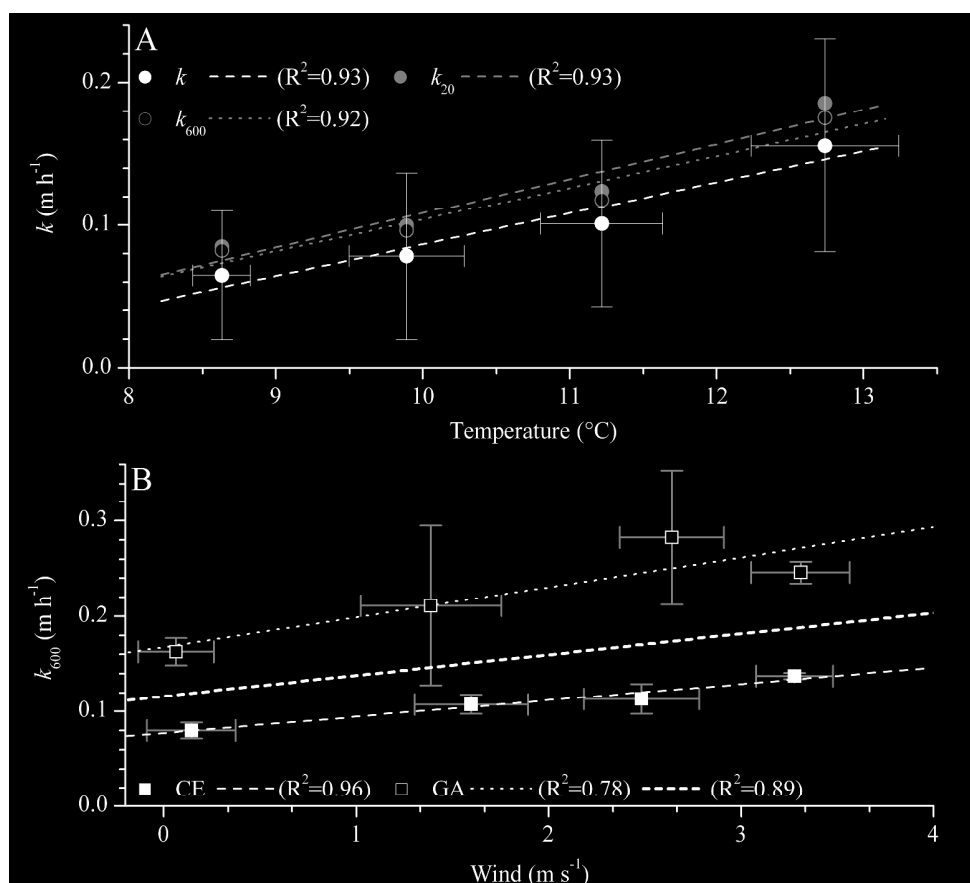


Figure 4. Temperature and wind dependencies of the gas transfer velocity k . (A) Temperature relationship of k at CE. Values for k (solid black circles), k normalized to 20°C (k_{20} ; open grey circles) and to a Schmidt number of 600 (k_{600} , solid grey circles) were clustered into 1.5°C temperature increments to account for temporal misalignments and to provide the most robust linear analysis ($R^2 > 0.9$; see Supporting Information Fig. 4). (B) Standardized k_{600} as a function of wind speed for CE (solid black squares), GA (open white squares) and both sites combined (dotted line). Wind speeds were clustered into 1 m s^{-1} bins to account for the dominant magnitude of wind fluctuations (see Supporting Information Fig. 5). Linear trends were obtained via least squares regression.

