Waste glass as a source for green synthesis of microporous adsorbent for efficient removal of heavy metals

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# 17 Abstract

Microporous analcime Adsorbent (MaA) was cogently synthesized in a hydrothermal 18 reaction where a waste silica glass powder was mixed into NaOH solution. The satisfactory 19 reaction properties were achieved by regulating the conditioning time (Ct), reaction 20 temperature (Rt), and relative ratio of the reactants ( $Rr = SiO_2:Na_2O$ ). XRF, XRD, SEM, BET, 21 FTIR, AFM, TG and TEM analysis formed part of the selected samples. The prepared MaA 22 adsorbent was then applied to treat  $Pb^{2+}$ ,  $Cd^{2+}$  and  $Cu^{2+}$  ions, thus effectively allowing the 23 24 physicochemical properties (pH, temperature and contact duration), on the adsorption amount to be examined. Upon completion, the results indicated that the initial pH as well as the contact 25 duration had notable effect on the adsorption amount. Conversely, the temperature change had 26 27 an insignificant effect on the equilibrium adsorption amount. In addition, a dosage of 0.1 g/L of MaA, concentration of 100 mg/L, pH ranging from 6~8, and temperature of about 25°C were 28 found to be the optimum process conditions for the adsorption of the examined heavy metal 29 samples, whereas difference in contact time was recorded as follows: 1h for Pb<sup>2+</sup> and Cu<sup>2+</sup> ions 30

with adsorption amounts of 150.26 mg/g and 148.19 mg/g, respectively; and 3 h for Cd<sup>2+</sup> ion 31 with adsorption equal to 145.22 mg/g. In the analysis of the trend, the coefficients of correlation 32  $(R^2=0.99)$  of the Langmuir isotherm model were increasingly consistent compared to 33 Freundlich isotherm model ( $\mathbb{R}^2$  from 0.10 to 0.55), thus indicating that the process to be a 34 homogeneous monomolecular layer adsorption. Moreover, the kinetic aspects were similarly 35 consistent in relation to quasi-secondary kinetic equation, which then further established that 36 37 the process was primarily controlled by ion exchange, extra-particle, intra-particle, and liquid film diffusion. 38

# Keywords: Waste Glass; Green Synthesis; Analcime Zeolite; Heavy metals; Adsorption kinetics; Wastewater treatment.

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#### 1. Introduction

43 The adverse impact of solid waste pollution and other harmful substances on the natural ecosystem, human well-being, and the overall life's quality is a grave and critical global 44 45 predicament. Human activities that release contaminated pollutants into the air, water and soil 46 have continuously worsened the environment. Accordingly, whereas the management of such pollutants remains a great challenge, it is essential that it is resolved with utmost urgency. An 47 effective and efficient implementation of management practices such as recycling, reusing and 48 rational disposal could minimize pollution risks thereby optimizing the safety and protection 49 of the environment. It has been estimated that the annual worldwide production of solid waste 50 is about 2.01 billion tons, with 4-8% of the total volume comprising glass waste [1, 2]. As a 51 52 solid material with unique vitreous properties and stable silicate composition, glass is commonly used in various applications. For instance, in early 2021, approximately 22.75 53 54 million tons of waste glass was recorded in China, of which about 10.05 million tons were recycled, corresponding to a 44.2% recycling rate [3]. Although glass can be converted from 55

the solid broken or non-broken waste to produce by melting at high temperature a new glass 56 product repeatedly without losing its quality, its sorting by color and from other waste remain 57 58 a big challenge and onerous, especially in China where they are a lack of waste sorting infrastructures. Sorting the glass from multitudes of waste materials or by color increases 59 undeniably its market value. Furthermore, because of its heavy weight, transportation of glass 60 wastes to recycling plants demands a comparatively higher logistical cost. Thus, from an 61 62 economic, environmental and health perspective, recycling and re-utilization of waste glass is 63 a necessity.

As a non-biodegradable material by nature, glass has a very long-life cycle, and so as a 64 65 waste, adversely impacts the environment for an extended period without altering its chemical 66 properties. In fact, perpetual recycling of glass hardly alters its physicochemical properties due to the stable silicate (SiO<sub>2</sub>) and alumina (Al<sub>2</sub>O<sub>3</sub>) content. The two compounds are nearly similar 67 to zeolite in composition, thus creating the likelihood of a synthesis of functional minerals 68 through a suitable hydrothermal reaction for its applications as adsorbents. This property, 69 70 however, makes it a filter composite to remove harmful constituents [4], such as pollutants treatment from wastewater, oils and organic [5], pathogenic bacteria [6], and odors [7, 8]. In 71 72 fact, over the past decades, the need for adsorbents, which can effectively eliminate the 73 hazardous constituents from contaminated water, has increased. In particular, the need exacerbated due to the demand for clean water following pressures of population increase and 74 industrial activities for domestic and commercial use, respectively. Likewise, growing demand 75 76 for services, particularly in food production, has aggravated the degradation and pollution of natural water sources, which further worsens the state of drinking water [9-11]. Inorganic 77 pollutants, metalloids, organic pollutants, and microorganisms pollutes water sources and are 78 79 classified as heavy metals [12, 13]. Due to their large and increasing industrial use, heavy metals (HM) like lead (Pb), cadmium (Cd) and copper (Cu), etc. are of serious concern when 80

discharged as wastewater [14, 15] As toxins and pollutants, these elements through adsorption, bio-availability, bio-concentration, and bio-magnification exposes human physiology to reproductive, neurological, hematopoietic, skeletal, neurological, cardiovascular and renal systems disruptions [16-18]. Following these hazardous attributes, it is imperative that an alternative composite that can better absorb or eliminate heavy metals be developed.