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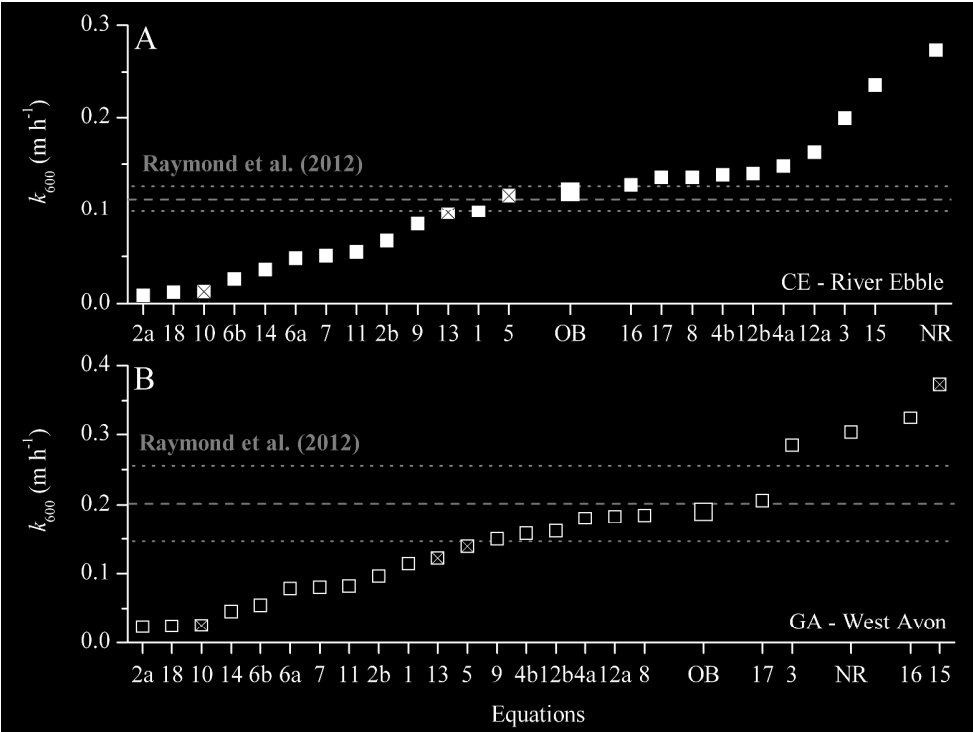


Figure 5. Estimates of k_{600} (in m h^{-1}) for (A) river Ebble and (B) West Avon. Estimates are obtained from different published hydrological parameterizations (Equations 1 – 18, and Raymond et al. (2012)); from the O_2 budget (OB) method used in this study (see Eq. 4); and from the nighttime regression (NR) method. Equation numbering follows Table 4. Note that crossed equations were reported to be the “top-performer” within a specific mean depth and mean flow range from an extensive database of tracer-based k_2 values and hydrological parameters (see Palumbo and Brown 2014). Mean value and uncertainty range (dashed and dotted lines) for the hydrological parameterizations of Raymond et al. (2012) were obtained by combining mean and range from of each equation. (see Table 4; Supporting Information Fig. 6). Note that to better highlight the differences between the OB, NR and common parametrizations, the equation order was re-arranged to show an incremental increase in k_{600} .

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Supporting information for**Headwater gas exchange quantified from O₂ mass balances at the reach scale**

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10 pages, 1 table, 6 figures

Supporting Tables

Table 4. Estimates of k_2 at 20°C ($k_{2(20^\circ\text{C})}$, in day⁻¹) from established empirical equations applied to the CE and GA study sites. Input variables[#]: d – stream depth (m), u – flow velocity (m s⁻¹), u^* – friction velocity (m s⁻¹), s – stream slope (m m⁻¹), Q – discharge (m³ s⁻¹), and $Fr = u/\sqrt{gd}$ – Froude number with g being the gravitational acceleration constant. Note that for equations providing k_{600} (in m day⁻¹) $k_{2(20^\circ\text{C})}$ values were scaled based on Eq. 7 and the O₂ Schmidt number at 20°C.

Eq.	Reference	Abbr. ^{##}	Equations	CE $k_{2(20^\circ\text{C})}$ [day ⁻¹]	GA
1	O'Connor and Dobbins (1958)	OD	$k_2 = 3.9 \frac{u^{0.5}}{d^{1.5}}$	6.303	5.206
2a	Churchill et al. (1962)	E ₄	$k_2 = 0.0217 \frac{u^{2.695}}{d^{3.085} s^{0.825}}$	0.563	1.044
2b		CEB	$k_2 = 5.01 \frac{u^{0.969}}{d^{1.673}}$	4.227	4.382
3	Krenkel and Orlob (1963)	E ₆ , KO	$k_2 = 173.01 \frac{(us)^{0.404}}{d^{0.66}}$	12.658	13.010
4a	Owens et al. (1964)	E ₈	$k_2 = 6.91 \frac{u^{0.73}}{d^{1.75}}$	9.407	8.226
4b		E ₉ , OEG	$k_2 = 5.35 \frac{u^{0.67}}{d^{1.85}}$	8.825	7.201
5	Dobbins (1965)	DB*	$k_2 = 55.2 \frac{1 + Fr^2}{(0.9 + Fr)^{1.5}} \frac{(us)^{0.375}}{d} \coth \left[\frac{4.75(us)^{0.125}}{(0.9 + Fr)^{0.5}} \right]$	7.443	6.342
6a	Langbein and Durum (1967)	E ₇	$k_2 = 5.14 \frac{u}{d^{1.33}}$	3.029	3.582
6b		LD	$k_2 = 5.14 \frac{u}{d^{0.67}}$	1.681	2.472
7	Issacs and Gaudy (1968)	IG	$k_2 = 4.76 \frac{u}{d^{1.5}}$	3.264	3.650
8	Cadwallader and McDonnell (1969)	E ₃ , CM	$k_2 = 186.07 \frac{(us)^{0.5}}{d}$	8.611	8.386
9	Negulescu and Rojanski (1969)	NR	$k_2 = 10.91 \left(\frac{u}{d} \right)^{0.85}$	5.419	6.856
10	Thackston and Krenkel (1969)	TK*	$k_2 = 24.9 \frac{u^*(1 + Fr^{0.5})}{d}$	0.813	1.140
11	Padden and Gloyna (1971)	PG	$k_2 = 4.53 \frac{u^{0.703}}{d^{1.054}}$	3.473	3.758
12a	Bennett and Rathbun (1972)	E ₁ , BR1	$k_2 = 32.69 \frac{u^{0.413} s^{0.273}}{d^{1.408}}$	10.357	8.365
12b		E ₂ , BR2	$k_2 = 5.58 \frac{u^{0.607}}{d^{1.689}}$	8.884	7.357
13	Parkhurst and Pomeroy (1972)	PP*	$k_2 = 48.5 \frac{(1 + 0.17Fr^2)(us)^{0.375}}{d}$	6.140	5.590
14	Bansal (1973)	BN	$k_2 = 1.81 \frac{u^{0.6}}{d^{1.4}}$	2.254	2.044
15	Owens (1974)	–	$k_2 = 50.8 \frac{u^{0.67}}{d^{0.85}}^{###}$	14.998	17.013
16	Tsivoglou and Neal (1976)	E ₁₀ , TN	$k_2 = k_2' us^{####}$	8.100	14.850

17	Smoot (1988)	SM	$k_2 = 543 \frac{u^{0.5325} s^{0.6236}}{d^{0.7258}}$	8.634	9.387
18	Thackston and Dawson (2001)	TD*	$k_2 = 4.97 \frac{u^*(1 + 9Fr^{0.25})}{d}$	0.740	1.077
19a	Raymond et al. (2012)	Rm ₁	$k_{600} = 5037(us)^{0.89}d^{0.54}$	7.150	10.524
19b		Rm ₂	$k_{600} = 5937(1 - 2.54Fr^2)(us)^{0.89}d^{0.58}$	7.965	11.520
19c		Rm ₃	$k_{600} = 1162u^{0.85}s^{0.77}$	6.106	7.321
19d		Rm ₄	$k_{600} = 951.5(us)^{0.76}$	6.169	7.018
19e		Rm ₅	$k_{600} = 2841us + 2.02$	8.048	7.410
19f		Rm ₆	$k_{600} = 929(us)^{0.75}Q^{0.011}$	6.488	7.296
19g		Rm ₇	$k_{600} = 4725(us)^{0.86}Q^{-0.14}d^{0.66}$	8.115	13.108

#: Average stream depth and flow velocity are taken from (Table 1). The average shear velocity, u_* , computed as $u_* = u(C_D)$ with C_D being the drag coefficient (Wüest and Lorke 2003). An average C_D of 3.3×10^{-3} was used for both sites based on fi surveys of the River Avon sub-catchments (Rovelli et al. 2017). The average slope, 0.002 m m^{-1} , was estimated from GPS measurements during the respective field campaigns.

##: Reference equation numbers and abbreviations from Aristegi et al. (2009) and Palumbo and Brown (2014), respectively.

###: This equation requires depth in cm and flow velocity in cm s^{-1} .

####: with k_2' being $31183 \text{ s m}^{-1} \text{ d}^{-1}$ for $Q < 0.280 \text{ m}^3 \text{ s}^{-1}$ and $22500 \text{ s m}^{-1} \text{ d}^{-1}$ for $Q > 0.280 \text{ m}^3 \text{ s}^{-1}$, respectively (Palumbo and Brown 2014).