Various methods for the elimination of HM ions from wastewater are currently available, 86 which include the processes such as coagulation [19, 20], chemical precipitation [1, 21], ion 87 exchange process [22, 23], membrane filtration or separation [24], reverse osmosis [25, 26] 88 and adsorption [27-29]. Of these processes, adsorption is comparatively becoming a better 89 90 alternative because of its lower cost, easier and faster operation, and wider range of 91 applicability [30-32]. Meanwhile, the search for a suitable and promising adsorbent with high adsorption capacity, rapid adsorption, and desorption kinetics as well as low energy is very 92 crucial to meet pilot and industrial level requirements. Consistent with the foregoing criteria, 93 additional considerations such as long-term durability, cheaper costs, sustainability, and 94 environmental friendliness should be prioritized. Number of suitable adsorbents for removing 95 HM, in particular carbon nanotubes, activated carbon, graphene oxide, mesoporous silica, 96 97 mesoporous carbon, clays, zeolites, metal organic frameworks and adsorbents obtained from 98 agricultural or industrial wastes have been developed [9]. Among these adsorbents, synthetized zeolites have drawn particular attention due to that its worldwide availability, which can be 99 found in different structures, its stable chemical compositions, good adsorption properties, 100 101 simple production method, and its high affinity for heavy metals removal. Analcime (NaAlSi<sub>2</sub>O<sub>6</sub>H<sub>2</sub>O) is a specie of zeolite and an important chemical mineral composed of 3D 102 rigid structure, which has been utilized in recent years for diverse applications. However, pure 103 104 and premium-quality analcime (ANA) is extremely rare, thus non-artificial and precious crystal must be sourced and purified to meet the industrial expectations and standard [33, 34]. 105

Previous studies have proved that favorable analcime may be synthesized by low-cost and 106 unhindered methods, e.g., the hydrothermal method [35, 36], especially from raw materials 107 108 such as coal fly ash, rice husk, quartz syenite, pyrophyllite, and amber container glass [37-41]. Although the use of recycled glass in the synthesis of zeolites has already been documented in 109 the literature, further studies and research are required on the hydrothermal conversion of silica 110 glass powder into synthetized zeolite for efficient removal of heavy metals from wastewater. 111 112 This work closely examines and considers the issue of hydrothermal conversion of silica glass powder into microporous adsorbent capable of treating Pb, Cd and Cu ions from wastewater. 113 114 The adsorbent is produced through a clean method, featuring XRF, XRD, SEM, BET, FTIR, AFM, TG and TEM. The data provided references for facile treatment of heavy metals that 115 may constitute a threat to human health. 116

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#### 2. Experimental section

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# 2.1 Materials

Beverage soda lime glass bottles having 69.43% SiO<sub>2</sub>, 15.35% Na<sub>2</sub>O, and 9.27% CaO 119 composition were used as raw material. The broken bottles were collected from Longgang 120 District Recycling Plant (Shenzhen). To avoid any inconsistencies due to mis-coloration, only 121 green color bottles were selected. The glasses were washed, dried, crushed to finer grit pieces, 122 123 and grounded using disc ball mill with 180 rpm speed for 30 min. The obtained fine glass powder (GP) was then screened and particle size  $<5 \mu m$  of the powder was collected. A fixed 124 ratio of glass powder GP:NaOH(aq, 3M) solution equal to 2:15 was adopted. The chemical 125 126 compositions in percentage of the NaOH, as specified by the manufacturer are Sulfate (SO<sub>4</sub>): 0.005, Phosphate (PO<sub>4</sub>): 0.001, Aluminum (Al): 0.002, Calcium (Ca): 0.01, Chloride (Cl): 127 0.005, Nitrogen (N): 0.001, Silicate (SiO<sub>3</sub>): 0.01, Potassium (K): 0.05, Iron (Fe): 0.001 and 128 Heavy metals (calculated as Pb): 0.003. 129

#### 2.2 Formation of the microporous analcime zeolite

The solid waste glass was converted into microporous powder through a hydrothermal 131 132 reactor. The measured glass powder was added to NaOH solution and mixed for about 5 min. The mixed slurry was then poured into a hydrothermal synthesis reactor, and imperviously 133 sealed for 3 hours at a conditioning temperature of 150°C. After the conditioning and normal 134 cooling, the resultant mixture was filtered through vacuum filtration equipment and thereafter 135 136 continuously cleaned with de-ionized water to neutralize. Finally, the resultant solid product was subjected to an 80°C drying heat for 24 hours. Fig. 1 illustrates the formation procedures 137 138 of the microporous analcime (MaA).



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Fig. 1 Experiment illustration: (a) Silica glass powder (GP) having 69.43% SiO<sub>2</sub>, 15.35% Na<sub>2</sub>O, 9.27% CaO
composition, (b) Pre-mixing of GP into NaOH solution, (c) Hydrothermal synthesis, (d) Filtration and deionization, (e) Wet analcime zeolite, (f) Drying process, (g) Microporous Analcime Adsorbent (MaA), Structure
of analcime [Na<sub>8</sub>Al<sub>8</sub>Si<sub>16</sub>O<sub>48</sub>(H<sub>2</sub>O)<sub>8</sub>]: (i) Crystal structure of analcime, (ii) 6-membered rings in analcime crystal,
4-membered rings in analcime crystal.

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#### 2.3 Adsorption of HM from contaminated solutions by MaA

Adsorption kinetic of the MaA in relation to heavy metals was recorded. 0.1 grams of dried
MaA was added into 10 mL solution of heavy metals with a mass fraction of 100 mg/L. The

modification of the pH's solutions was performed from 4.0-8.0. The mixtures were separately 150 stirred at 300 r/min at temperature varying between 20-40°C. An aliquot of 2 mL of the 151 152 prepared solution was withdrawn and filtrated via a syringe fitted with 0.22 µm membrane at time frames between 0–1440 min, followed by the pH control for different solution. Thereafter, 153 the dissolution rate of  $Pb^{2+}Cd^{2+}$  and  $Cu^{2+}$  was analyzed using inductively coupled plasma mass 154 spectrometer (Thermo Scientific iCAP RQ ICP-MS). Finally, the adsorption efficiency (AR) 155 156 and adsorption capacity (AC) of the MaA composite on the heavy metal's ions were calculated 157 using Eqs. (1-2).

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$$AR (\%) = \frac{C_0 - C}{C_0} \times 100\%$$
 (1)

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$$AC(mg/g) = \frac{(C_0 - C)V}{m}$$
 (2)

where *Co* denotes the metal ions concentration before adsorption (mg/L); *C* is the metal ions concentration after adsorption (mg/L); *V* is the volume of the aqueous solution (mL) and *m* is the mass of MaA adsorbent (g).

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### 2.4 Characterization methods

The element composition of GP and MaA were recorded by X-ray fluorescence (XRF, 165 Thermo Fisher ARL Perform'X). Diffraction pattern was recorded via X-ray diffractometer 166 (XRD, D8 Advance). The structure morphology was studied using field emission scanning 167 electron (Zeiss Gemini SEM 300), and the main chemical components distributions were 168 collected with the aid of energy dispersive X-ray spectroscopy (X-Max<sup>N</sup> Oxford Instruments). 169 The total BET surface area (S<sub>BET</sub>) and the distribution of the pore size were measured by 170 Micromeritics ASAP 2460. Fourier transform infrared spectroscopy (FTIR) was used to collect 171 the spectra at wavenumber ranging from 400–4000 cm<sup>-1</sup>. AFM investigation was carried out 172 on an Atomic Force Microscope (Dimension Icon). Thermogravimetric (TG) measurement was 173 performed on a Differential Scanning Calorimetry (TG-DSC STA 449 F5 Jupiter). TEM 174

imaging was obtained on an electron microscope (Talos F200X S/TEM) equipped with a fieldemission gun.

- 177 **3. Results and discussion**
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# 3.1 Synthesis and adsorption mechanism

Waste glass (WG) has silicate properties (MxO-nSiO<sub>2</sub> > 80%, M=Na, Ca, K, etc., x=1 or 179 2) and amorphous properties (~100%). The preparation of zeolite from WG is considered as an 180 optimization of solid waste recycling. By mechanically milling WG, ultra-fine glass powder 181 can be obtained, thereby increasing the specific surface area which consequently ensures an 182 activating effect on the glass micro-spheres. Under an alkaline environment, the amorphous 183 184 silica chains in the broken glass powder are feasible chemically. By increasing the reaction 185 temperature, the kinetics reaction accelerates, which in turn speeds up the production of analcime zeolite crystals from the glass powder. Using waste glass as the silica source and 186 reacting with NaOH solution in the reaction system, the main components in the waste glass, 187 such as SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, Na<sub>2</sub>O, CaO, etc., are gradually dissolved. In general, the reactivity of glass 188 powder in the alkali solution mainly comes from the Si dissolved in the glass body network 189 structure. SiO<sub>4</sub> tetrahedron is the basic unit of the silicate glass network structure. SiO<sub>4</sub> 190 tetrahedron is connected by bridging oxygen (Bridging Oxygen, BO); alkali metals such as Na, 191 192 K, Ca and non-bridging oxygen (Non-Bridging Oxygen, NBO) and SiO<sub>4</sub> tetrahedron connection [42]. 193

Under the hydrothermal condition, SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub> ions in the solution gradually crystallize and precipitate to form analcime zeolite crystals. Water molecules play an important role in the reaction as solvent and crystal grow This kind of zeolite has good adsorption, ion exchange properties and can be used as catalyzer. Hence, it interacts with heavy metal ions in the solution through ion exchange, chemical adsorption, and surface complexation (Fig. 2). Ion exchange leads to the replacement of cations Na<sup>+</sup>, K<sup>+</sup>, etc. in the zeolite crystals by heavy metal ions, forming ions adsorbed on the surface or in the pores of the analcime. Oxygen atoms on the surface of zeolite are electron-rich, and chemisorption enhances the stability of adsorption through the configuration of chemical bonds within oxygen atoms on the surface of zeolite and heavy metal ions. Surface complexation further enhances the adsorption performance through the composition of complexes amidst the hydroxyl groups (OH<sup>-</sup>) on the exterior of the analcime and the heavy metal ions.