*: These equations were identified to be the most suited (i.e., top performer) for the site mean depth and flow based on the suggestions of Palumbo and Brown (2014).

Supporting Figures

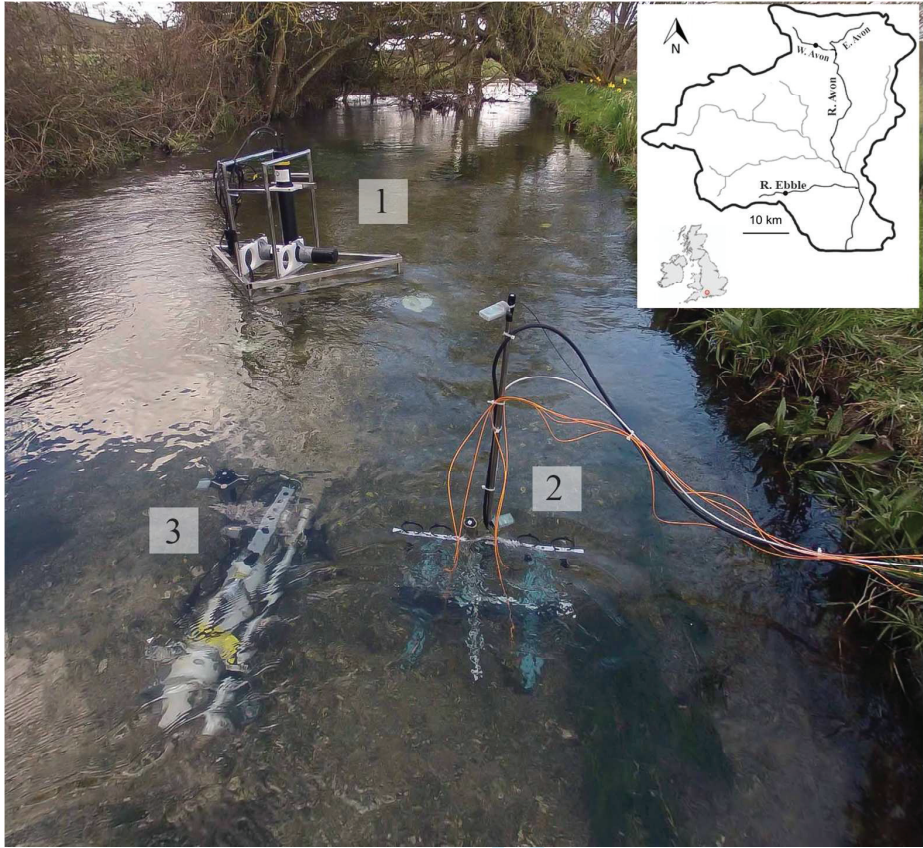


Figure S1. Catchment of the Upper River Avon and field measurement setup in the River Ebble (UK). The instruments consisted of [1] an aquatic eddy co-variance module, [2] a water column incubation stand, and [3] a CTD logger, which was also equipped with a PAR sensor and an O₂ optode. The setup also included riparian piezometers and a meteorological station (*see* Heppell et al., 2017). Dots on the catchment maps indicate the investigated reaches on the rivers Ebble (CE) on the Chalk, and West Avon (GA) on the Greensand.