Fig. 2 Synthesis of MaA and it adsorption mechanism on heavy metals: (a) Structure of silica glass, (b) Nonbridging oxygen (NBO) atoms sites hydroxylation by water dissociation and Na–OH formation: (i) Water
adsorption at the NBO site, (ii) NBO protonation (SiOH), and subsequent establishment of Na–OH interaction,
(c) MaA microporous adsorbent: (i) Tetragonal trioctahedral crystalline form observed via Scanning Electron
Microscope, (ii) Schematic of the pore structure, (d) Heavy metals adsorption process: (1) Physical adsorption
(Electrostatic attraction–Van der Waals' force), (2) Microprecipitation, (3) Ion exchange, (4) Surface
complexation.

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#### **3.2** Characterization of the microporous analcime zeolite

### *3.2.1 Elemental composition and morphology*

The elemental composition of the glass microspheres used in the hydrothermal process 221 were SiO<sub>2</sub> (69.43 wt %), Na<sub>2</sub>O (15.35 wt %) and CaO (9.27 wt %). Other elements such as 222 Al<sub>2</sub>O<sub>3</sub>, SO<sub>3</sub>, Fe<sub>2</sub>O<sub>3</sub>, TiO<sub>2</sub>, MnO, MgO and K<sub>2</sub>O were also found in negligible percentages. 223 Different types of glasses were distinguished according to their composition and silica mineral 224 content varying from 65 to 75%. SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> were the main minerals in the zeolization 225 process. During the 3 h hydrothermal treatment, the glass minerals were converted into purer 226 analcime zeolite (NaAlSi<sub>2</sub>O6•H<sub>2</sub>O) having clearer crystallinity, as confirmed by the XRD 227 pattern (Fig 3.a). The result is consistent with similar experiments conducted by Azizi et al. 228 [36], affirming that well-crystallized analcime gradually formed as the synthesis time extended. 229 In addition, the diffraction peaks of the analcime were predominant, indicating that these 230 hydrothermal conditions are sufficient to generate pure analcime. 231





Fig. 3 XRD and SEM morphology: (a) XRD pattern showing NaAlSi<sub>2</sub>O6•H<sub>2</sub>O as the predominant phase, (b) 20μm
structure of MaA composed of many well-formed crystals, (c) 2μm structure of MaA showing two big crystals,
(d) 1μm pores structure of MaA, (e, f) 200nm large-scale of the pores structure presented in MaA.

Fig 3. (b, c, d, f) are the SEM micrographs of the microporous material recorded at different 237 magnitudes. Evidently, multiple single analcime crystals are formed on the surface or 238 agglomerated amongst the powdery particles (Fig 3.b, c). As is widely known and generally 239 accepted, the zeolite nucleation is often determined by various factors, including 240 supersaturation degree of nucleation revulsion and reaction solution. The large-scale single 241 crystals observed in the structure can be adduced to the moderate degree of nucleation, since it 242 243 was revealed that until the crystals grow to the largest sizes, the small amount of nucleation can effectively supply sufficient reactive species in the reaction system [43, 44]. The 244 245 micrograph in Fig 3.d shows thin lamellas agglomerated micro pores distributed over the entire surface, which are more visible at 200 nm magnitude (Fig 3.e, f). At this scale, the porosity of 246 the material is more perceptible, and the interconnected oval-shaped pores are visible. The 247 permeability of the structure can be attested to the fact that the glass micro spheres become soft 248 and soluble during the hydrothermal reaction in NaOH dissolution. At this stage of 249 decomposition, the particles lose weight, and the pressure induces vaporized gas, which 250 generates pores in the structure of the formed crystals. 251

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### 3.2.2 BET permeability and surface area

The BET permeability and the surface area (SA) of the MaA were noted, as shown in Fig. 253 4. Specifically, the SA of MaA was recorded and was found to be around 63.69 m<sup>2</sup> g<sup>-1</sup>, with 254 Langmuir surface area of about 70.24 m<sup>2</sup> g<sup>-1</sup>. A desorption hysteresis was observed from P/Po 255 = 0.7 to 1.0 (Fig. 4a) due to the capillary condensation in the micro/meso-pores of MaA. Fig. 256 4.b presents the isotherm pressure composition of MaA. The absolute pressure varied between 257 0-700 mmHg, and the weight N<sub>2</sub>% ranged from 0-25. The BJH adsorption and desorption 258 259 aggregate volume of pores ranging 1.0-300 nm diameter were recorded to be respectively around 0.337 cm<sup>3</sup> g<sup>-1</sup> and 0.344 cm<sup>3</sup> g<sup>-1</sup>. Similarly, DH adsorption and desorption aggregate 260 volume of pores from 1.7 to 300 nm in diameter are ranged from 0.338 cm<sup>3</sup> g<sup>-1</sup> to 0.340 cm<sup>3</sup> g<sup>-</sup> 261

<sup>1</sup> (Fig. 4 c, e, g). The BJH and DH cumulative surface pore area were also recorded and presented in Fig. (4 d, f, h). It can be clearly noted that, between 1.0-300 nm, the cumulative surface area is around  $52.61 \text{m}^2 \text{ g}^{-1}$  and  $55.76 \text{ m}^2 \text{ g}^{-1}$ , respectively for BJH adsorption and desorption; while at 1.7-300 nm, the DH revolves around 42.91 m<sup>2</sup> g<sup>-1</sup> and 47.18 m<sup>2</sup> g<sup>-1</sup>, respectively, for adsorption and desorption cumulative surface area. In addition, the average diameter of adsorption and desorption pores were, respectively, 22.04 and 15.74 nm, which indicated that the porosity of MaA is higher.



Fig. 4 BET Adsorption/Desorption isotherm results: (a) Isotherm linear plot, (b) Isotherm pressure composition,
(c) BJH Adsorption dV/dD pore volume, (d) BJH Adsorption dA/dD pore area, (e) BJH Desorption dV/dD pore
volume, (f) BJH Desorption dA/dD pore area, (g) Cumulative pore volume vs. Pore width, (h) Cumulative surface
area vs. Pore width.

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#### 3.2.3 FTIR and AFM analysis

The morphology of MaA was further characterized by FTIR and AFM (Fig. 5). Fig. 5a shows the FTIR spectra of MaA, where the wavenumber varies from 914.12 cm<sup>-1</sup> to 3400.26 cm<sup>-1</sup>. The transmission percentages of 55.37, 52.92, 72.00, 92.33, 78.60, 92.42 and 91.05 were assigned respectively for 914.12, 954.19, 1040.85, 1170.38, 1420.11, 1642.82 and 3400.26 cm<sup>-1</sup>

<sup>1</sup> wavenumbers. The sharp bands at 914.12, 954.19 cm<sup>-1</sup> and the shoulder bands from 1040.85 280 and 1170.38 cm<sup>-1</sup> are due to the symmetric and asymmetric Si-O stretching oscillations. The 281 recordings of the band at 1420.11 cm<sup>-1</sup> is assigned to the vibration of  $CO_3^{2-}$  [45], and the band 282 around 1642.82 cm<sup>-1</sup> is attributed to the bending vibration of H–O–H of the adsorbed H<sub>2</sub>O and 283 H<sub>2</sub>O in the interlayer. Additionally, the large-band closely at 3400.26 cm<sup>-1</sup> wavenumber is due 284 to the stretching vibration of O-H [46, 47]. Fig. 5b details the results obtained from the atomic 285 286 force microscopy (AFM). The morphology of MaA shows irregular shapes with different particles sizes (Fig. 5b-i-ii), indicating the presence of multiple analcime crystals as described 287 288 by the SEM results. Evaluation of the 2D Planar and 3D surfaces between -1.3~2.0 nm in Fig. 5b(i-ii) shows the thin and polished appearance of MaA. From the height-length contour 289 through the solid line (Fig. 5b-iii), the average thickness of the porous MaA is estimated at 290 around 0.918 nm, indicating the slenderness of MaA. Notably, the result was obtained on the 291 surface layer of analcime without any ultrasonication treatment, which is known to 292 significantly direct the particle size dispersion as well as enhance the constancy and steadiness 293 of emulsions. 294



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Fig. 5 Characterization of MaA by FTIR and AFM: (a) FTIR spectra, (b) Atomic force microscopy (AFM)
imaging: (i) 2D Planar height surface, (ii) 3D surface morphology, (iii) Height-length contour with distance
between 0 to 1000 nm.

MaA is also distinguished and portrayed by DTG and DTA as shown in Fig. 6 and Table 1. It is noted from the DTA curve that there are two predominant peaks, which occur respectively after 100 and 300°C (Fig. 6a). The DTA curve also presents variable endothermic peaks.



305 Temperature (°C) time ranges
 306 Fig. 6 DTG-DTA analysis of MaA: (a) Derivative thermogravimetry ratio, (b) Mass loss, (c) Differential thermal
 307 analysis, (Table 1) Mass loss with respect to the temperature and time ranges.
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The endothermic peak occurring around 200°C in the DTA curve is abrupt and represents 309 310 the removal of physically adsorbed water from the MaA configuration. Moreover, two 311 consecutive endothermic crests are also noted at the broad thermal conditions from 500 to 312 800°C, indicating evaporation of the water tightly bound to the configuration as well as dehydroxylation by a greater water loss at higher temperatures (Fig. 6b). The curves describing 313 314 the mass loss with regard to the temperature and their respective values are presented in Fig. 6c and Table 1. As shown, the mass loss is a function of the temperature increase. As a result, 315 in the range of 30-1000°C, the mass loss drops from 0.91 to 0.78% with a total loss of 3.33% 316

within 97 min (Table 1), indicating that MaA is more porous and can be considered as anadsorbent material.