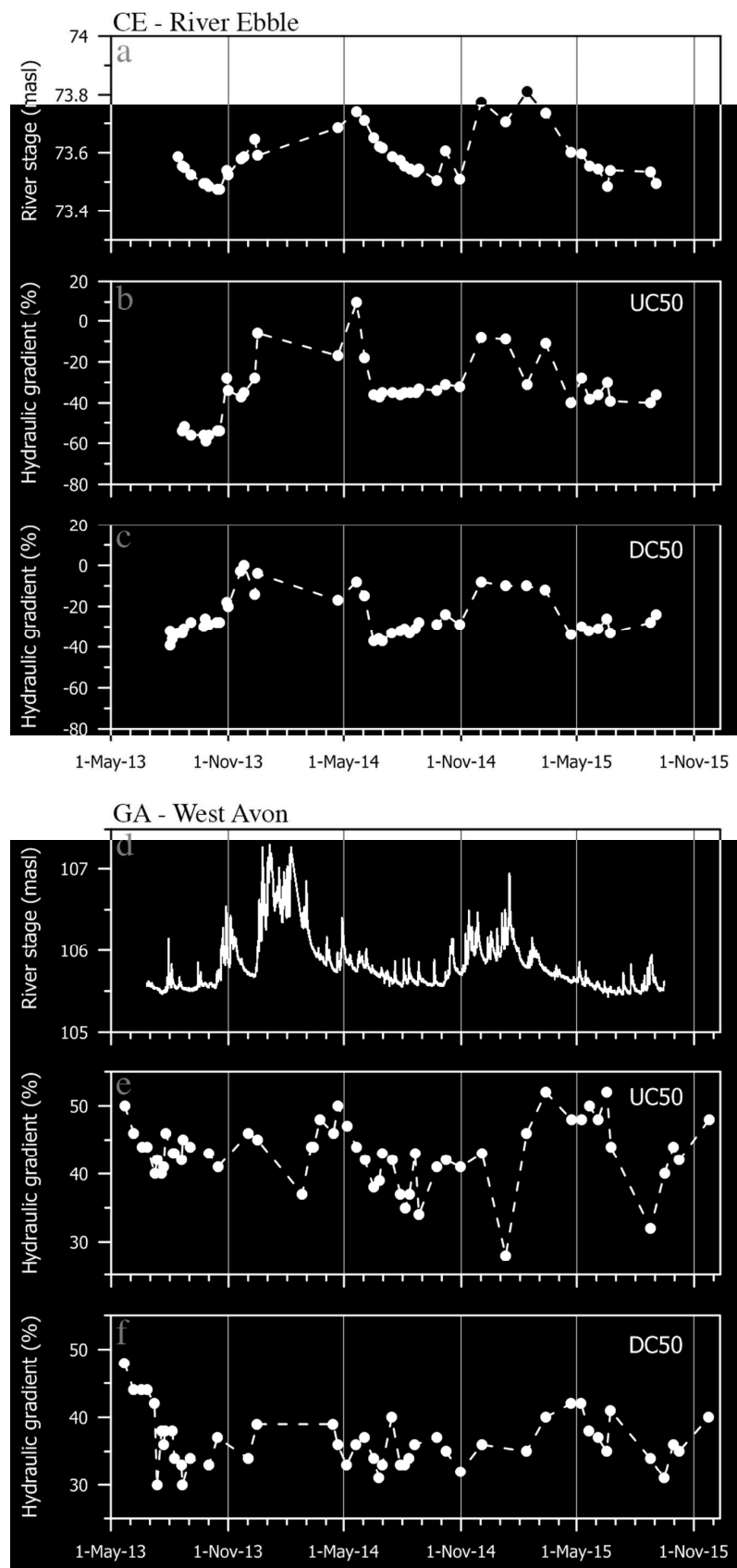


Figure S2. Stream stage and groundwater hydraulic gradient at the rivers Ebble (CE; a–c) and West Avon (GA; d–f). The hydraulic gradient was determined from in-stream 50 cm deep piezometers 10 m apart, upstream (UC50) and downstream (DC50), from dipped levels. Positive gradients indicate groundwater upwelling, i.e. a net inflow of groundwater into the stream, while negative gradients indicate downwelling, i.e., a net loss of water from the stream to the aquifer. Estimates for spring 2013 were assumed to be equal to the same period in 2014, as mean seasonal gradients were found to be comparable across consecutive years. Stage plot for CE (a) are based on dips, while GA stage time series (d) was obtained at 15-min interval from a pressure logger (HOB0 pressure transducer; Onset, USA) installed in the piezometer.