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#### 3.2.5 TEM electron microscope analysis

321 To study the microscopic appearance and distribution of MaA adsorbent nanoparticles, the TEM images are shown in Fig. 7. In general, the thinness of the fibers that make up MaA can 322 be clearly observed. The black specks below the fiber surface (Fig. 7a) are the result of the 323 aggregation and deposition of MaA nanoparticles at a later stage of synthesis. 2D pattern of a 324 SAED section was also captured (Fig. 7b). The pattern indicates diffraction spots, which are 325 related to the crystal structure of the sample. A large-scale single crystal was observed in the 326 327 structure by the aid of SEM and the image is displayed in Fig. 7c. As explained in section 3.2, 328 a moderate degree of nucleation is needed for the growth of large size crystal and a small amount of nucleation can effectively supply enough reactive species in the reaction system. 329 The distinctive chemical elements are also evenly distributed on the surface of MaA, as 330 presented in Fig. 7 (d, e, f, g, h, i). O and Si are high-density elements with atomic fraction of 331 about 66.90% and 18.91%, respectively. Tiniest traces of Ca, Na, Mg and Al are also visible at 332 5.22%, 4.33%, 2.90% and 1.73% respectively. In light of the foregoing, it can be confirmed 333 with certainty that the synthetized MaA adsorbent is characterized by the discrete nanoparticles 334 335 with homogeneous pore surface, which results in the eminent adsorption property for the full destruction of HM ions. 336



Fig. 7 TEM morphology of MaA: (a) TEM nanosheets imaging, (b) selected area electron diffraction (SAED)
pattern, (c) SEM large scale single crystal of MaA, (d, e, f, g, h, i) Elemental mapping of O, Na, Mg, Al, Si and
Ca at 100 nm scale.

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## 3.3 Heavy metals adsorption capability of the MaA adsorbent

343 *3.3.1 Effect of initial pH* 

The potential of hydrogen (pH) in solution influences the adsorbent by changing the exterior charge as well as the degree of protonation of the adsorbent, thus increasing the model ions in the solution. This aspect greatly influences the solution concentration and the adsorption process of heavy metals ions in wastewater [48, 49]. Because Pb<sup>2+</sup>, Cd<sup>2+</sup> and Cu<sup>2+</sup> solutions

generate precipitation at different pH, this research only discusses the effect of adsorption of 348 MaA at pH varying between 4~8. It is important to emphasize that these conditions can vary 349 depending on the specific conditions of the solution, such as the presence of other ions and 350 temperature. In this study, three different heavy metal solutions of Pb, Cd and Cu were prepared 351 with initial concentration of 100 mg/L. A volume of 10 mL of the concentration was taken and 352 mixed with 0.1 g of MaA. The slurry was then mixed separately in a thermostatic oscillator at 353 354 the set conditions of temperature T=25°C, time t=1h and vibration frequency n=300 rpm/min. Afterwards, a volume of 10 mL of the homogeneous liquid of each metal was collected and 355 356 adsorption experiment test was performed.

As shown in Fig. 8a, the adsorption rates of  $Pb^{2+}$ ,  $Cd^{2+}$  and  $Cu^{2+}$  by MaA show different 357 trends against pH level. The removal of Pb<sup>2+</sup> by MaA at different pH presents rather linear 358 trend compared to the other two metals. The removal rate rose with the increase of the pH of 359 the adsorption mixture attaining the maximum of 95.83 mg/g at pH=8. However, it was also 360 found from the same figure that, the removal of  $Cd^{2+}$  and  $Cu^{2+}$  by MaA has a higher adsorption 361 rate at pH=6. A similar curve pattern was observed for both metals and the maximum removal 362 rate was about 78.23 mg/g and 49.28 mg/g, respectively for Cd<sup>2+</sup> and Cu<sup>2+</sup>. Moreover, the 363 elimination of  $Cu^{2+}$  was much lower than that of  $Pb^{2+}$  and  $Cd^{2+}$  at dissimilar pH values, and a 364 net difference of the Cu solution color was observed after the addition of MaA (Fig. 8d). 365 Notably, only the solution of Cu ion was evidently lighter blue and became transparent after 366 the addition of MaA. The solution of Pb and Cd ions were colorless and transparent and 367 retained their respective appearance even after addition of MaA adsorbent. 368

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#### 3.3.2 Effect of temperature

To better clarify the influence of thermal conditions on the removal of the studied metals by MaA, the pH value of the mixture was kept to 4.0-8.0, while temperature of the thermostatic oscillator was adjusted to 20°C, 25°C, 30°C, 35°C and 40°C, respectively. The other conditions

were kept constant. The thermal impact on the adsorption efficiency is shown in Fig. 8b. 373 Evidently, the adsorption of the heavy metals does not significantly increase when the 374 temperature is ranged from 20-40°C. With further increase of the temperature to 25°C, the 375 adsorption increases only slightly and is most remarkable in the  $Cu^{2+}$  ions solution. From these 376 results, it can be concluded that the temperature does not have much influence on the 377 elimination of the studied heavy metals. Consequently, ambient temperature (25°C) is 378 recommended when MaA adsorbent is used for treating  $Pb^{2+}$ ,  $Cd^{2+}$  and  $Cu^{2+}$  ions in wastewater. 379 This novel combination can facilitate an ecologically friendlier, simpler and broader on-site 380 381 application of MaA for the treatment of contaminated water.