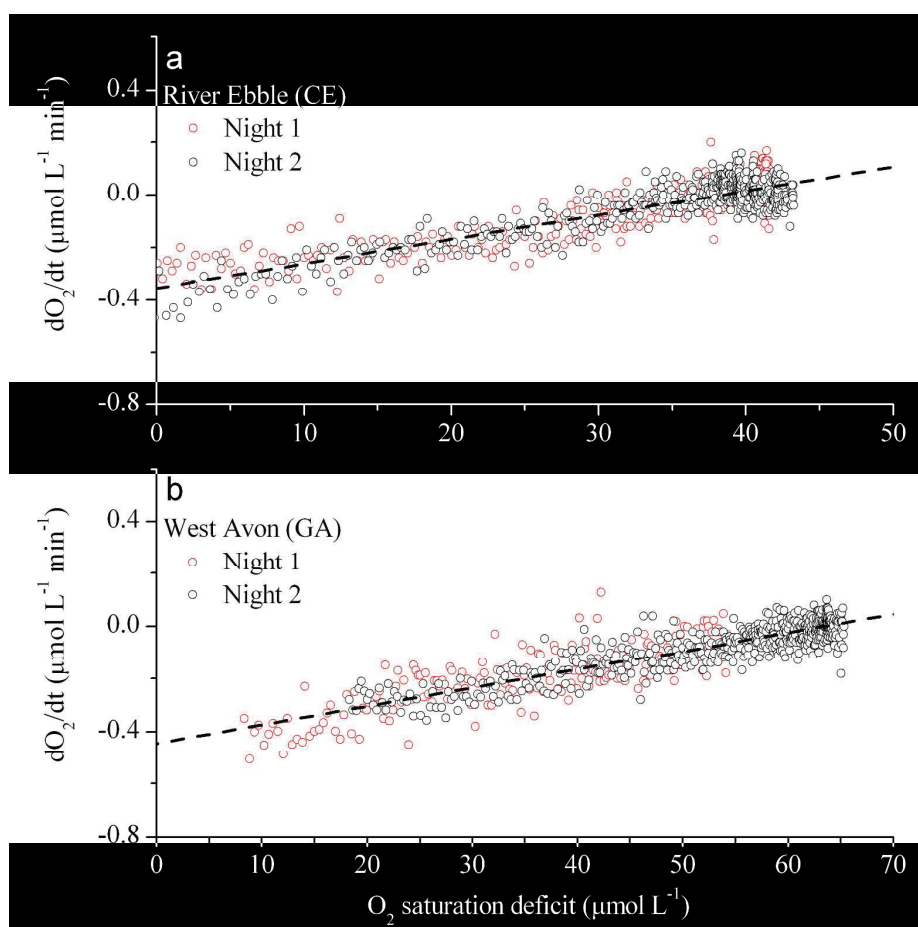


Figure S3. Nighttime regression (NR) method applied to in-stream measurements of O_2 at the rivers (a) Ebble (CE) and (b) West Avon (GA). The dashed line indicates the linear regression fitted through both night's data combined, with the slope representing the nighttime gas exchange coefficient (k_{NR}) and the intercept representing nighttime respiration. Values of k_{NR} and associated regression coefficients, R^2 , are presented in Table 2. Note that no statistically significant ($p < 0.05$) difference was observed between k_{NR} from night 1 and 2 at GA, while k_{NR} values at CE were statistically different, but within $<10\%$.