382

#### 3.3.3 Effect of contact time

The equilibration duration is of special significance while considering the economical 383 aspect of wastewater reclamation and treatment. The transfer of metal ions induced by steering 384 forces (vibration or concentration differential), the accessibility of active sites, etc. [50], and 385 bonding interactions between metal ions and the adsorbent are some of the factors affecting 386 387 equilibration duration. The impact of contact duration of MaA on the metals was also examined. 388 The dosage of 0.1 mg/L of the adsorbent was adopted. Meanwhile, other parameters were regulated as follows: reaction temperature was 25 °C, adsorption time was 0~1440 min, and 389 the pH was 6. It was noticed that, at the first 60 min, the adsorption of Pb<sup>2+</sup> and Cu<sup>2+</sup> reached 390 equilibrium, and Cd<sup>2+</sup> approached equilibrium 2 h later, after a total contact time of 3h (Fig. 391 8c). The equilibrium adsorption amounts were 150.26 mg/g, 145.22 mg/g, and 148.19 mg/g, 392 respectively for Pb<sup>2+</sup>, Cd<sup>2+</sup>, and Cu<sup>2+</sup>. Moreover, the analysis indicated that the adsorbed 393 amount of Pb<sup>2+</sup> by MaA adsorbent was larger than that of the other two heavy metal ions, and 394 395 the adsorption process in this case was faster than that of the other metals. In summation, a reaction period of 1h is needed for the adsorption to attain an equilibrium state when treating 396 Pb and Cu ions, while 3h is needed for the total elimination of Cd metal ion. If all three metals 397

399

are treated simultaneously by MaA adsorbent, 3h treatment is recommended, which can simplify and suitably smooth the adsorption process.



400Time (h)Heavy metals absorption test401Fig. 8 Effect of different parameters on the heavy metals adsorption: (a) Initial pH, (b) Temperature, (c) Contact402time, (d) Mixing of MaA into Pb, Cd, Cu solutions with thermostatic oscillator at the set conditions T=25°C, t=1h403and n=300 rpm/min.

- 404
- 405

#### 3.4 Adsorption isotherms of MaA adsorbent

The adsorption proficiency of the microporous MaA adsorbent was examined by analyzing its adsorption isotherms. Various models were employed to explain the experimental findings in the form of isothermic adsorption [51-53]. The Langmuir and Freundlich adsorption models were employed in this research to shed light into the final concentration and absorbed amount of the lead (Pb), cadmium (Cd) and copper (Cu) after addition of MaA adsorbent. The Langmuir model describes monolayer adsorption, whereas the Freundlich model illustrates the process of heterogeneous adsorption. Langmuir model assumes that a monomolecular layer covers the surface of the adsorbent, and the adsorbates have the same force at the solid surface and do not interact with each other. It can be mathematically expressed by:

415 
$$q_e = bq_m \rho_e / (1 + \rho_e) \tag{3}$$

416 
$$R_L = l/(l + b\rho_0)$$
 (4)

417 Where  $q_e$  denotes the equilibrium adsorption amount, *b* the Langmuir adsorption constant, 418  $q_m$  the saturated adsorption capacity.  $R_L$  designates the separation coefficient reflecting the 419 magnitude of affinity between the adsorbent and adsorbate,  $R_L > I$  (non-preferential adsorption), 420  $R_L = I$  (linear adsorption),  $0 < R_L < I$  (preferential adsorption),  $R_L = 0$  (irreversible adsorption) [54, 421 55].

The Freundlich model, on the other hand, is a factual adsorption equation that predicts a non-homogeneous adsorption process with sites on the surface of the adsorbent having different adsorption energies, and is expressed as:

425 
$$q_e = K_F \rho^{1/n}$$
 (5)

426

427 Where  $K_F$  is the Freundlich constant,  $\rho$  denotes the adsorbate's equilibrium concentration 428 and *n* is the Freundlich exponent [56, 57].

The kinetic adsorption models can also be used to express the speed of the adsorption during the process, with contact time as a variable. In this study, the adsorption kinetics of the studied heavy metals by MaA adsorbent was carried out by taking, respectively, 10 mL of Pb<sup>2+</sup>  $Cd^{2+}$  and  $Cu^{2+}$  solution with a concentration of 100 mg/L. A mass m = 0.1 mg of MaA adsorbent was added into the solutions and the mixtures were subjected to a thermostatic oscillator under the conditions of 25°C, pH=6, n=300 rpm/min. The adsorption kinetics of the adsorbents are mainly explored by two kinetic models, the quasi-primary kinetic model [58] and the quasi-secondary kinetic model [59]. The mathematical form of the model is:

437 
$$ln(q_e - q_t) = ln q_e - \frac{k_l}{2.303}t$$
 (6)

$$438 \qquad \frac{t}{q_t} = \frac{1}{k_2 q_e^2} \cdot \frac{t}{q_e} \tag{7}$$

Where *t* designates the adsorption time (min),  $q_t$  and  $q_e$  denote, respectively, the adsorption at time *t*, and the adsorbed amount per unit mass (mg/g) when equilibrium is reached. The quasi-primary kinetic rate constant (min<sup>-1</sup>) is expressed through  $k_1$  and the quasi-secondary kinetic rate constant [g/(mg min)] is expressed through  $k_2$ . Plotting *t* with the help of  $lg(q_e-q_t)$ yields  $k_2$ . Plotting *t* with the help of  $t/q_t$  yields  $k_2$  and  $q_e$  [60].