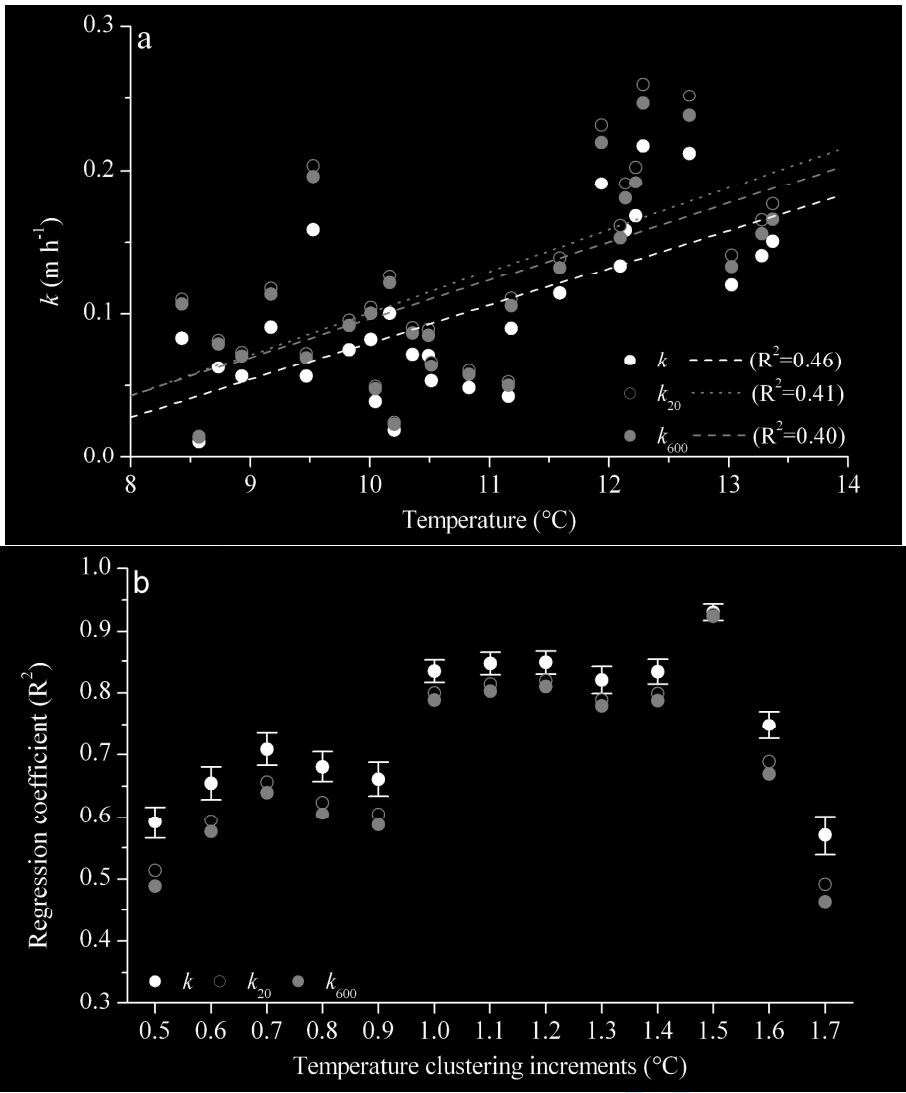


Figure S4. Temperature dependencies of the gas transfer velocity k at river Ebble (CE). (a) Local gas transfer velocity, k , and k standardized to 20°C (k_{20}) and to a Schmidt number of 600 (k_{600}) as a function of temperature. (b) Effect of temperature clustering increments on the relationship between temperature and local oxygen gas transfer velocity, k , and for k standardized to 20°C (k_{20}) and to a Schmidt number of 600 (k_{600}). For each increment, only clusters with $n \geq 3$ were considered usable for analysis by linear regression, to ensure that sparse single data points or data pairs would not bias the relationship; similarly, only increments with at least 4 data clusters were further considered for the regression analysis. The highest correlation ($R^2 > 0.9$) was obtained by clustering temperature in 1.5 °C increments. The standard deviation bars of R^2 values were comparable in size for k , k_{20} and k_{600} , but are only shown for k .