444

Table 1 Adsorption isotherm fitting by MaA

HM-id		Freundlich				
	$q_m/(mg \cdot g^{-l})$	$b/(L \cdot mg^{-l})$	$R^2$	Κ	1/n	$R^2$
Pb	75.0811	0.0323	0.9974	85.59	0.0418	0.1029
Cd	75.5300	0.1127	0.9956	114.4	0.2105	0.5858
Cu	74.0542	0.0701	0.9996	67.1	0.2471	0.5547

445

\**HM-id* = *Heavy metals identification* 

The process of adsorption of Pb, Cd and Cu on the MaA adsorbent were fitted using the 446 contact time data in Fig. 7c, as shown in Table 1, where the correlation coefficients of 447 Freundlich adsorption isotherm are  $R^2 = 0.1029$ , 0.5858, and 0.5547, respectively for Pb, Cd 448 and Cu. Similarly, the  $R^2$  of the respective metals are 0.9974, 0.9956, and 0.9996 for the 449 Langmuir adsorption isotherm. The results indicate that the regression constant of the 450 Langmuir isotherm is higher compared to the Freundlich isotherm. In addition, the adsorption 451 data is in line with that of the Langmuir isotherm. In sum, the Langmuir adsorption isotherm 452 equation can better characterize the adsorption process for the proper removal of Pb, Cd and 453 Cu by using the microporous MaA adsorbent. 454

455

Table 2 Kinetic fitting by MaA

HM-id		Quasi-p	orimary kinetic		Quasi-secondary kinetic			
	$Q_{e,exp}/(mg \cdot g^{-1})$	$Q_{e,cal}/(mg \cdot g^{-l})$	$K_l/min^{-l}$	$R^2$	$Q_{e,cal}/(mg \cdot g^{-l})$	$K_2/(g \cdot mg^{-1} \cdot min^{-1})$	$R^2$	
Pb	1027	663.7	0.5412	0.2456	1074.3	0.00201	0.9933	
Cd	306	163.2	0.5385	0.2341	323.6	0.00847	0.9991	
Cu	239	100.8	0.5323	0.3084	249.3	0.01040	0.9971	





Fig. 9 Adsorption kinetics results: (a) Quasi-primary kinetic fitting, (b) Quasi-secondary kinetic fitting.

The results from the quasi-primary and quasi-secondary kinetic models are presented in 461 Table 2 and Fig. 9. As shown, the coefficients of the quasi-primary kinetic models are estimated 462 to  $R^2 = 0.2456$ , 0.2341, and 0.3084, respectively for Pb, Cd and Cu, whereas, for the quasi-463 secondary kinetic, the coefficients are 0.9933, 0.9991, and 0.9971. Accordingly, the results 464 show that the quasi-secondary kinetic model presents the largest  $R^2$  coefficient, good linear 465 correlation, and the  $R^2$  values obtained from all metals fitted better the kinetic equations 466 compared to the values obtained for the quasi-primary reaction kinetic equations. The results 467 denote that the general adsorption efficiency of  $Pb^{2+}$ ,  $Cd^{2+}$  and  $Cu^{2+}$  by employing MaA is 468 primarily controlled based on chemical process, deducible to the electron transfer or exchange 469 by covalent forces between adsorbent and adsorbate. The adsorbent surface is charged during 470 chemical adsorption, hence reacting with the metals. In addition, a conclusion can be drawn 471 that, the adsorption of  $Pb^{2+}$ ,  $Cd^{2+}$  and  $Cu^{2+}$  by MaA adsorbent prepared using waste glass is 472

473 more compatible with this model. Moreover, the obvious adsorption of all these heavy metals
474 inherently occurs via the chemisorption mechanism, which plays a dominating role during the
475 adsorption process [53, 61-63].

476

# 4. Conclusions

Waste glass-based microporous analcime adsorbent with high surface area was cogently 477 synthesized through hydrothermal conditions. The optimum yield and permeability were 478 479 achieved at a low thermal condition of 150°C and NaOH molarity (3M). The adsorption capacity of the porous adsorbent was examined by removing lead (Pb), cadmium (Cd) and 480 481 copper (Cu) from aqueous solution. It was intended as an efficient redress for contaminated water. This adsorbent eliminated, respectively, 150.26 mg/g and 148.19 mg/g of lead and 482 copper after 1h of treatment and was able to absorb efficiently 145.22 mg/g of cadmium within 483 3 h. The obtained data are more consistent with the Langmuir adsorption model than the 484 Freundlich adsorption model, suggesting that the process was a homogeneous monomolecular 485 486 layer adsorption. Similarly, the adsorption kinetic results were congruent with the quasisecondary kinetic equation, confirming that the process is mainly controlled by chemisorption 487 process for expeditious elimination of Pb, Cd and Cu. In essence, this research proposes a 488 simpler and cleaner procedure for producing pure and efficient adsorbent from waste glass 489 490 powder, thus a new waste-to-useful resource. The experiments also demonstrated a harmless treatment of heavy metals that may be hazardous to human health. 491

492

# Declaration of interests

The authors declare that they have no known competing financial interests or personalrelationships that could have appeared to influence the work reported in this paper.

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