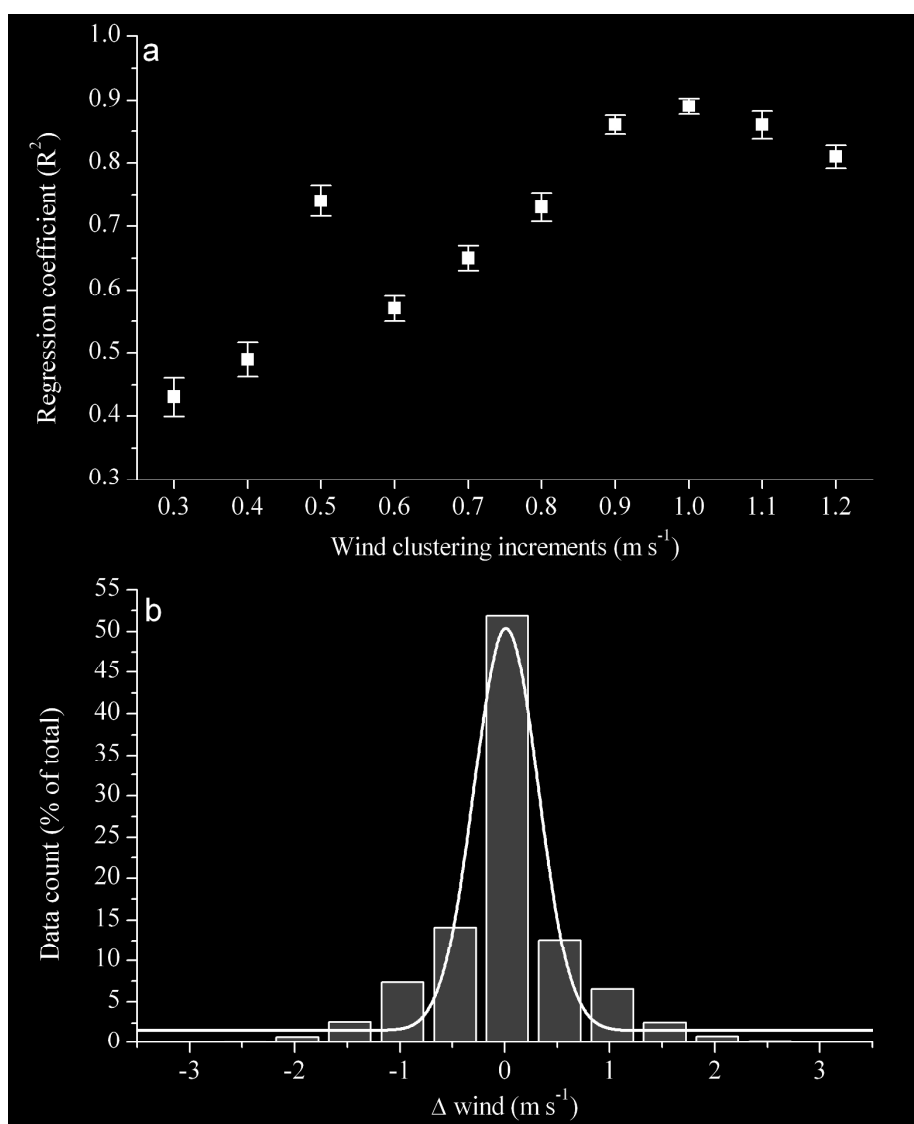


Figure S5. (a) Effect of wind clustering increments on the relationship between wind speed (m s^{-1}) and the standardized oxygen gas transfer velocity to a Schmidt number of 600 (k_{600}). For each increment, only clusters with $n \geq 3$ were considered suitable for analysis by linear regression, to ensure that sparse single data points or data pairs would not bias the relationship; similarly, only increments with at least 4 data clusters were further considered for the regression analysis. Note that the highest correlation was obtained by clustering wind dynamics in 1 m s^{-1} increments. Error bars indicate the standard deviation of R^2 . (b) Frequency count analysis on combined wind measurements at river Ebble (CE) and West Avon (GA). Based on a Gaussian distribution curve fit ($R^2=0.97$), $>90\%$ of the wind fluctuations were within $\pm 1 \text{ m s}^{-1}$.

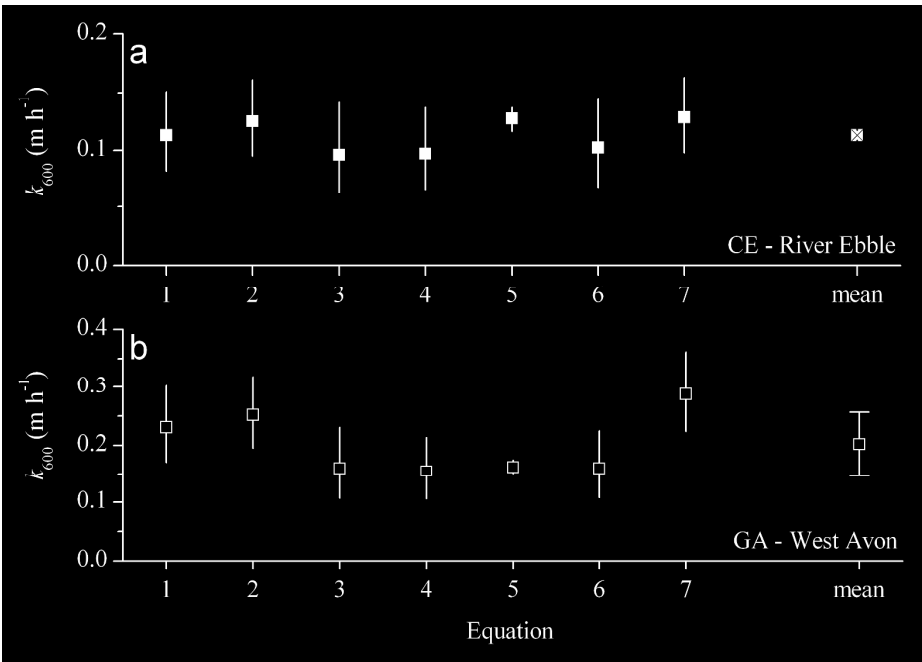


Figure S6. Prediction of gas transfer velocity (k_{600}) for (a) River Ebble (CE) and (b) West Avon (GA) based on each streams' hydraulic properties and the equations provided by Raymond et al. (2012). Error bars on each equation represent the statistical range of the estimates and were obtained by accounting for the variability (i.e., standard deviation) of each parameter (*see* Raymond et al. 2012). The combined mean value \pm standard deviation from all equation is also provided for comparison.